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LOCKHEED-CALIFORNIA CO BURBANK

A METHOD OF ANALYSIS FOR GENERAL AVIATION AIRPLANE STRUCTURAL C--ETC(U)

SEP 76 G WITTLIN, M A GAMON

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A METHOD OF ANALYSIS FOR GENERAL AVIATION
AIRPLANE STRUCTURAL CRASHWORTHINESS

LOCKHEED-CALIFORNIA COMPANY, BURBANK

SEPTEMBER 1976

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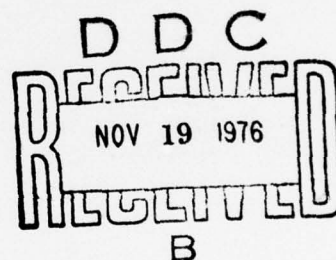
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A METHOD OF ANALYSIS FOR
GENERAL AVIATION AIRPLANE
STRUCTURAL CRASHWORTHINESS

Gil Wittlin

Max A. Gamon



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16. Abstract The results of the Task I effort to develop a method of analysis of the structural response of general aviation airplane subjected to a crash environment are presented. A review and evaluation of 8491 accidents obtained from National Transportation Safety Board (NTSB) tapes are presented. Eighteen (18) accident cases from the FAA Civil Aeromedical Institute (CAMI) files are discussed. The performance parameters and structural design characteristics associated with 61 general aviation airplane models are used to establish several airplane categories for light fixed-wing aircraft. An accident data computer program, developed by the Cessna Aircraft Company, is presented. The requirements for performing computerized crash analysis of general aviation airplanes during probable accident conditions are described. Program KRASH, as modified to meet the requirements of the general aviation industry, is described and assessed with the use of two sets of crash test (stall-spin and overturn) data for a single-engine high-wing and a single-engine low-wing airplane. The mathematical models and the comparison of analysis and test results for both airplanes and accidents are presented. Program KRASH is shown to have the potential to be used as an analytical tool which can facilitate the development of improved crashworthiness in general aviation airplanes.			
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METRIC CONVERSION FACTORS

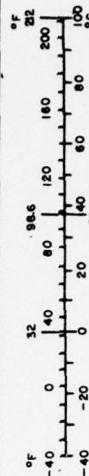
Approximate Conversions to Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
in	inches	2.5	centimeters	cm
ft	feet	30	meters	m
yd	yards	0.9	kilometers	km
mi	miles	1.6		
AREA				
in ²	square inches	6.5	square centimeters	cm ²
ft ²	square feet	0.09	square meters	m ²
yd ²	square yards	0.8	square meters	m ²
mi ²	square miles	2.6	square kilometers	km ²
	acres	0.4	hectares	ha
MASS (weight)				
oz	ounces	28	grams	g
lb	pounds	0.45	kilograms	kg
	short tons (2000 lb)	0.9	tonnes	t
VOLUME				
teaspoon	teaspoons	5	milliliters	ml
fl oz	fluid ounces	15	milliliters	ml
c	cups	30	milliliters	ml
pt	pints	0.24	liters	l
qt	quarts	0.47	liters	l
gal	gallons	0.95	liters	l
ft ³	cubic feet	3.8	liters	l
yd ³	cubic yards	0.03	cubic meters	m ³
		0.76	cubic meters	m ³
TEMPERATURE (exact)				
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C

*1 in. = 2.54 exactly. For other exact conversions and more detailed tables, see NBS Misc. Publ. 286, Units of Weights and Measures, Price \$2.25, SD Catalog No. C13.110.286.

Approximate Conversions from Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
mm	millimeters	0.04	inches	in
cm	centimeters	0.4	inches	in
m	meters	3.3	feet	ft
km	kilometers	1.1	yards	yd
		0.6	miles	mi
AREA				
cm ²	square centimeters	0.16	square inches	in ²
m ²	square meters	1.2	square yards	yd ²
km ²	square kilometers	0.4	square miles	mi ²
ha	hectares (10,000 m ²)	2.5	acres	
MASS (weight)				
g	grams	0.035	ounces	oz
kg	kilograms	2.2	pounds	lb
t	tonnes (1000 kg)	1.1	short tons	
VOLUME				
ml	milliliters	0.03	fluid ounces	fl oz
l	liters	2.1	pints	pt
		1.06	quarts	qt
l	liters	0.26	gallons	gal
m ³	cubic meters	35	cubic feet	ft ³
		1.3	cubic yards	yd ³
TEMPERATURE (exact)				
°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature	°F



FOREWORD

This report was prepared by the Lockheed-California Company under Contract DOT-FA75-WA-3707. The report contains a partial description of the effort performed as part of Task I and covers the period from July 1975 to July 1976. The work was administered under the direction of the Federal Aviation Administration Development Section C, with H. Spicer acting as Technical monitor.

The program leader was Gil Wittlin of the Lockheed-California Company. Important contributions were made to the program by the Cessna Aircraft Company, which participated as a subcontractor. Under the direction of D. J. Ahrens and W. B. Bloedel, the Cessna Aircraft Company provided valuable data with regard to general aviation structure, designs, and procedures and developed a computer program for selecting accident data from NTSB tapes. M. A. Gamon of the Lockheed-California modified program KRASH, which he originally developed. R. Ortiz of the Lockheed-California Company provided valuable computer programming support. P. C. Durup of the Lockheed-California Company assisted in the preparation of reports. The Lockheed effort was performed under the supervision of J. E. Wignot.

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SUMMARY

The results of the Task I effort to develop a method of analysis of the structural dynamic response of general aviation airplanes subjected to a crash environment are presented.

Included in this report is the review and evaluation of 8491 accidents obtained from the National Transportation Safety Board (NTSB) tapes for the period 1971 through 1973, the detail evaluation of 18 accident cases from the FAA Civil Aeromedical Institute (CAMI) accident files, and the performance parameters and structural design characteristics associated with 61 general aviation airplane models produced by the major domestic manufacturers. Several categories are established and presented which relate airplane configuration (low-wing, high-wing, single-engine, twin-engine), performance (speed, weight), usage, and occupant capacity. The accident data is related to the airplane categories with the use of a computer program designed to select and process NTSB accident data. This computer program was developed by the Cessna Aircraft Company during this task and is described, in detail, in Appendix A. The accident data is presented with regard to the potential of incurring fatalities during probable accident conditions.

The current and near future computer capability available to the general aviation industry was investigated and found to be compatible with the reasonably large computer programs needed to perform crash analysis. Requirements for performing computerized crash analysis of general aviation airplanes during probable accident conditions are presented. These requirements are compatible with the need to analyze reasonably complex crash conditions, yet, not impose unrealistic and costly investments in specialized manpower and/or equipment to facilitate improved future crashworthy designs.

Program KRASH is briefly described. The modifications to meet the requirements of the general aviation industry, as well as expand KRASH's versatility, flexibility and economy of operation are described. The capability

of program KRASH, modified during Task I, is assessed with the use of two sets of crash test data (stall-spin and overturn) for a single-engine high-wing airplane and a single-engine low-wing airplane. The tests and their results are described in detail. The math models for both airplanes and crash conditions are presented.

Program KRASH is shown to have the potential to be used as an analytical tool which can facilitate the development of improved crashworthiness in general aviation airplanes. The program requires verification with fully instrumented full scale crash tests to ascertain its maximum capability, as well as define its limitations.

The results of the Task I effort are summarized prior to stating the Task I conclusions. Appendices B and C are included and contain film analysis data, airplane model data and typical structural data and configurations for the two airplanes which are analyzed in Task I.

The development of a KRASH User's Manual and structural crashworthiness design guidelines during the Task I effort is described in a separate document.

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SECTION 1

INTRODUCTION

1.1 BACKGROUND

The general aviation industry has grown to the point where their airplanes now carry 90 million people annually and operate out of all the nation's 12,700 airports (Reference 1). Since general aviation airplanes have been proven to be competitive with other forms of transportation, it can be anticipated that the industry's growth rate will continue to accelerate rather than abate. With the increase in air traffic there has been an increase in the number of injuries and fatalities as a result of aircraft accidents. Correspondingly, an increasing effort is being expended to reduce the number of persons injured and the number of deaths resulting from vehicular accidents. The aircraft industry has been mindful of their obligations in this area over a number of years. Through the guidance of the FAA (CAA in the past) great strides have been made in the prevention of accidents by including improved air safety and airworthiness characteristics in the design of aircraft. FAA requirements have been developed and proven by study, tests and operations, that have led to significant improvements to survivability in controlled crashes. These requirements have primarily pertained to seat, harness and seat attachment strength capabilities. General airframe capability requirements for controlled crashes have been in the form of showing that the ditching characteristics and structural strength, under certain impact conditions, will not inhibit egress from the airframe.

The controlled crash requirements have undoubtedly provided some measure of protection for the more severe uncontrolled crash. Efforts such as the joint program sponsored by the FAA (CAA) and the Department of Agriculture in 1950 at Texas A and M have resulted in the development of an agricultural airplane with significant crashworthy features. The designers recognized

that to survive a crash that may be encountered by this airplane, the occupant chances of survival could be increased by placing the hopper, a large mass item, ahead of the pilot which then acted also as crushable material on impact. In addition, the cockpit was designed to provide a protective cage for the pilot during uncontrolled crash conditions and was equipped with a seat and harness of commensurate capabilities. This effort illustrated what could be accomplished with an airplane of a specific configuration having a definable mission and that normally flies at low airspeeds. This agricultural airplane program undoubtedly has resulted in the saving of a number of lives because it formed the basis for later agricultural airplane designs.

FAA sponsored research in the areas of seat harness designs, seat attachment strengths, and fire hazards has improved the occupant's chances to survive under crash conditions. With the progress in technologies and the ability to reduce them to practice, further advancements in crashworthiness can be expected. However, the methods that are to provide the advancements must be adaptable to a number of practical considerations in order to be successful. Some of these considerations are:

- o ease of airframe producibility,
- o operational use of the airplane,
- o adaptability to various preliminary design iterative procedures,
- o effect on airframe weight and cost, and
- o adaptability to various airframe configurations and airplane crash conditions.

In addition to these practical considerations, the methods that produce the advancements in crashworthiness must reliably predict for occupant safety whether or not

- o the structure containing the habitable space will collapse sufficiently to impinge upon the occupant,
- o the structure will crush and deform in a controlled predictable manner such that the forces imposed upon the occupant are minimized, and

- o the occupant is protected from lethal blows as a result of contact with hardware.

Through efforts sponsored by the FAA, NASA/LRC (Reference 2), and the U.S. Army, Fort Eustis Directorate, methods have been and are being developed which predict the response of airframes and the occupants to impacts encountered in crash conditions. The methods vary in concept, detail, and philosophy; but all approaches have as an end objective the provision of a tool by which the crashworthiness of aircraft can be improved. Since the airframe must properly dissipate the energy imposed by a crash impact, the ability to describe the energy absorption characteristics of the various parts comprising the airframe as well as their interaction is of prime importance. There are a number of programs for predicting the airframe response accurately in the elastic range backed by a great amount of test data. However, the energy in the elastic range of an airframe is minor when compared to the total energy to be absorbed in a crash. Consequently, the success of any methods that are intended to predict airframe response to a crash impact depends primarily on the ability to define the airframe response in the nonlinear range.

Ideally the nonlinear response could be analytically obtained by using a micro-finite element representation of the structure. However, several difficulties have to be overcome before such a representation can become practical such as: definition of the exact characteristics of the element (linear and nonlinear) and how they interface, management of the large amount of data that would be required, and proper handling of the expected large deflections (in the order of 10 times the dimensions of the elements). In addition, as a practical matter, experience with crushing of sheet/stringer types of built-up structures indicates that, although the total performance is repeatable, the detail response of the various parts of the structure will vary as a result of differences, within tolerance, encountered in manufacture. These difficulties with the micro-finite element representation which may be overcome in the future) and the need to provide guidance in selection of adequate crashworthy structural concepts early in the preliminary design stages of an airframe to minimize penalties, suggest that a simpler representation be employed.

Recent efforts, References 3 and 4, have shown that complete vehicle analysis for multidirectional crash conditions can be performed in a practical and cost-effective manner. The programs described in References 3 and 4 involved verification of analytical techniques with full-scale vehicle and substructure testing. The results of these programs and that of the FAA sponsored three-dimensional mathematical model of an aircraft seat, occupant, and restraint system (Reference 5) form the basis for the formulation of analytical methods for evaluating and upgrading the crashworthiness of general aviation airplanes.

The development of analytical methods to assess the crashworthiness capability of airplanes, while important, is not sufficient in itself to assure that general aviation airplanes will be crashworthy in the future. In addition, supporting procedures and rational crash design criteria are required. The development of methods for showing compliance with crashworthiness design criteria requires that particular consideration be given to the crash condition as it applies to different types of airplanes and to different operational requirements which affect the probable crash conditions. In Reference 1 it is stated that 72 percent of all general aviation operations are for commercial purposes (business, air taxi, commuter airlines), 23 percent involves personal transportation and proficiency flying, and 5 percent involves sport flying. Thus, using accident data in conjunction with usage data can provide some indication of the accident conditions that are most likely to produce the greatest amount of fatalities and injuries.

In general, the basic ingredients for a further step forward in improving the crashworthiness of future general aviation airplanes are available; however, refinements and verification of the analytical methods are needed along with formulation of the procedures needed to incorporate the techniques in the iterative design process.

1.2 PROGRAM OBJECTIVES

The objectives of the program are:

- o to develop a computerized mathematical simulation which can predict the dynamic response of general aviation airplanes when exposed to a crash environment,

- o to develop proposed design crash environment criteria for general aviation airplanes,
- o to identify and analyze preliminary design concepts to be used in formulating a potentially optimum crashworthy airframe design configuration for future consideration, and
- o to develop a user's manual for the mathematical simulation including supporting structural crashworthiness design guidelines.

To facilitate the achievement of the stated objectives, the study is performed in the following three technical tasks.

Task I - Development of a mathematical simulation

Task II - Verification of mathematical simulation with full-scale controlled crash test data

Task III - Development of proposed design crash environment criteria and the formulation of an optimum conceptual crashworthiness configuration

The goals for each of the major tasks are delineated as follows.

TASK I GOALS

- o Evaluate and summarize accident data to assist in developing computer modeling requirements, selection of test conditions for verification of a computer simulation and developing crash environment design criteria.
- o Identify general aviation airplane structural design features and the characteristics and crash conditions that the mathematical models must be capable of treating.
- o Evaluate current and future computer capability within the general aviation industry.
- o Modify, as needed, the capability of existing computer program KRASH to meet the requirements for modeling light fixed-wing propeller driven general aviation airplanes under crash conditions.
- o Develop a user's manual and supporting structural crashworthiness design guidelines to facilitate the application of program KRASH by industry members.

TASK II GOALS

- o Provide compatibility between the output of the computerized mathematical model developed in Task I and the input requirements of the mathematical model of an aircraft seat, occupant and restraint system (Reference 5).

- o Perform three full-scale controlled crash tests using fully instrumented single-engine high-wing airplanes representing both probable accident conditions and a potentially catastrophic impact condition.
- o Verify the crash analysis capability using controlled crash test data for single-engine high-wing airplanes (to be performed during the program) and available crash test data for a twin-engine low-wing airplane and a partial airframe structure.
- o Perform correlation studies using test and analytically derived data and refine the mathematical simulation, as required.

TASK III GOALS

- o Perform parametric variation studies to demonstrate the capability of the mathematical simulation to model a wide range of airplane configurations and crash conditions.
- o Develop proposed design crash environment criteria based on the results of Tasks I and II.
- o Formulate an optimum conceptual crashworthiness configuration taking into consideration the crash environment, current and future crash-worthy features, and the cost, weight, and performance trade-off penalties.

In this report only Task I related items are presented. Task II and Task III will be reported on at a later date.

SECTION 2

REVIEW AND EVALUATION OF GENERAL AVIATION AIRPLANE DESIGN CHARACTERISTICS

2.1 AIRPLANE CONFIGURATIONS

The development of a mathematical model which is capable of predicting the dynamic response of the structure and occupants for light fixed-wing airplanes during severe, yet survivable, accidents requires that consideration be given to those conditions that influence the manner in which the structure containing habitable space deforms and the forces that are imposed on the occupant from the response of the airplane structure and/or the occupant's motion relative to hardware that he may impact. Examples of airplane configuration design characteristics that potentially influence the load pulse imparted to the seat during a crash are:

- o location of the wing relative to the cabin and occupant position
- o location of engine, or engines, with respect to the cabin; wing mounted (high or low), forward or aft
- o type of landing gear; fixed or retractable

The loads imposed on the airframe and the occupants are a function of airplane usage, structural design, and location of major masses and attachments. Consequently, it is desirable to identify the various airplane configurations and associated characteristics in a manner which will lead to the development of mathematical modeling requirements and rational crash environment design criteria. The following types of airplane configurations represent a majority of the various configurations of airplane designs presently operating:

- a. single-engine, low-wing
- b. single-engine, high-wing
- c. twin-engine, low-wing

d. twin-engine, high-wing

There are a few variations within these categories, such as a tandem push/pull propellor driven airplane.

2.2 OPERATIONAL USAGE AND GENERAL STRUCTURAL DESIGN CHARACTERISTICS

A total of 61 general aviation basic airplane models, produced by the seven leading domestic manufacturers in the industry, were reviewed with regard to their operational usage and structural design characteristics. While not all inclusive, the data is representative of more than 95 percent of the general aviation airplanes currently in operation. Pertinent information such as: probable usage, approximate maximum cruise (75 percent power) and stall speed (flaps down), number of engines, wing position, type of structure and passenger accommodations is noted. The data is compiled from Reference 6 and discussions with industry airplane design personnel. The following airplane manufacturers and their respective models* are represented:

Piper:	PA-18, PA-23, PA-24, PA-25, PA-28, PA-31, PA-32, PA-34, PA-36, PA-39
Beech:	A24R, B24R, B19, C23, V35B, F33, G33, A36, E55, B55, Baron 58, A60, B60, B80, A50, C90, E90, B99
Cessna:	150, 172, 177, 180, 182, 185, 188, 206, 207, 210, 310, 337, 340, 401, 402, 414, 421
Bellanca:	Viking 300A, Champion 7ECA/7GCAA/7KCAB Citabria, 8GCBC, 8KCAB
Grumman-American:	AA-1B, AA-5, AA-5B, AgCat
Mooney:	Ranger (Mark 21), Chapparral (Super 21), Executive
Rockwell International:	112A, 500S, 685, 690, S2R

* Some models are no longer manufactured.

The categories of usage associated with general aviation airplanes are listed below along with the category general description.

- a. Agriculture: Application of chemicals or seeding crops involving low altitude maneuvering flight.
- b. Sport, aerobatic: Performance of sporting and aerobatic functions usually involving high maneuvering load factors.
- c. Training: Used for instructional purposes usually involving initial flight training. Some of the larger airplanes may be classified as trainers for instrument rating purposes which is not the usage that would lead to the accidents encountered in initial flight training operation.
- d. Business, executive: This category may overlap into several areas, such as transport, cargo, and in a few cases testing and developing equipment. These airplanes in some cases may operate out of uncontrolled airfields.
- e. Commuter, transport, air taxi: Used to carry people for commercial purposes in very short-range flights and may include operations from uncontrolled airfields.
- f. Cargo, freight: Hauling of freight or cargo which can include operations from uncontrolled airfields.
- g. Utility: This is a multipurpose usage. Generally, an airplane in this category is used in activities such as ranching, photographing, power and pipeline inspection, ambulance work, and support transportation which requires operating from unprepared airfields.
- h. Pleasure: Generally applicable to smaller economical airplanes used mainly for the purposes of flight proficiency and personal transportation.

Most of the airplanes, with the exception of agricultural airplanes, have multiple uses. Some airplane models have as many as three different usages. Of the 61 airplane models included in this evaluation, twenty (20) are twin-engine low-wing airplanes, twenty-four (24) are single-engine low-wing airplanes, including five* agricultural types, thirteen (13) are single-engine high-wing airplanes, and four** (4) are twin-engine high-wing airplanes. The usage of the airplanes, considering the number of engines, can

* One biplane is included.

** One has the engines mounted in tandem on the fuselage.

be seen by the following distribution. (Because some models are used for multiple purposes, the total number of usages exceeds the number of models included in the evaluation.)

<u>Usage</u>	<u>Number of Airplanes</u>	
	<u>Twin-Engine</u>	<u>Single-Engine</u>
Executive/Business	18	20
Training	3	11
Commuter	10	10
Aerobatics/Sport	-	11
Cargo/Freight	5	4
Utility	2	7
Agriculture	-	5

Table 1 presents a matrix of airplane configurations as a function of maximum takeoff weight and usage.

Table 2 identifies the general structural design characteristics of the major airframe regions such as the wing, fuselage, engine attachments, landing gear, and empennage associated with different categories of airplanes. (The categories shown in Table 2 are defined in Section 2.3.)

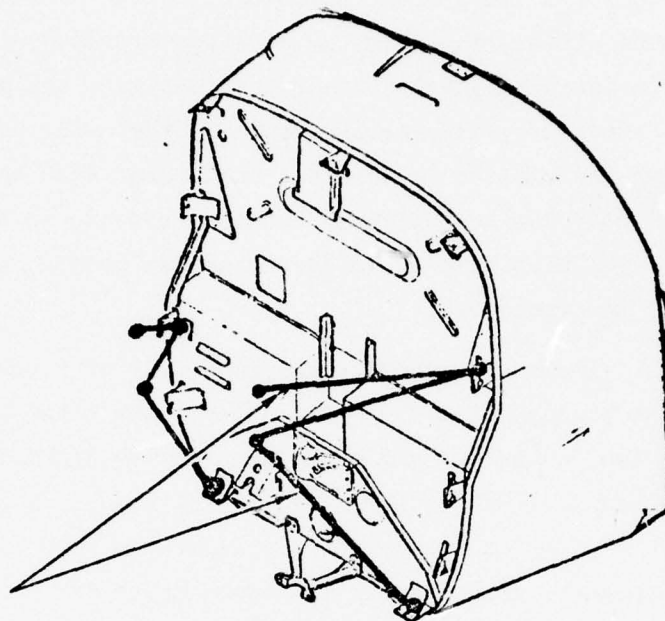
Engine mounts are generally either of a steel tube arrangement type or of a keel type. Figure 1 illustrates an arrangement for each of these two types. The structural characteristics for the two arrangements will differ; and, consequently, the modeling requirements will have to satisfactorily represent their behavior if a reasonably accurate assessment of the entire airframe response is to be performed. The failure of the tubular structure (Figure 1(a)) may likely be through dynamic instability which will occur at a load which is substantially below the yield stress. Wherein failure through elastic instability occurs, the load carrying capability of the structural element tends to decrease rapidly as deflection increases once the failure

TABLE 1. MATRIX OF AIRPLANE CONFIGURATIONS AND MAXIMUM TAKEOFF WEIGHT AND USAGE					
Maximum Takeoff Weight (lb)	Single-Engine Low-Wing	Single-Engine High-Wing	Twin-Engine Low-Wing	Twin-Engine High-Wing	
≤ 2000	Trainer Utility	Aerobatic Pleasure Trainer			
2000-2499	Trainer Sport Utility Pleasure	Trainer Business Aerobatic Utility Pleasure			
2500-3999	Business Agriculture Commuter Trainer Utility Pleasure	Business Utility Cargo/Freight Commuter Pleasure			
4000-5999	Agricultural (a)		Business Commuter Cargo	Business Commuter	
6000-7999			Business Commuter Cargo/Freight	Business Commuter Cargo/Freight	
8000-12500				Business Commuter	
(a) Consists of one low wing and one biplane					

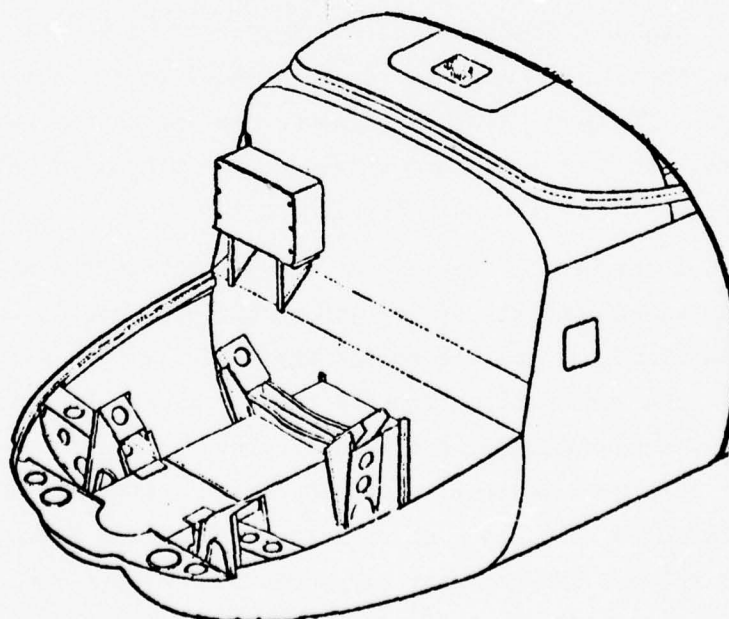
TABLE 2. STRUCTURAL DESIGN CHARACTERISTICS OF CURRENT GENERAL AVIATION AIRPLANES

Structure	Category 1 Single-Engine, Low or High-Wing, Weight < 2500 lb.	Category 2 Single-Engine, Low or High-Wing, Weight 2500-4000 lb.	Category 3, Single- Engine, Low-Wing, (a) Agricultural Use Only, Weight 2500-4000 lb.	Category 4 Twin-Engine, Low or High-Wing, Weight 4000-10900 lb.
Wing	<ul style="list-style-type: none"> o Braced Wing 1,2 or 3 spar, mostly metal, some wood spars o Cantilever 1,2 or 3 spar, mostly metal, some wood spars 	<ul style="list-style-type: none"> o Cantilever 1,2 or 3 spar mostly metal, some wood spars 	<ul style="list-style-type: none"> o Braced 1 or 2 spar metal construction 	<ul style="list-style-type: none"> o Cantilever 1,2 or 3 spar, mostly metal, some wood spars o One braced, all metal
Fuselage	<ul style="list-style-type: none"> o All-metal semi-monocoque o Rectangular section welded steel tube o Keel formed by floor and lower skin (cabin), semi-monocoque (rear) 	<ul style="list-style-type: none"> o All-metal semi-monocoque o Weld steel tube o Welded steel tube (cabin), semi-monocoque (rear) 	<ul style="list-style-type: none"> o Rectangular section welded steel tube o Welded steel tube (cabin), semi-monocoque (rear) o Long nose section o Isolated occupant region o Strong turnover structure 	<ul style="list-style-type: none"> o All-metal semi-monocoque
Engine Attachment	<ul style="list-style-type: none"> o Tubular 	<ul style="list-style-type: none"> o Tubular o Keel 	<ul style="list-style-type: none"> o Tubular 	<ul style="list-style-type: none"> o Tubular o Keel
Landing Gear	<ul style="list-style-type: none"> o Tail wheel o Tricycle o Cantilever spring main gears o Nonretractable 	<ul style="list-style-type: none"> o Tail wheel retractable o Tricycle retractable and nonretractable o Cantilever spring main gears o Hydraulically activated system 	<ul style="list-style-type: none"> o Tail wheel type o Nonretractable o Cantilever spring main gears 	<ul style="list-style-type: none"> o Mostly tricycle retractable o Some nonretractable with cantilever spring main gears o Hydraulic or electro-mechanical actuated system
Tail Unit	<ul style="list-style-type: none"> o Cantilever all-metal o Welded steel tube and channel with fabric covering 	<ul style="list-style-type: none"> o Cantilever all-metal 	<ul style="list-style-type: none"> o Welded steel tube o Cantilever all-metal 	<ul style="list-style-type: none"> o Cantilever all metal
(a) With the exception of one biplane				

ENGINE
SUPPORT
MOUNTS
(TYPICAL
BOTH SIDES)



(a) Tubular



(b) Keel

Figure 1. Two Typical Engine Mount Arrangements

load has been reached. The keel mount arrangement shown in Figure 1(b) can be expected to behave differently. The mount structure for this configuration can be considered to be an integral part of the fuselage, and as such the deformation of the structure will involve crushing that will absorb considerable energy during the plastic deformation associated with the post-failure region. The location of the two different mounts relative to the impact region and terrain will also have an influence on the loading that each of the structures will be exposed to.

The wings in all airplane categories are generally of a cantilever (with the exception of one biplane with flying wires and interplane struts) design with either a one, two, or three spar arrangement. The lighter weight airplanes usually have supporting brace struts for the wing. While most wings are all metal, some of the lighter weight airplanes use wood spars. The wings for the heavier airplanes, particularly the twin-engine airplanes (4,000 pounds and up) generally are unbraced and are of an all metal construction. The empennage for most airplanes is usually an all metal cantilever structure. The landing gear arrangement tends to be a function of weight, the light weight (<2500 pounds) airplane uses a tricycle or tailwheel nonretractable landing gear, wherein the main gears are usually of a cantilevered metal spring design. The agricultural airplanes use tailwheel type nonretractable landing gears, while the heavier single-engine airplanes (2500-4000 pounds) predominantly employ retractable tricycle gears.

Fuselage construction for most of the airplanes (the agricultural airplanes are an exception) are of semi-monocoque construction. A few of the single-engine airplanes and all of the agricultural type airplanes use a welded steel tube construction for the cabin region. In some instances a combination of semi-monocoque and welded tube construction is employed. The agricultural airplanes generally contain design features that are unique such as isolated cockpit, long nose section and strong turnover structure. In all the airplanes the occupant accommodation designs and arrangements vary widely and include individual seats, reclining seats, front and rear facing seats, bench seats, side facing seating, tandem seating, articulated seats, progressively collapsible seats, and a variety of lap belt and shoulder

harness arrangements. Details concerning material characteristics, typical structural components and examples of fastening methods used in the design and construction of general aviation airplanes are presented in Appendix B.

Table 3 presents a grouping of the general aviation airplanes as a function of configuration, maximum takeoff weight, stall speed, operating speed, usage and occupant capacity. Combining the data presented in Tables 1 through 3 provides the following general information on the three major airplane configurations.

a. Twin-engine low and high-wing airplanes

- o Maximum takeoff weight range is 3700 pounds to 10,900 pounds, with the majority of twin-engine low and high-wing airplanes weighing between 5300 and 8700 pounds and between 5700 and 9600 pounds, respectively..
- o Stall speed (landing configuration) range is 59 to 82 knots.
- o Cruise speed range (75 percent of max. power) is 162 to 280 knots.
- o Retractable tricycle gears are used.
- o Both tubular and keel type engine mounts are used.
- o A predominantly semi-monocoque fuselage structure is used.
- o Shoulder harnesses and design features which would reduce the potential for occupant injury from impact with structure (padding, no protrusions) are not incorporated as standard features.
- o Occupant capacity ranges from 4 to 11 (except B99 airliner).

b. Single-engine low and high-wing airplanes, except agricultural airplanes

- o Maximum takeoff weight range is 1560 to 3900 pounds.
- o Stall speed (landing configuration) range is 38 to 61 knots.
- o Maximum cruise speed (75 percent max. power) range is 100 to 176 knots.
- o Occupant capacity ranges from 2 to 6.
- o Both retractable and non-retractable type landing gears are used.
- o Wing construction is usually unbraced cantilever with two or three spars.

TABLE 3. RELATIONSHIP OF GENERAL AVIATION AIRPLANE CONFIGURATIONS TO PERFORMANCE PARAMETERS, USAGE AND OCCUPANT CAPACITY					
Airplane Configuration	Maximum Takeoff Weight (Pounds)	Stall Speed Range, Flap Down (Knots)	Cruise Speed Range, 75 Percent Max. Power (Knots)	Primary Usage	Occupant Capacity
Single-Engine Low-Wing	< 2500	49-54	108-128	Training Pleasure	1-4
Single-Engine High-Wing	< 2500	38-45	100-114	Training Pleasure Aerobatics	2-4
Single-Engine Low-Wing	2500-4000	49-61	132-176	Business Commuting Training Utility	4-7
Single-Engine High-Wing	2500-4000	45-59	124-163	Business Utility Cargo	4-7
Single-Engine Low-Wing (a)	2900-6000	47-59	101-138	Agriculture	1
Twin-Engine Low-Wing	3700-10900	59-82	162-247	Commuting Business Cargo Commuting	4-17 (b)
Twin-Engine High-Wing	4600-10250	61-77	170-280	Business Cargo Commuting	4-11
(a) Includes one biplane					
(b) 17 occupants for 1 airplane only, otherwise maximum is 11					

- o Fuselage structure is semi-monocoque design.
 - o Shoulder harnesses and design features which would reduce the potential for occupant injury from impact with structure (padding, no protrusions) are not generally incorporated as standard features.
- c. Single-engine agricultural airplanes
- o The maximum takeoff weight range is 2900 to 6000 pounds.
 - o The stall speed (landing configuration) range is 47 to 59 knots.
 - o The maximum cruise speed (75 percent max. power) range is 101 to 138 knots.
 - o Crashworthy design features such as overturn structure, shoulder harness, padded instrument panel, isolated cockpit and long nose structure are incorporated.
 - o The fuselage consists of a welded steel tube truss type of structure.
 - o Wing construction is generally braced cantilever design with the exception of one biplane.
 - o Landing gears are non-retractable tailwheel with cantilevered spring steel main gears.
 - o Single place cockpit.
 - o Payload carried forward of the pilot.
 - o A tubular engine mount support structure is used.

The design characteristics of the various categories of general aviation airplanes described herein indicate that there is a tendency for a particular manufacturer to generally use the same type of design features, including structure, because of past success, engineering cost considerations and ease of manufacture.

2.3 AIRPLANE CATEGORIES

The review and evaluation of the various airplane configurations discussed in Sections 2.1 and 2.2 indicate that there are several categories that can be established to facilitate the accident data evaluation, the development of mathematical modeling requirements and the development of crash environment design criteria. The crash environment depends primarily

on airplane usage and operating speeds while the modeling requirements, to ascertain the survivability of occupants during a crash, include consideration of not only the crash environment but also the airplane structural configuration. From Table 3 it can be seen that light single-engine airplanes (<2500 pounds) have similar usage and operational requirements, irrespective of the wing and engine configuration. This situation implies that they may be exposed to the same crash environment. How the airplanes respond to the crash environment can be influenced by the location and method of attachment of the major mass items (i.e. wing, engine). Similarly it can be expected that the heavier weight (2500-4000 pound) single-engine airplanes (except agricultural configurations) and the twin-engine airplanes, because of their differences in weight, operating speeds and usage, can each be exposed to their own particular crash environment, which is not a function of the wing and engine locations. (Agricultural airplanes, because of their unique mission, can be exposed to an entirely different crash environment than that of the other airplanes.) Consequently, the definition of the crash environment for general aviation airplanes can be obtained from as little as four categories, as shown in Table 4. On the other hand, the requirements for modeling the different airplanes and assessing current capability to protect occupants during a severe crash may indicate the need for additional categories. Thus subcategories (i.e. 1A, 1B, 2A, 2B, and 4A, 4B), shown in Table 4, are also established and used as noted in the following sections of this report.

TABLE 4. CATEGORIES FOR GENERAL AVIATION AIRPLANES

Category	Airplane Configuration	Maximum Takeoff Weight (Pounds)	Stall Speed Range Flap Down (Knots)	Cruise Speed Range 75 Percent Max. Power (Knots)	Primary Usage	Occupant Capacity
1	Single-Engine A. Low-Wing B. High-Wing	< 2500	38-54	100-128	Training Sport Aerobatic Pleasure	1-4
2	Single-Engine A. Low-Wing B. High-Wing	2500-4000	45-61	124-176	Business Utility Commuting Training	4-7
3	(a) Single-Engine Low-Wing	2900-6000	50-53	101-122	Agriculture	1
4	Twin-Engine A. Low-Wing B. High-Wing	> 4000-10900	59-82	162-280	Business Cargo Commuting	4-11 (b)
(a) Includes one biplane						
(b) Except for 1 airplane accommodates 17						

SECTION 3

REVIEW AND EVALUATION OF ACCIDENT DATA

3.1 SOURCES OF DATA

The primary sources for the accident data used in the study are:

- o FAA Civil Aeromedical Institute (CAMI), Oklahoma City, Oklahoma
- o The National Transportation Safety Board (NTSB), Washington, D.C.
- o General aviation accident investigation summaries and reports

The FAA Civil Aeromedical Institute is situated in Oklahoma City. Crash investigators from CAMI cover only a selected number of accidents that mostly occur in the states of Oklahoma, Texas and Arkansas. The records for each accident contain, when available, the airplane make and model identification, the flight condition under which the accident occurred (i.e. crop spraying maneuvers, loss of power, stall on turn, obstacle impact), impact angle, post crash behavior, stopping distance, structural damage, use and condition of seat belts and harness, number of occupants involved, occupant injuries/fatalities, and cause of injuries/fatalities. Some of the accident reports contain photographs of the airplanes in the post crash condition. Copies of 18 accident reports, obtained from CAMI, were reviewed and evaluated. The results of this effort are contained in Section 3.2 of this report.

The National Transportation Safety Board compiles records of accidents that have occurred throughout the nation. The data from these accidents are stored on tape by calendar year. While the tapes may be accessed such that a requester may solicit several sheets of data concerning each accident, much of the information needed to support this program does not appear as a regular part of the format. The Cessna Aircraft Company,

prior to developing the program described herein, developed a computer software program which utilizes portions of the accident data from the NTSB tapes. While the format of the Cessna accident software program provides useful information it was decided that in order to meet the objectives of this project the software program should be refined. The changes to the software program and the results of the NTSB data evaluation are presented in Section 3.3. Details of the software program (a copy of which has been submitted to the FAA) including a User's Manual and listing are presented in Appendix A.

In addition to the NTSB and CAMI data, several reports which provide summaries of accident data and/or descriptions of selected accidents were reviewed. The information obtained from these reports was included as part of the accident review and evaluation. In particular, the information contained in References 7, 8, 9, 10 and 11 was reviewed and the applicable data is integrated into the discussions contained in Sections 3.2 and 3.3.

3.2 CAMI DATA

At the initiation of this program, CAMI investigation reports (References 7 and 8) were reviewed. The latter reference contains a summary of 110 accident investigations and presents data describing the accident, identifying the airplane, on the location of the accident, on the accident type, concerning airplane damage, and data on occupant injury. The summary data provided in Reference 8 was used as a guide in the selection of the detailed accident cases that were obtained from CAMI. Photographs and case histories came from an on-site search of CAMI records. The criteria for selecting a CAMI recorded accident for detail review required that the particular accident report contain information regarding one or more of the following: flight path angle at impact; impact velocity; stopping distance; airplane pitch, roll or yaw angle at impact; and availability of photographs.

Data for the 18 accident cases selected from CAMI files for detail review, are presented in Table 5. Table 6 is a summary of the results

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI (f)

Accident Case		Accident Type	Maximum Takeoff Weight (lb)	Kinematics			Structural Damage		Cabin Accommodations					Occupant Injury Data (h)					Remarks	
1	2	3	4	Impact Angle (degrees)	Distance (feet)	Fuselage	Wings	Terrain Composition	Seat Failures	Lap Belt	Shoulder Harness	Fatal (a)	Critical (b)	Serious (c)	Moderate (d)	Minor/None (e)	Probable Area of Fatal Injury	Probable Area of Occupant Impact Post Crash		
1	Piper PA-25 NC1282	Single-Engine, Low-Wing		45	NA	1. Fwd nose strut crumpled. 2. Cock-pit bent.	1. Destroyed by tree	Hard Ground	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	1. Instr. Panel at windshield 2. Hopper 3. Rudder Pedal	No	No
2	Cessna C-140 N90045	Single-Engine, High-Wing		30	64	Fwd Nose Section		Hard Ground	NA	NA	NA	NA	NA	NA	NA	1C		1. Control wheel 2. Rudder Pedal 3. Lower Fuse-lage Structure	No	No
3	Cessna C-182B	Single-Engine, High-Wing		NA	NA	Fin torn off by wire		Water	NA	NA	NA	NA	NA	NA	NA	IP 1C		1. Instr. Panel		Asphyxiation

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI(2) (Cont'd)

Accident Case	Airplane Designation	Airplane Configuration	Maximum Takeoff Weight (lb)	Accident Type	Kinematics			Structural Damage		Cabin Accommodations										Occupant Injury Data (h)					Remarks
					Impact Angle (degrees)	Distance (feet)	Fuselage	Wings	Terrain Composition	Seat Failures	Lap Belt		Shoulder Harness		Fatal (a)	Critical (b)	Serious (c)	Moderate (d)	Minor/None (e)	Probable Area of Fatal Injury	Probable Area of Occupant Impact Post Crash				
											Used	Failed	Installed	Used								Failed			
																							Used	Failed	
4	Piper PA-24-250	Single-Engine, Low-Wing	2900	Struck Ground (Enroute)	0	305	Fuselage Broke Aft of Cabin		Mid	2* Yes	No	NA	NA	NA	NA			1P	1C			1. Inst. Panel	No	Two Passenger Seat Back	
5	Mooney M-20 N2570W	Single-Engine, Low-Wing		Hit Trees & Impact Ground (Forced Landing)	9	NA	Damaged by Trees	Grassy pasture		NA	NA	NA	NA	NA	NA	1P	1C			*		1. Inst. Panel	Yes	Fatality (En- gine in auto Comp) accident. Victim dead before crash.	
6	Piper PA-28 N0730J	Single-Engine, Low-Wing		Impact Ground (Enroute)	45	NA	Destroyed	Swamp Like		2 Yes	No	No	-	-	-	1C	1P					1. Inst. Panel	No		

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI(f) (Cont'd)

Accident Case	Airplane Designation	Airplane Configuration	Maximum Takeoff Weight (lb) (2)	Accident Type	Kinematics			Structural Damage		Cabin Accommodations					Occupant Injury Data (h)					Remarks			
					Impact Angle (degrees)	Distance (feet)	Fuelage	Wings	Terrain Composition	Seat Failures	Lap Belt			Shoulder Harness	Fatal (a)	Critical (b)	Serious (c)	Moderate (d)	Minor/None (e)		Probable Area of Fatal Injury	Probable Area of Occupant Impact	Post Crash
											Used	Failed	Installed										
7	Piper PA-22 N2642A	Single-Engine, High-Wing		Stalled (Takeoff)	< 10	159	Crumpled	Crumpled	Black Top Road	No	Yes	1*	NA	NA	NA	1C	3P			1. Severe Lacerations & Bruises (Upper Head & Torso)	1. Inst. Panel & Control Wheel	No	*Pilot Seat Belt Fitting Failed
8	Luscombe 8A N71153 1946	Single-Engine, High-Wing		Unstable Air Down Draft (Enroute)	20	NA	Wind-Shield Broken		River Bed	NA	Yes	No	NA	NA	NA		1C				1. Inst. Panel 2. Rudder Pedal	No	
9	Cessna C-150 N23177 68	Single-Engine, High-Wing	1600	Hit Tree (Enroute)	15	75	Tail Section Broke Off		Pasture	No	Yes	No	NA	NA	NA		1C 1P				Suspect Upper Cabin Structure	No	

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI (c) (Cont'd)

Accident Case	Airplane Designation	Airplane Configuration	Maximum Takeoff Weight (lb)	Accident Type	Kinematics			Structural Damage		Cabin Accommodations					Occupant Injury Data (h)					Remarks	
					Impact Angle (degrees)	Deceleration Distance (feet)	Fuelage	Wings	Terrain Composition	Seat Failures			Facial (a)			Critical (b)	Moderate (c)	Minor/None (d)	Probable Area of Fatal Injury (e)		Probable Area of Occupant Impact Post Crash
										Used	Failed	Installed	Used	Failed	Shoulder Harness						
10	Piper PA-22 N2955P	Single-Engine, High-Wing		Hit Turbulence from a Commercial jet taking off. Diving into ground (landing).	50	NA		L. Wing Torn Crumpled	Hard Soil	1* Yes	No	NA	NA	NA	1C 1P			1. Inst. Panel 2. Control Wheel 3. Rudder Bars	No	*Front Seat Pulled loose from track	
11	Beech C55 N4807J	Twin-Engine, Low-Wing		Impacted Ground in R.H. Turn (Enroute)	50	38		Destroyed	Grassy Field	2* Yes	1**	NA	NA	NA	1C 1P			High G Impact Occupants thrown from A/C	No	*One seat thrown 190', one seat thrown 267' **Belt buckle failed	
12	Piper PA-22 N8723C	Single-Engine, High-Wing		Hit Fence (attempted landing after engine failure in take-off)	12	48		Fuelage broken off of tail assy.	Hard Ground	NA	No	NA	NA	NA	1C 1P 3P			1. Inst. Panel 2. Control 3. Post	No		
				Considered Non-survivable																	

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI(r) (Cont'd)

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI(x) (cont'd)

Accident Case	Airplane Designation	Airplane Configuration	Maximum Takeoff Weight (lb)	Accident Type	Kinematics			Structural Damage		Cabin Accommodations						Occupant Injury Data (h)						Remarks																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
					Impact Angle (degrees)	Distance (feet)	Fuselage	Wings	Terrain Composition	Seat Failures				Fatal (a)		Critical (b)	Serious (c)	Moderate (d)	Minor/None (e)	Probable Area of Fatal Injury	Probable Area of Occupant Impact																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
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13	Ercoupe N2208H	Single-Engine, Low-Wing		Landed short in thick growth of trees (landing)	20	NA	1. Nose Gear L.E. Damaged 2. Lvr Fuse-lage Substantially shield	Woods	NA	NA	NA	NA	NA	NA	NA	1C				1. Inst. Panel 2. Wind-shield	No	No	1. Inst. Panel 2. Wind-shield	No																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI (p) (Cont'd)

Accident Case			Maximum Takeoff Weight (lb)		Accident Type		Kinematics			Structural Damage		Cabin Accommodations					Occupant Injury Data (h)						Remarks
Airplane Destination	Airplane Configuration				Impact Angle (degrees)	Distance (feet)	Fuelage	Wings	Terrain Composition	Seat Failures	Lap Belt	Shoulder Harness		Fatal (a)	Critical (b)	Serious (c)	Moderate (d)	Minor/None (e)	Probable Area of Fatal Injury	Probable Area of Occupant Injury	Fire Post Crash		
16 Piper PA-24 N6028P	Single-Engine, Low-Wing		Struck fence & dam, landed in farm pond. (power failure in takeoff)	45	NA	1. Main Gear & Nose Gear Separated. 2. Windshield broken.	NA	NA	Earth-Dam	1* 2**	No	NA	NA	NA	1C 2P					1. Head lacerations & bruises. Drowned. 2. Massive Head Injuries (No seat belts).	1. Head lacerations & bruises. Drowned. 2. Massive Head Injuries (No seat belts).	No	*L. aft leg of R. front seat broken. **Rear passengers did not use lap belt.
17 Mooney 20	Single-Engine, Low-Wing		Hit Tree during cruise	15	NA	Extensive		Farm Land	Yes	Yes	No	NA	NA	1C						Impact with Inst. Panel.			

TABLE 5. Description of Detailed Accident Cases Obtained From CAMI(r) (Cont'd)

Accident Case	Airplane Designation	Airplane Configuration	Maximum Takeoff Weight(lb) (g)	Accident Type	Kinematics			Structural Damage		Cabin Accommodations						Occupant Injury Data (h)						Remarks		
					Impact Angle (degrees)	Deceleration Distance (feet)	Fuelage	Wings	Terrain Composition	Seat Failures	Lap Belt			Shoulder Harness	Fatal (a)	Critical (b)	Serious (c)	Moderate (d)	Minor/None (e)	Probable Area of Fatal Injury	Probable Area of Occupant Impact		Post Crash	
											Used	Failed	Installed										Used	Failed
18 Mono-coupe 110 High-Wing N1230	Stalled, Impacted ground (engine failure in take-off. Attempted LH turn back to field. Stalled at 200' altitude)	60	NA	Crumpled	Crumpled	NA	Yes	Yes	1*	NA	NA	NA	1C*	1P					Skull & Extremity Fractures	1. Inst. Panel 2. Cabin Structures	No	*RH seat belt stitching failed.	*Death within 24 Hours	

(a) Fatal. Death within 24 hours.

(b) Critical. Lacerations, fractures and bruises with dangerous bleeding, concussion with unconsciousness longer than 30 minutes, depressed fractures of skull, dangerous intracranial damage, dangerous internal injuries, etc.

(c) Serious. Concussion with unconsciousness 5 to 30 minutes, comminuted fractures of nose, arms, legs, and back, loss of eye, internal injuries, etc.

(d) Moderate. Mild bone fractures, mild concussion with unconsciousness less than 5 minutes, "disfiguring" lacerations and bruises without severe hemorrhage, etc.

(e) Minor or None. Minor cuts, bruises, sprains, broken or loosened teeth, dislocated nose, etc.

(f) Data obtained from FAA AERONAUTICAL CENTER, CAMI, Oklahoma, Project No. 74-779-120A (O1545) May 1975

(g) Data is entered in this column only when such information was supplied in the CAMI Report.

(h) C denotes crew and P denotes passengers.

TABLE 6. RESULTS OF SELECTED CAMI ACCIDENT DATA

Frequency of Occurrence		Damage, Failures, Injuries	
<u>Phase of Operation</u>		<u>Cabin Damage</u>	
		Intact, None	4
(a) Takeoff	4	Minor, Moderate	8
Landing	4	Substantial, Destroyed	6
Cruise	8		
Aerial Application	2		
<u>Type of Accident</u>		<u>Structure Damage</u>	
		Intact, None	0
Stall	3	Minor, Moderate	7
Ground/Water Impact	5	Substantial, Destroyed	11
Contact w/tree/object	5		
Landing Short	1	<u>Impact with Control Panel/Knobs</u>	
Side of Hill	2	Yes	15
Miscellaneous	2	No	1
		Unknown	2
<u>Angle of Impact (degrees)</u>		<u>Seat Failures</u>	
		Yes	9
0-10	4	No	3
11-20	5	Unknown	6
21-30	1		
31-45	3	<u>Injuries (Total)</u>	
46-90	4	Fatalities	15
Unknown	1	Serious and/or Critical	15
		Moderate	6
<u>Roll/Yaw Attitude</u>		Minor, None	4
		<u>Lap Belt Failures (TOTAL)</u>	
Significant Roll/Yaw	3	Yes	6
Slight or No Roll/Yaw	9	No	27
Overturn	2	Unknown	7
Unknown	4		
<u>Terrain</u>			
Hard Soil	7		
Grassy Land	4		
Water	1		
Mud/Swamp	2		
Trees	1		
Mountainous/hilly	2		
Unknown	1		
(a) Generally impact occurs with tree, object, or ground, due to bad weather or stall.			

of the review of the 18 accident cases. Included in the summary are 9 single-engine high-wing airplanes, 8 single-engine low-wing airplanes and one twin-engine low-wing airplane.

An examination of Table 6 shows that for the 18 CAMI accident cases, 38 percent of the occupants died and another 38 percent of the occupants received serious or critical injuries. Seat failures occurred in 50 percent of the 18 accidents. In those accidents in which lap belts were used, lap belt failures occurred 15 percent of the time. A very significant statistic is that in 15 of 16 reported cases, impact of occupants with the instrument panel and/or control knobs occurred. In only two of the 18 accidents that were reviewed were the airplanes equipped with shoulder harnesses and only one person involved in these accidents used the harness. The occupant that used his harness suffered a minor injury while, in the same accident, the other occupant, who did not use his harness, was thrown through the windshield and received a severe injury. This distribution of accidents for the 18 selected cases by phase of operation and accident type is similar to the distribution noted in the NTSB data evaluation. The angle of impact is ≤ 45 degrees in 13 of 17 (77 percent) cases in which this information was reported. This impact angle data is consistent with the overall data presented in References 7 and 8, which show the impact angle to be ≤ 45 degrees in 20 of 28 accidents (71.4 percent) and 22 of 28 accidents (78.6 percent), respectively. The cabin damage assessment of the 18 cases shows moderate, minor or no cabin damage in 67.5 percent of the accidents where this information is reported. Reference 9 states that the cabin remains intact in 67.3 percent of the accidents. Substantial structural damage occurs in approximately 60 to 65 percent of the accidents.

The following discussion of the 18 accidents describes and illustrates typical crashes and the resultant damage to the structure and injury to the occupants. One of the prime concerns in reviewing accident data is to relate the critical structural regions for typical crashes to general aviation airplane mathematical modeling requirements.

Figure 2 shows the post crash condition of a single-engine low-wing agricultural airplane (case 1, Table 5). This particular airplane was reported to have stalled, while engaged in aerial application of insecticide, nosed over, and impacted hard soil at an approximate angle of 45 degrees. The pilot was wearing a helmet, shoulder harness and a 3-inch seat belt. The helmet penetrated the windshield and was torn off. The seat belt and shoulder harness broke in the webbing. The pilot was thrown straight forward and suffered moderate head and extremity injuries. In Figure 2 it can be seen that the tubular framework of the cockpit maintained its integrity, with regard to cabin volume. The impact energy was absorbed by the forward section of the fuselage as can be seen by the substantial damage forward of the cockpit.

Figure 3 shows the results of a single engine low wing airplane (case 4, Table 5) used primarily as a commuter. The accident report states that the airplane encountered bad weather and contacted the ground in a flat attitude and skidded 305 feet up and over a small hill. All the occupants were wearing seat belts and none of the belts failed. No shoulder harnesses were in the aircraft. One serious and three moderate injuries were sustained. The two front occupants impacted the upper and lower section of the instrument panel with their heads and extremities, respectively. All the seats stayed intact. In Figure 3 it can be seen that the forward fuselage, the cabin region and the rear fuselage did not undergo large deformations which is consistent with the kinetic energy absorbed in the post-impact slideout of 305 feet.

Figures 4 and 5 illustrate the post-crash condition of the instrument panel and airplane, respectively, of a single engine high wing airplane (case 10, Table 5). The airplane, with the pilot and one passenger on board, while landing at an airport, was caught in the turbulent wake of a commercial jet and crashed on the runway. No shoulder harnesses were in the aircraft. Both occupants, who were wearing seat belts, sustained severe injuries. The seats tore loose during the crash and the occupants impacted the instrument panel. The airplane which impacted the ground initially with its left wing sustained a crushed forward

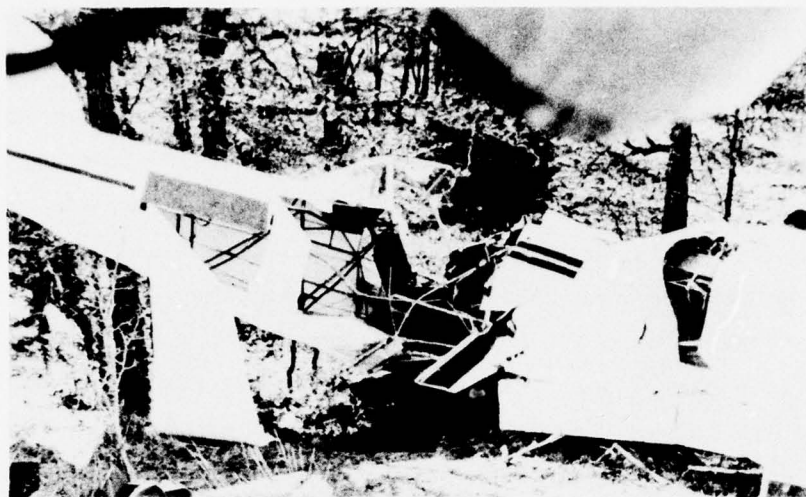


Figure 2. Side View of the Post Crash Condition of a Single-Engine Low-Wing Agricultural Airplane (Accident Case 1)



Figure 3. Side View of the Post Crash Condition of a Single-Engine Low-Wing Commuter Type Airplane (Accident Case 4)

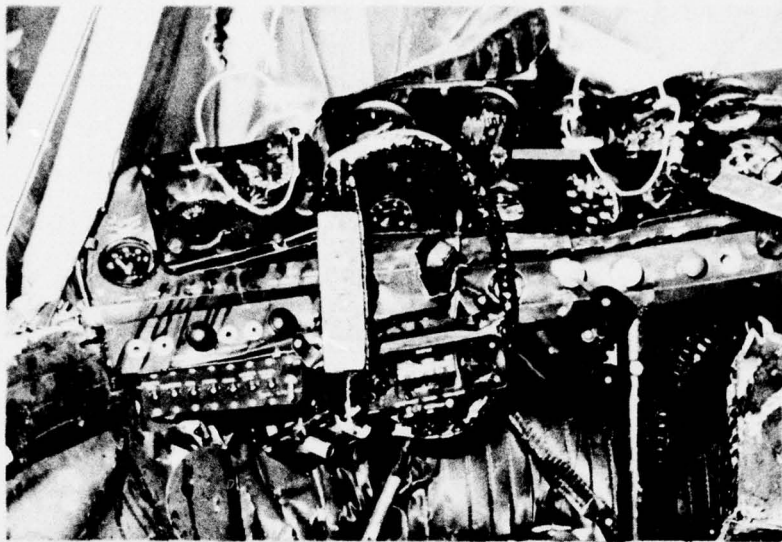


Figure 4. View Looking Forward of the Post Crash Condition of Instrument Panel (Accident Case 10)

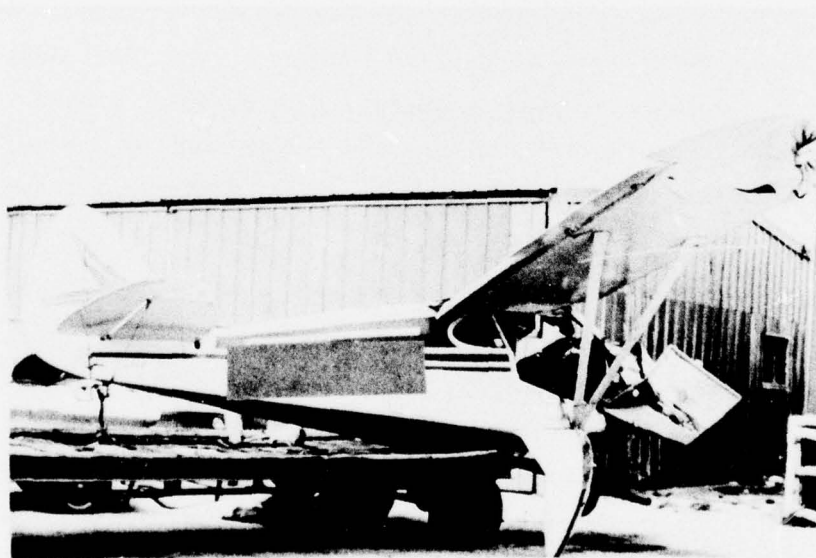


Figure 5. Side View of the Post Crash Condition of a Single-Engine High-Wing Airplane (Accident Case 10)

fuselage and crumpled left wing (not shown). However, as can be seen in Figure 5, the aircraft structure from approximately the location of wing brace attachments at the fuselage to the tail shows no significant external damage. The white head outlines in Figure 4 show where the heads of the occupants impacted the instrument panel.

Figures 6 and 7 depict the post crash condition of the structure and the cockpit, respectively, for a single-engine high-wing airplane (case 12, Table 5). The accident report states that the airplane, containing a pilot and four passengers, had just taken off and was approximately two miles from the airport when the engine started to miss. As the pilot returned to land, the engine stopped and the pilot made an emergency landing in a field. The left wing tip and landing gear struck the top strand of a four foot high fence. The airplane experienced two impacts. Seat belts were in use and they did not fail. No shoulder harnesses were installed. The occupants were thrown to the left and forward. The pilot suffered a severe injury, the co-pilot a moderate injury and the three passengers in the rear received minor or no injuries. Figure 7 shows the dent at the top of the instrument panel caused by the co-pilot's head on impact. The crushing sustained by the left wing and lower forward fuselage and the failure of the left main and nose gears can be seen in Figure 6. Most of the impact energy was absorbed by the lower forward fuselage.

Figures 8, 9, 10 and 11 show the post crash damage for several different accidents. Figure 8 shows the post crash damage to a single-engine low-wing airplane (case 5, Table 5) when the right wing first contacted muddy ground after the airplane hit the tops of small trees. Figure 8 shows that the damage to the airplane is primarily confined to the wing tips, engine and forward fuselage. For the most part, the cabin appears in good condition although the forward lower fuselage absorbed most of the impact energy. The airplane shown in Figure 8 does not look as if it sustained damage as a result of inverting, which the accident report indicates took place. The three occupants in the airplane experienced critical and fatal injuries. Figure 9 shows the post crash



Figure 6. Side View of the Post Crash Condition of a Single-Engine High-Wing Airplane (Accident Case 12)

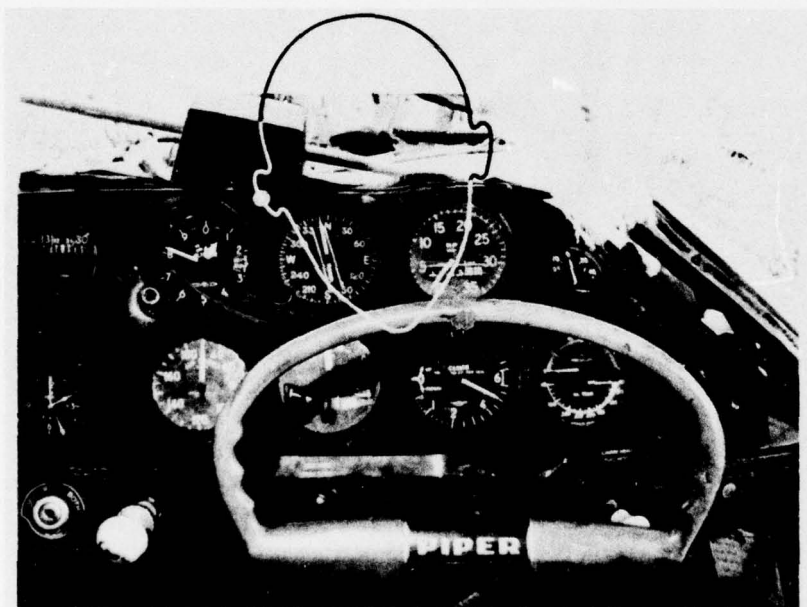


Figure 7. View Looking Forward of the Instrument Panel Impact Region (Accident Case 12)



Figure 8. Overall View of the Post Crash Condition of a Single-Engine Low-Wing Airplane (Accident Case 5)



Figure 9. Side View of the Post Crash Condition of a Single-Engine Low-Wing Airplane (Accident Case 11)

condition of a low-wing single engine airplane (case 11, Table 5) which landed short in a thick growth of trees. The airplane sustained forward fuselage and wing leading edge damage. All other visible structure appears to have escaped damage. The pilot, who was flying alone, experienced a severe injury as a result of impacting the instrument panel. Figure 10 shows the post crash condition of a single-engine high-wing airplane (case 14, Table 5). The airplane, containing a pilot (rear) and one passenger (front), crashed into the side of a hill while flying low on a hunting mission. Both occupants were fatalities. Although they were wearing seat belts, the pilot's seat belt failed at its attachment allowing the pilot to be thrown on top of and over the front seat passenger. Both occupants impacted the instrument panel. Structural damage to the forward fuselage, wing, landing gear and forward cabin region appears severe. Figure 11 shows the post crash condition of a single-engine low-wing airplane (case 16, Table 5). While on takeoff, the airplane with a pilot and two passengers failed to clear a fence. The nose gear and nose section struck an earthen dam, bounced over it and sank in the pond. (The photograph was taken after the airplane was removed from the pond). Occupants were thrown forward and to the left. All three occupants drowned. However, both front seat occupants received massive head injuries caused by impact with the instrument panel. The cabin remained intact. The interior and instrument panel (not shown) appeared in good condition after the crash.

The results of the evaluation of the selected CAMI accident cases are in general agreement with the overall conclusions in Reference 8 and 10. The CAMI data indicates that, while the cabin remains intact, occupants are still exposed to a high injury or fatality potential and it appears that improved crashworthiness can be obtained by providing restraint systems and airframe structural deformation characteristics that are consistent with the physiological capabilities of the occupants.



Figure 10. Side View of the Post Crash Condition of a
Single-Engine High-Wing Airplane (Accident Case 14)



Figure 11. Side View of the Post Crash Condition of a
Single-Engine Low-Wing Airplane (Accident Case 16)

3.3 NTSB DATA

A current Cessna software program, used to survey accident reports produced by the NTSB, is modified in accordance with the requirements of the program described in this report. The details of the software program including a User's Manual and listing are provided in Appendix A.

The program searches the NTSB accident tapes and summarizes all case histories which contain data concerning any of the following items.

- Impact Angle
- Impact Velocity
- Stopping Distance
- Seat Failure
- Seat Belt Failure
- Attitude at Impact

A summary of the NTSB accident tape data files is assembled by individual airplane models by manufacturer and a grand summary of all airplanes, irrespective of manufacturer or model, is also compiled. The individual accident cases and aircraft model summaries are screened to insure that no irrelevant accident data is retrieved from the NTSB tapes. The screening criteria is identical for the individual accident cases and the model summaries with departure from this norm occurring only in the summary print-out under the "Major Phases of Operation".

Initial screening is accomplished by selecting those accidents which involve airplanes produced by the following seven manufacturers:

- Beech Aircraft Corporation
- Bellanca Aircraft Corporation
- Cessna Aircraft Company
- Gruman American Aviation Corporation
- Mooney Aircraft Company

Piper Aircraft Corporation
Rockwell International Corporation

The models chosen from those of the above manufacturers are limited to a gross weight of less than 12,500 pounds (FAR 23) and are propeller driven. A secondary screening of the NTSB tapes is accomplished by selecting accidents of certain types which are identified in the NTSB accident data files. The following list identifies the types of accidents used in the search.

Ground Water Loop-Swerve
Stall
Wheels Up
Hard Landing
Nose Over/Down
Roll Over
Overshoot
Undershoot
Collision with Ground/Water
Collided with Obstacles
Dragged Wingtip, Float, or Pod*
Airframe Failure*
Engine Tearaway*
Engine Failure or Malfunction*
Propeller Failure*
Turbulence*

The above grouping of accidents is selected to delineate occurrences which would cover a majority of the hazards that might be encountered in general aviation operations. Also, the above list should include those accidents in which major airframe failure, loss of cabin crashworthiness capability or occupant injury may occur. Some of the types of accidents which are not included because they are not relevant to the study are; collision between aircraft, lightning strike, hail damage, bird strike, ditching and missing aircraft. The accident types listed above that are noted by an asterik are considered secondary data and are not necessarily related to impact conditions.

Tertiary screening of the NTSB tapes is accomplished by selecting "Phases of Operation" which are identified in five (5) major categories in the NTSB code classification manual. Three major phases of operation (takeoff, in-flight and landing) are used to screen the accident tapes for the summary and also the individual accident case print out. This technique is employed throughout the individual accident case retrieval. However, in the summaries under "Major Phases of Operation" two additional phases of operation (static and taxi) were selected for data retrieval and are printed out under the heading of "other".

The modifications to the Cessna program for handling accident data provide the following three types of printout.

- Concerning a Particular Airplane - The following data, if available from the accident reports, is provided: airplane identification number; accident date; airplane manufacturer; structural damage; nature of the flight; terrain; type of accident; phase of operation; cause/factor injury index; qualitative assessment of impact severity; estimated acceleration levels; severity of the damage; and data regarding stopping distance, direction of principal deceleration, seat belt failures, seat failures, use of shoulder harnesses and death due to fires, if information is available. A sample printout of a modified accident report, obtained from NTSB tapes, is shown in Figure 12.
- Concerning an Airplane Model by the Year - Derivatives of a model are combined (i.e. Cessna Model 150 includes 150, A150, A150K, etc.). Included in the summary are airplane manufacturer and model designation, date; (number of accidents and occupants involved, and number of accidents with fatalities and injuries), total number of injuries; flight conditions, accident types, impact conditions, airplane cabin occupant capacity and impact area (terrain).
- Concerning Accident Data for All Airplanes for a Given Period of Time - The format of the data is the same as that for the individual airplane summary. A sample of this output is shown in Figure 13.

The NTSB accident summary for 1971 through 1973 includes a survey of accidents. A total of 8,491 accidents are surveyed. Of this total 8,030 (95%) involved airplane models that are used to establish the different airplane categories presented in Table 3 (Section 2.2). Foreign manufactured airplanes that are final assembled or marketed by the major domestic

DATE	04/22/72
AIRCRAFT MAKE	AERO COMOR
AIRCRAFT MODEL	500-B
AIRCRAFT DAMAGE	DESTROYED
FIRE AFTER IMPACT	YES
KIND OF FLYING (GENERAL AVIATION)	PLEASURE/PERSONAL TRANSP
TYPE OF ACCIDENT, FIRST	COLLIDED WITH
TYPE OF ACCIDENT, FIRST	TREES
PHASE OF OPERATION, FIRST	LANDING
AIRPORT PROXIMITY	FINAL APPROACH
RUNWAY COMPOSITION	WITHIN 5 MILES
RUNWAY LENGTH	CONCRETE
TERRAIN (TYPE) OF AIRPORT	10000
	HILLY
CAUSE / FACTOR	IMPROPER IFR OPERATION
CAUSE / FACTOR	ATTEMPTED OPERATION W/KNOWN DEFICIENCIES IN EQUIPMENT
CAUSE / FACTOR	LACK OF FAMILIARITY WITH AIRCRAFT
CAUSE / FACTOR	LOW CEILING
CAUSE / FACTOR	RAIN
CAUSE / FACTOR	FOG
INJURY - INDEX	
PILOT	F S M N Z T
PASSENGERS	1 1
TOTAL ABORD	4 4
	5 5
REMARKS	ACFT RADIOS OPERATED INTERMITTENTLY WHILE ENROUTE
	E. DESCENDED 800 MDA ON ILS APCH. 1 HR DUAL IN TYPE
AIRCRAFT SERIAL NUMBER	00001384-138
RATE OF DECELERATION	EXCESSIVE
DIRECTION OF PRINCIPAL DECELERATION	FORWARD
STOPPING DISTANCE	85
DAMAGE SEVERITY - IMPACT (NCA-TRANS. AIRCRAFT)	EXTREME

Figure 12. Individual Airplane Output Format, NTSB Data

AIRCRAFT MANUFACTURER / MODEL - ALL	/ ALL
MAXIMUM TO WEIGHT -	POUNDS
WING CONFIGURATION	
NUMBER OF ENGINES / LOCATION -	
GENERAL INFORMATION	
TOTAL NUMBER OF ACCIDENTS SURVEYED	- - - - - 8491
TOTAL APPLICABLE ACCIDENTS SURVEYED	- - - - - 7471
TOTAL NUMBER OF OCCUPANTS	- - - - - 15609
AVERAGE NUMBER OF OCCUPANTS PER ACCIDENT	- - - - - 2
NUMBER OF ACCIDENTS WITH AT LEAST ONE (1) FATAL INJURY	- - 1217
NUMBER OF ACCIDENTS WITH AT LEAST ONE (1) SERIOUS INJURY AND NONE MORE SERIOUS	- 638
NUMBER OF ACCIDENTS WITH AT LEAST ONE (1) MINOR INJURY AND NONE MORE SERIOUS	- - 1032
NUMBER OF ACCIDENTS WITH NO INJURY AND NONE MORE SERIOUS	- - - - - 4589
***** TOTALS OF SERIOUSNESS OF INJURIES *****	
	FATAL SERIOUS MINOR NONE
PILOT	1134 584 956 4795
COPILLOT	81 21 15 91
PASSENGERS	1257 544 897 4767
* OTHER	48 40 47 310
* OTHER INCLUDES DUAL STUDENT & CHECK PILOT	
FLIGHT CONDITIONS -	

Figure 13. Grand Total Summary For 1971 through 1973

FLIGHT CONDITIONS -

TOTAL NUMBER OF ACCIDENTS WHICH OCCURRED DURING THE FOLLOWING FIVE MAJOR PHASES OF OPERATION /
NUMBER OF ACCIDENTS WITH AT LEAST ONE FATALITY WHICH OCCURRED DURING THE MAJOR PHASE

TAKEOFF - - 1355 / 113
IN FLIGHT - 2450 / 888
LANDING - - 3666 / 216
OTHER - - - 375 / 16
NOT REPORTED 11 / 6

NINE (9) MOST FREQUENT MINOR PHASES OF OPERATION WITHIN THE FIRST THREE MAJOR PHASES ABOVE
LISTED IN DESCENDING ORDER OF FREQUENCY

MINOR PHASE OF OPERATION	TOTAL NO. OF ACCIDENTS	***** INJURIES *****		
		FATAL	SERIOUS	MINOR
1. NORMAL CRUISE	477	411	200	366
2. INITIAL CLIMB	383	231	193	354
3. FINAL APPROACH	252	125	148	221
4. UNCONTROLLED DESCENT	249	511	25	14
5. LEVEL OFF/TOUCHDOWN	201	27	69	237
6. ROLL	106	3	16	120
7. TRAFFIC PATTERN-CIRCLING	101	67	59	71
8. GO-AROUND	98	46	52	84
9. OTHERS	590	503	269	309
				115

EIGHT (8) MOST FREQUENT TYPES OF ACCIDENTS WITHIN THE FIRST THREE MAJOR PHASES ABOVE
LISTED IN DESCENDING ORDER OF FREQUENCY

TYPE OF ACCIDENT	TOTAL NO. OF ACCIDENTS	***** INJURIES *****		
		FATAL	SERIOUS	MINOR
1. ENGINE FAILURE OR MALFUNCTION	719	289	318	743
2. COLLISION WITH GROUND/WATER	569	961	180	129
3. COLLIDED WITH	549	480	255	309
4. STALL	540	550	271	256
5. GROUND-WATER LOOP-SWERVE	119	1	23	141
6. OVERSHOOT	99	19	40	114
7. OTHERS	285	228	104	224
8. NOT REPORTED				115

NOTE -- OTHER IS SUM OF ALL ACCEPTABLE PHASES AND TYPES EXCEPT THOSE LISTED

Figure 13. Grand Total Summary For 1971 through 1973 (Continued)

IMPACT CONDITIONS

TOTAL NUMBER OF ACCIDENTS WHICH RECORD IMPACT ANGLES - 27

IMPACT ANGLE NUMERICAL SUMMARY -

AVERAGE ANGLE DEGREES	IMPACT ANGLE CATEGORIES - DEGREES					
	0-15	16-30	31-45	46-60	61-75	76-90
62	4	2	5	1	2	13
						98+

TOTAL NUMBER OF ACCIDENTS WHICH RECORD IMPACT VELOCITY - 2

IMPACT VELOCITY NUMERICAL SUMMARY -

AVERAGE VELOCITY KNOTS	IMPACT VELOCITY CATEGORIES - KNOTS			
	1-30	31-60	61-90	91-120
148			1	1
				120+

TOTAL NUMBER OF ACCIDENTS WHICH RECORD STOPPING DISTANCES - 499

STOPPING DISTANCE NUMERICAL SUMMARY -

AVERAGE STOPPING DISTANCE - FEET	STOPPING DISTANCE CATEGORIES - FEET						
	1-60	61-120	121-180	181-240	241-300	301-360	360+
194	174	87	73	48	38	17	62

OCCUPANT INJURY NUMERICAL SUMMARY AT RESPECTIVE AIRCRAFT DAMAGE SEVERITY INDICES -

DAMAGE SEVERITY	*** FATAL ***		*** OCCUPANT INJURY ***		*** NONE ***	
	FATAL	SERIOUS	MINOR	SEVERE	MODERATE	MINOR
EXTREME	1701	152	18	1		
SEVERE	96	59	14	4		
MODERATE	21	6	3	2		
MINOR	17	1	4			
NONE						5

Figure 13. Grand Total Summary For 1971 through 1973 (Continued)

AIRCRAFT CABIN ACCOMMODATIONS -

NUMBER OF ACCIDENTS IN WHICH SEAT FAILURE OCCURRED	- - -	149
TOTAL NUMBER OF SEAT FAILURES	- - - - -	328
NUMBER OF ACCIDENTS IN WHICH SEAT BELT FAILURE OCCURRED	-	204
TOTAL NUMBER OF SEAT BELT FAILURES	- - - - -	344
* NUMBER OF SHOULDER HARNESS USED	- - - - -	237
* NUMBER OF SHOULDER HARNESS FAILURES	- - - - -	21
* NUMBER OF CRASH HELMETS USED / NOT USED	- - - - -	442 / 68

* APPLICABLE TO AGRICULTURAL AIRCRAFT ONLY

IMPACT AREA

PERCENT OF ACCIDENTS WHICH OCCURRED IN PARTICULAR TERRAIN TYPE

TERRAIN TYPE

	PERCENT ACCIDENT OCCURRENCE (1)
--	---------------------------------------

UNKNOWN/NOT REPORTED

52

LEVEL, FLAT

19

ROLLING

8

MOUNTAINOUS

6

DENSE WITH TREES

4

HILLY

4

WATER-LAKES, RIVERS, ETC.

3

PLOWED

2

OTHER

1

CITY AREA

1

(1) PERCENT IS RATIO OF PARTICULAR TERRAIN TO NUMBER OF ACCIDENTS SCREENED

Figure 13. Grand Total Summary For 1971 through 1973 (Continued)

CAUSE / FACTOR GRAND SUMMARY

CAUSE / FACTOR SUMMARY	CAUSE	FATAL ACCIDENTS	NONFATAL ACCIDENTS
** PILOT **			
1. INADEQUATE PREFLIGHT PREPARATION AND/OR PLANNING		200	829
2. FAILED TO OBTAIN/MAINTAIN FLYING SPEED		304	630
3. FAILED TO MAINTAIN DIRECTIONAL CONTROL		3	740
4. IMPROPER LEVEL OFF		4	687
** COPILOT **			
1. IMPROPER LEVEL OFF			5
2. IMPROPER LEVEL OFF			4
** DUAL STUDENT **			
1. IMPROPER LEVEL OFF		8	25
2. IMPROPER LEVEL OFF			32
** CHECK PILOT **			
1. IMPROPER LEVEL OFF			7
2. IMPROPER LEVEL OFF			1
** AIRFRAME **			
1. BRAKING SYSTEM (NORMAL SYSTEM)			65
2. NORMAL RETRACTION/EXTENSION ASSEMBLY			59
** MISCELLANEOUS ACTS, CONDITIONS **			
1. OVERLOAD FAILURE		52	1067
2. FUEL EXHAUSTION		27	370
3. FUEL STARVATION		24	264
4. MATERIAL FAILURE		13	262

Figure 13. Grand Total Summary For 1971 through 1973 (Continued)

manufacturers are included in the final summary but not in the development of airplane categories. This accounts for the difference between 8491 accidents and 8030 accidents. The data is reviewed with regard to the potential for an occupant fatality to occur (for accidents in which at least one injury is reported), the distribution of accidents by terrain conditions, the total number of occupants involved, the total number of fatalities, and the total number of accidents. To facilitate the evaluation, two ratios are established. The first ratio (Ratio No. 1) is for all accident types and relates the total number of fatalities to total number of occupants involved in all accidents. This ratio is defined below as:

$$\text{Ratio No. 1} = \frac{\text{total number of fatalities}}{\text{total number of occupants}} \text{ (all accidents)}$$

The second ratio (Ratio No. 2) defines the number of fatalities relative to the number of occupants involved for a particular accident type. This ratio is established for accident types such as the stall, collision with ground/water and collision with obstacle.

$$\text{Ratio No. 2} = \frac{\text{number of fatalities}}{\text{number of occupants}} \text{ (for a particular accident type)}$$

involving an injury

Obviously, larger airplanes, which carry more passengers, will have a higher ratio of fatalities to accidents than the smaller airplanes. In dividing by the number of occupants involved for each particular accident type a more rational manner of comparing different size and weight airplanes on an equal basis can be utilized.

Both ratios are intended to give an indication of the occupant's chance for a fatal injury potential in each category of airplane as well as in all the airplanes combined.

Table 7 presents a summary of the accident distribution for general aviation airplanes in accordance with the terrain configuration. The summary is based on a sampling of airplanes for the three airplane categories (categories 1, 2 and 4 of Table 4) for which the majority of accident data

TABLE 7. SUMMARY OF TERRAIN CONFIGURATIONS FOR ACCIDENTS (NTSB DATA 1971 THROUGH 1973)

Type Terrain	All Airplanes		Single-Engine, High-Wing (a)		Single-Engine Low-Wing (b)		Twin-Engine Low-Wing (c)	
	Number of Accidents	Percent	Number of Accidents	Percent	Number of Accidents	Percent	Number of Accidents	Percent
Level, Flat	1,444	46.0	339	40.9	175	37.0	43	36.1
Rolling	676	21.6	186	22.5	193	26.0	22	18.5
Mountainous	422	13.5	146	17.6	92	19.4	19	16.0
Hilly	253	8.1	91	11.0	53	11.2	13	10.9
Dense with Trees	253	8.1	67	8.0	30	6.4	15	12.6
City	84	2.7	--	--	--	--	7	5.9
	3,132	100	829	100	473	100	119	100
(a) Based on Category 1B Type Airplanes, 2-4 Occupants, Sport, Trainer, Pleasure, and Business Usage.								
(b) Based on Category 2A Type Airplanes, 2-6 Occupants, Sport, Trainer, and Business Usage.								
(c) Based on Category 4 Type Airplanes, 4-10 Occupants, Executive, Commuter, and Cargo Usage.								

is available. Although the number of accidents per terrain configuration varies somewhat for the different airplane categories, each category of airplanes has about the same percent of accidents per terrain configuration. Single-engine airplanes have accidents in rolling, mountainous and hilly terrains, somewhat more often, percentage-wise, than do the twin-engine airplanes. The reason may be associated with the fact that engine failure in a twin-engine airplane does not mean that a landing needs to be made immediately.

Table 8 provides a summary of the accident data using the different categories of accidents, the accident data pertinent to the models within each of the categories and the two ratios described earlier. Ratio No. 1 will identify the more crashworthy categories of airplanes, whether it be due to the structural design or the crash environment, to be those with lower ratios than that of the composite of all airplanes. On this basis the smaller lighter weight airplanes and the agricultural airplanes appear to be more crashworthy than the other airplanes.

The data presented in Table 8 indicates that the most probable accident for the lighter weight airplanes (<2500 pounds) is a stall condition. The most fatal accidents for heavier weight airplanes (>2500 pounds) are associated with collisions with ground or water. This particular type of accident can be either controlled or uncontrolled in nature. The NTSB information does not provide sufficient data with which to delineate between the two situations. Miscellaneous accident types, such as a hard landing, undershoot, overshoot, ground swerve, generally do not result in fatalities. The 1971 through 1973 NTSB data indicates that less than 5 percent of the occupants involved in these types of accidents received fatal injuries. This value is extremely low by comparison to the overall average of 45.5, 70.7, and 39 percent, respectively, for all categories of airplanes involved in the three major accident types shown in Table 8.

From the data shown in Table 8, of the three major accident types, the most survivable appears to be an accident which is initiated by contact with some obstacle. One possible reason for this is that this type of

TABLE 8. SUMMARY OF ACCIDENT DATA EVALUATION (NTSE DATA 1971 THROUGH 1973)

Category (a)	Number of Accidents Surveyed	Ratio (b) No. 1	Ratio No. 2 (c)			Order of Occurrence of Accident Type (Percent Distribution (d))		
			Stall	Collision with Ground	Collision with Obstacle	Stall	Collision with Ground	Collision with Obstacle
1 (<2500)	4502	.122	.439	.652	.326	1(37.5)	3(29.2)	2(33.3)
2 (>2500)	2245	.149	.408	.625	.346	3(22.3)	1(49.1)	2(28.6)
3 (Agriculture)	601	.081	.300	.222	.273	2(39.0)	3(6.5)	1(54.5)
4 (2 Engines)	682	.283	.728	.788	.695	3(21.3)	1(44.3)	2(34.4)
All Categories	8030	.147	.455	.707	.390	3(32.5)	2(33.6)	1(33.9)

(a) See Table 4 for Complete Definition of Categories.

(b) Ratio No. 1 = (Total Number of Fatalities/Total Number of Occupants) All Accidents

(c) Ratio No. 2 = (Number of Fatalities/Number of Occupants) For a Particular Accident Type Involving an Injury and/or Fatality

(d) Accident Types Involving an Injury. Percentage distribution is for the three types shown. Applicable to the Ratio No. 2.

accident occurs close to the ground at reduced airplane operating speeds (i.e. landing, approaches and takeoffs) and the impact angle usually is flat. The least chance of occupant survival occurs in collisions with the ground. With the exception of agricultural airplanes, at least 62 percent of the occupants that are involved in this type of accident sustain a fatal injury. While collisions with the ground represent a wide range of accidents (e.g. forced landings, bad weather, misjudged altitude and/or clearance), most of the accidents generally occur at speeds approaching that of cruise.

The agriculture airplanes (Category 3) which have a takeoff weight comparable to that of the single-engine airplanes used primarily for business, utility, commuter and cargo purposes (Category 2), demonstrate considerably more crashworthiness capability for all the three major accident types. Factors that most likely account for this difference are:

- Agricultural airplanes are designed with specific crashworthy features (overturn pylon, long fuselage, harness, isolated cockpit) that are compatible with their mission.
- Agriculture airplanes may crash under more controlled conditions, usually after hitting some obstacle.
- The pilots of agricultural airplanes generally are more experienced in emergency conditions than the average general aviation pilot.

While the agricultural airplanes provide a greater chance of occupant survivability during a crash, the pilot will sustain a fatal injury in about 30 percent of the accidents in which injuries occur.

The data presented in Table 8 indicates that benefits due to improvements in crashworthiness design for the twin-engine airplanes may provide the biggest payoff in reducing the degree of severe or fatal injuries that are sustained relative to the number of people involved. However, on an absolute basis there have been substantially more fatalities in single-engine airplane accidents than in twin-engine airplanes because there are substantially more single-engine airplanes in operation. Therefore, from a life saving point of view, if a priority is to be assigned, emphasis should be placed on upgrading the crashworthiness characteristics of

single engine airplanes.

Table 9 sets forth the accident data for the categories wherein a distinction is made between a low-wing configuration and a high-wing configuration and indicates that:

- o With the exception of the comparisons between high-wing and low-wing configurations for both light airplanes (< 2500 pounds) and two-engine airplanes in accidents involving collision with obstacles, the deviation from the mean value does not exceed ± 8.5 percent for all accident types and airplane categories noted in Table 9. This trend indicates that for the airplane and accidents considered and the period of time covered (1971-73) the location of the wing, for a particular category of airplane, is not very significant with regard to fatality potential in injury incurred accidents.
- o The low-wing, single-engine airplane experiences approximately the same rate of fatalities in accidents involving stall as do the high-wing, single-engine configurations. The data for the lower weight (< 2500 pounds) airplane indicate a slightly higher fatality rate for the high wing airplane (45.7 versus 38.6 percent). This trend is reversed for the higher weight (2500-4000 pound) category (38.5 percent versus 43 percent).
- o The lower weight (< 2500 pounds) low-wing, single-engine airplanes experience approximately the same rate of fatalities in accidents involving collision with ground/water as do the high-wing, single engine airplanes (66.3 versus 64.5 percent). For the heavier weight (2500 to 4000 pounds) single-engine airplanes, the fatality rate for the ground/water type of accident is slightly in favor of high-wing configurations (67.4 versus 56.8 percent).
- o The heavier weight (2500 to 4000 pounds) low-wing, single-engine airplanes experience approximately the same rate of fatalities in collision with obstacle type accidents as compared to the high-wing configuration (35.3 versus 34.2 percent). The lower weight (< 2500 pounds) low-wing, single-engine airplanes exhibit higher rates of fatalities for this type of accident when compared to the high-wing configuration (38.3 versus 28.3 percent). However, a closer examination of the lower weight category shows that for airplanes weighing between 2000 and 2500 pounds the rate of fatality for this type of accident is relatively close (38.9 for the low-wing configuration and 32.5 percent for the high-wing configuration). The rate of fatalities for the extremely light-weight airplanes (< 2000 pounds) for this type of accident is 27 percent for the low-wing configuration and 24.4 percent for the high-wing configuration. The low fatality rate for these light-weight airplanes may

TABLE 9. SUMMARY OF ACCIDENT DATA FATALITIES TO OCCUPANTS INVOLVED BY SUBCATEGORIES AND ACCIDENT TYPES (NTSB DATA 1971 THROUGH 1973)								
Subcategory (a)	Number of Accidents Surveyed	Ratio No. 2 (b), Percent			Deviation from Mean Average Value of Ratio No. 2 (c) for Category (Percent)			Collision with Obstacle
		Stall	Collision with Ground	Collision with Obstacle	Stall	Collision with Ground	Collision with Obstacle	
1A Low-Wing	1595	38.6	66.3	38.3	±8.5	±1.1	±15	
1B High-Wing	2907	45.7	64.5	28.3				
2A Low-Wing	933	43.	56.8	35.3	±5.4	±8.5	± 1.4	
2B High-Wing	1312	38.5	67.4	34.2				
4A Low-Wing	583	74.3	78.3	66.1	±2.6	±1.5	±11.5	
4B High-Wing	99	70.4	80.8	83.3				
(a) See Table 4 for definition of subcategories								
(b) Ratio No. 2 = (Number of fatalities/number of occupants) (for a particular accident type involving an injury and/or a fatality)								
(c) Based on average of low and high-wing ratio values for each type of accident								

be attributed to the lower impact speeds of these airplanes as a result of their lower flight speeds. The fatality rate associated with the agricultural airplane for this type of accident is 27.3 percent (Table 8). Since there are very few low-wing airplanes weighing less than 2000 pounds in the accident data as compared to 2000 to 2500 pound low-wing airplanes, the 38.9 percent shown in Table 9 is due to the fact that the weighted value is based on relative number of accident cases included.

- o The comparison of the number of fatalities by accident types for twin-engine high-wing and low-wing airplanes is generally within ± 3 percent of their mean average except for the case of impact with an obstacle. However, the sample of this type accident in the data bank for the twin-engine high-wing airplane is inadequate for a true comparison.

Ratio No. 2 (Table 8) is used in an effort to provide a level of severity of an accident by only including accidents in which injuries occur. (Accordingly, the data does not indicate the chances of survival in accidents which do not involve injuries). This ratio indicates that "collision with the ground" consistently results, except for the agricultural airplanes, in a high fatality rate. The impact velocities associated with this type of accident are higher and will require the absorption of a greater amount of energy than that of the stall and the obstacle collision types of accidents. Although it may not be practical from weight and cost effectiveness considerations to provide crashworthiness capabilities to fully cover this type of accident, the use of a consistent crashworthy design philosophy in the design of a new airplane should provide a reduction in potential fatalities.

The results of the CAMI and NTSB data review and evaluation indicates that work should be performed to evaluate the effectiveness of incorporating shoulder harnesses along with seat and safety belt installations that are consistent with the present structural crashworthiness capabilities of each of the general aviation airplane models now in operation.

SECTION 4.

MATHEMATICAL MODEL REQUIREMENTS

4.1 GENERAL AVIATION INDUSTRY COMPUTER CAPABILITIES

Seven members of the General Aviation Manufacturers Association (GAMA) were sent an inquiry regarding their current and anticipated computer capabilities. Included in the inquiry was a data sheet soliciting information regarding:

- o computer manufacturer and model number
- o core storage
- o peripherals (tapes, discs, drums)
- o systems (operating, plotting, interactive, Fortran levels)

The information was solicited from the manufacturers for the purpose of evaluating the capability of the general aviation industry to use program KRASH, modified as noted in Section 4.4, identify the types of changes that may be required in the program before it is distributed to the industry, and identify the equipment (or arrangements) required of the industry members in order to utilize KRASH to its fullest capability.

Based on the responses received from the manufacturers, the results of the survey indicate the following:

- o Access to a computer with 500,000 bytes or more is, or will shortly be available for six of the companies.
- o Four of the companies noted that they have 7 or 9 track tapes available for physical storage of data. However, KRASH, as presently coded, uses tapes only for plotting.

- o Four of the companies stated that they have discs comparable to the TELEX 6330 model used by KRASH. The discs are an internal means of managing data.
- o None of the companies have drums as part of their peripheral equipment. However, since the use of drums only increases the rate at which data is transferred, the only effect on the program will be in the area of computer run time.
- o The companies have different operating systems (mostly disc operating virtual systems) than the type of system that KRASH operates on (IBM 360 Multiprogramming with a Variable number of Tasks, MVT). The operating system is internal and only reflects the manner in which the computer jobs are managed, based on peripheral usage, allocation of core, and priorities.
- o Only one company has plotting capability.
- o Only one company has interactive capability.
- o All the companies use basic Fortran IV (F,G,H, levels)

Program KRASH currently requires 490,000 bytes of core. The program is written in basic Fortran IV, level H. It is compatible with the larger computers (CDC, IBM 360, 370), taking into consideration the normal adjustments in adapting to different operating systems. The general aviation industry is equipped to use program KRASH, as is, with the exception of the plot routine. The plot routine is most valuable in the presentation of data. Generally, unless operating in the interactive mode, the plots may not be available to the designer until a couple of days after the computer print-out is received, reviewed and input data changed. Currently, the plotting routine used in KRASH is stored in core and requires approximately 20 percent of the 490,000 bytes. Deletion of the current plot routine for the general aviation industry will allow for the following two alternatives.

- o Reduction in core size and, therefore, a higher run priority leading to faster turn-around time.
- o Maintain the same core size and enlarge the capability to treat larger math models (masses, members), or provide additional features at a future date.

Even if the current in-core plotting routine is replaced with an out-of-core plotting routine, the problem still remains that the industry does not currently, nor plans in the near future, to have plotting capability.

The major considerations for the industry with regard to using KRASH are: (1) whether to perform analysis using in-house computer facilities or to utilize a time sharing computer, (2) to use KRASH with its maximum capability (core size, plotting), which could involve additional capital investment, or to use a limited version of the program (smaller, no plotting)

4.2 GENERAL AVIATION AIRPLANE CRASH ANALYSIS REQUIREMENTS

The review and evaluation of general aviation airplane configurations, usages, operational and structural design characteristics, accidents, industry design practices and industry computer capabilities, indicates that the use of a computerized analytical technique for performing crash analysis would be an asset to the industry if it contained certain features. The development of a general aviation airplane industry crash analysis computer program must take into consideration the need to analyze reasonably complex crash conditions, yet not impose unrealistic and costly investments in specialized manpower and/or equipment to facilitate improved future crashworthy designs.

Ideally, the computer program should have the capability to:

- o Provide sufficient information which can be used to assess an occupant's chances for survival. As a minimum this information should consist of defining floor acceleration pulses and evaluating cabin damage and cabin geometry change.
- o Define forces, accelerations, velocities and displacements in three directions.
- o Treat multidirectional impact forces, angles and angular rates representative of the probable crash conditions associated with the different airplane usages and operational characteristics.
- o Represent various types of structural behavior for a wide range of structural element types, particularly wherein post-failure large deflections occur.

- o Treat structural failures and the consequences of the failures on surrounding structure.
- o Represent different airplane configurations such as high-wing, low-wing, single-engine, twin-engine, tandem engines, individual and multiple seating accommodations, weights up to at least 12500 pounds, and retracted or extended landing gear.
- o Provide the means to treat differences in terrain (level, hilly, water, dirt, concrete) using available data for describing the properties of the terrain.
- o Treat the significant phases of multiple impact crashes wherein the effect of an initial impact is accounted for in subsequent impacts during the same crash.
- o Utilize crash input acceleration magnitude, shape, duration and direction information as an input to the airplane, if available.
- o Provide data as part of the analysis which can be used to assess energy flow, member stresses, and structure rupture.
- o Facilitate usage and understanding of standard values, English symbols and simplified input requirements.

Furthermore, the program should be written in Fortran IV and be applicable for use on the larger size computers (i.e. IBM 360, IBM 370, CDC 6600) having at least 375,000 bytes of core storage. Plotting capability, while a potentially useful tool, can be dispensed with for the present. A plot routine should be compatible with the particular user's system, otherwise, unless all user's have "like" systems the plot routine will be superfluous.

While the description of the computer program's requirements is comprehensive, its usefulness will be inhibited unless the program is accompanied by appropriate documentation. As a minimum the documentation should consist of a User's Manual describing the theory, input-output requirements, a sample illustrative problem, techniques for representing structure, instructions on how to utilize specialized features, program limitations, and structural design guidelines.

4.3 PROGRAM KRASH

Program KRASH was developed for the purpose of providing a practical engineering analytical approach to determine the crashworthiness capabilities

of vehicles.

The digital computer program KRASH predicts the response of vehicles to multidirectional crash environments. The program computes the time histories of N interconnected masses. Each mass is allowed six degrees of freedom defined by inertial coordinates x_i , y_i , z_i , and Eulerian angles ϕ_i , θ_i , ψ_i , where $i = 1, 2 \dots N$. Euler's equations of motion are written for each mass. The equations of motion are integrated numerically to obtain velocities, displacements and rotations. Gravity forces, internal forces and moments, and external forces are computed. For small deflections a linear analysis is followed, and for large deflections general plastic deformation is allowed. The program provides for unloading and subsequent reloading along a linear elastic line.

A succinct description of program KRASH and the techniques it applies are presented in Reference 14, along with the experimental data obtained during a fully instrumented, full scale vehicle drop test with which the capability of the program was successfully verified. The essential features of program KRASH are:

- (a) The program is designed to provide sufficiently accurate data from which an assessment can be made of the occupant's chances of survival in a crash environment.
- (b) The formulation takes into consideration that the load-deflection behavior of a structure can be approximated using good engineering judgement so as to provide sufficiently accurate responses for the intended use.
- (c) The analysis is premised on the fact that only a portion of the major structural elements (and these can be readily identified) need be modeled in the post-failure region.
- (d) The program employs stiffness reduction factors (KR's) which are a method by which the linear stiffness of each structural element can be modified to treat nonlinear behavior.

Program KRASH's formulation is consistent with the amount and quality of detailed data that is available during a preliminary design study. Furthermore, analyses during preliminary design studies can serve to:

- o ascertain critical design regions wherein alterations to the structural response will be most beneficial,
- o determine the extent to which additional energy absorption is needed, and
- o determine the structural element load-deflection characteristics and, consequently, structural design and size requirements that are needed to meet a specified or desired crashworthiness capability.

Prior to the initiation of the study, program KRASH had the capability to:

- o Define a six-degree-of-freedom (DOF) response at each representative location, including three translations and three rotations (accelerations, velocities, and displacements are computed).
- o Determine mass accelerations, velocities and displacements, and internal member loads and deformations at each time interval.
- o Provide for general nonlinear stiffness properties in the plastic regime, including different types of load-limiting devices, and determine the amount of permanent deformation.
- o Determine how and when rupture of an element takes place and redistribute its load-carrying capability over the other structural elements involved.
- o Define mass penetration into an occupiable volume.
- o Provide for ground contact by external structure including sliding friction.
- o Include viscous damped internal elements.
- o Include a measure of injury potential to the occupants; for instance, the probability of spinal injury indicated by the Dynamic Response Index (DRI).
- o Determine the distribution of kinetic and potential energy by mass item, the distribution of strain and damping energy by element, and the crushing energy associated with each external spring.
- o Determine the vehicle response to an initial condition that includes linear and angular velocity about three axes and any arbitrary vehicle attitude.

- o Treat up to 80 masses (480 DOF), 100 internal (6 x 6) beam elements and provide plots of the responses.

A comprehensive description of KRASH prior to this program is presented in References 3 and 4. Changes to KRASH related to this program are described in Section 4.4. A complete description of KRASH updated for the general aviation airplane industry is presented in the User's Manual and Structural Design Guide (Reference 13).

4.4 MODIFICATIONS TO KRASH

The requirements of a computer program to meet the needs of the general aviation industry were evaluated both with regard to KRASH's capability, as developed previously, as well as to the modifications that could be incorporated to extend the program's capability and yet be consistent with the philosophy under which KRASH was developed, which is to be a practical preliminary design tool. Program KRASH, as originally developed, meets many of the requirements necessary to perform crash analysis of general aviation airplanes. To comply with the overall requirements and to facilitate KRASH's usage by the industry, several modifications are incorporated. Since a comprehensive discussion of each modification is contained in Section 1 of the User's Manual (Reference 13) a brief description of each is presented in the following paragraphs.

4.4.1 Generalized Impact Surface Capability

This modification allows the user to specify a surface which makes an angle with the horizontal of up to 90 degrees. The airplane represented by the math model can be positioned relative to the surface with the proper input data selection, or, if the user chooses, the program will automatically position the vehicle in the proper attitude relative to the surface using the existing external spring input data. This is a practical feature and requires only one additional input term, the angle of the slope. The generalized impact surface is applied in the analysis of a stall-spin crash test that impacts into a 45 degree slope which is described in Section 5. The generalized surface capability is useful for analyzing crash conditions involving hillsides, mounds and possibly trees.

4.4.2 Cabin Volume Change

The prime concern in a crash is the protection of the occupant. As is noted earlier, one of the design goals is to have the structure crush and deform in such a manner that a liveable cabin volume will be maintained for the occupant and that the occupant is kept from impacting structure or hardware in such a manner as to receive serious or fatal injuries. Consequently, coding is added to KRASH wherein any eight masses are specified for a particular volume. The original coordinate positions of the masses are used to compute an initial volume. The new coordinates of the specified masses are computed at each integration. The ratio of the new volume to the original volume is calculated and printed out along with the regular output print. Although usually only one volume (occupiable region) is of concern, the program allows the user to specify up to eight distinct volumes. This modification in no way alters the program's basic computations. Since there will be an occupant-seat-restraint system model available later in the program, a refinement for future consideration would involve combining the volume history from KRASH and the occupant model history to ascertain relative positions and velocities of the structure and occupant extremities.

4.4.3 Acceleration Pulse Input

KRASH is modified to include provisions for specifying an acceleration pulse magnitude, shape, duration and direction for as many as 50 mass-directions*. The program requires that the following information be defined:

- o location of pulse (which masses)
- o direction of pulse (one or more of six directions)
- o history of the acceleration at the specified mass and its direction

Once specified, the accelerations of the designated masses are prescribed in the subroutine where accelerations are normally computed so that system velocities, displacements and subsequent forces are computed thereafter. Generally, a crash analysis is initiated with a known set of impact velocities. The velocity at each mass point is integrated to obtain a

* Each mass can have accelerations acting in six directions.

displacement. The displacement is used to develop forces via external force-deflection curves and internal member stiffnesses. However, this routine makes it possible to excite the system with an acceleration. It may be most useful in modeling substructure (seat system) or where an impact can be idealized with an acceleration pulse, (i.e. water impact).

4.4.4 Internal Computation of Element Linear Stiffnesses

The internal computation of element linear stiffnesses involves providing the following input data for each member:

E = modulus of elasticity

G = shear modulus

J = polar moment of inertia

A = cross sectional area

L = member length

I_y, I_z = area moment of inertia about the y and z axis

The data is used in the program to formulate a 6 x 6 linear stiffness matrix for each element. One line (card) of input data per internal element member is required instead of six cards of stiffness terms as was formerly required. Since stiffnesses are often obtained from the member properties prior to input to the program, this change can result in a substantial saving in effort. Wherein stiffnesses are known from available data, material properties representative of the section can still be readily obtained since the beam stiffness terms are related to the member properties in a relatively straightforward manner. The formulation of linear stiffness within the program does not alter any of the basic computations. Direct input of the stiffness matrices is still available as an option.

4.4.5 Member Directional Stresses

The determination of member directional stresses is obtained using the material property data used by the program to compute linear stiffnesses. The computation of stresses is an option which can be used even for

members wherein direct input of the stiffness matrix is employed.

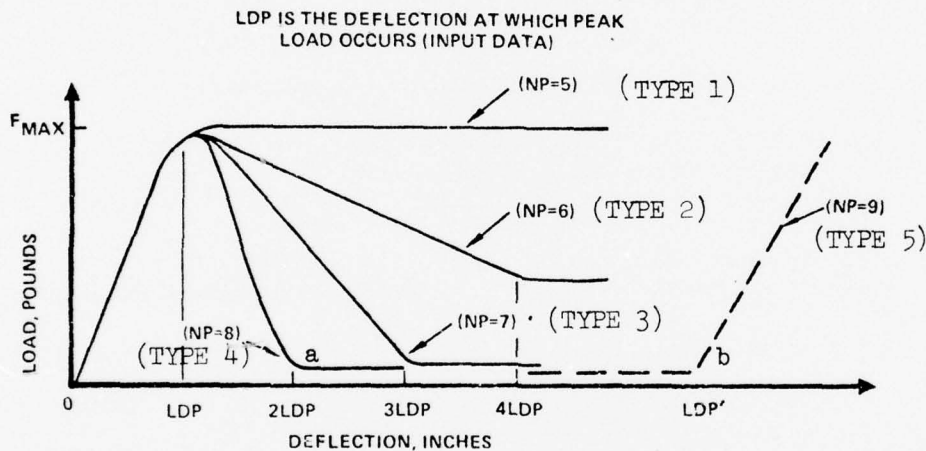
When stresses are desired, the program requires that the members be identified and that, in addition to the member properties used to formulate element stiffnesses, the respective distances to the neutral axis of the element and appropriate yield stress be provided. The procedure the program follows to compute stresses with the required input data is as follows.

- o Using member forces computed in the program and the member properties, the element stresses acting at the top, bottom, right and left side on each of the selected members is determined. The method of calculating the member forces is unchanged; stresses are calculated only for output information and are not used internally in the force calculations.
- o Combined stresses due to bending, axial, shear and torsional forces are computed.
- o The principal and maximum shear stresses are computed.
- o The maximum shear failure theory and the theory of constant energy of distortion for a combined axial and shear stress condition are applied.
- o Ratios of element stress to yield stress are computed during the entire analysis (A ratio of >1.0 indicates yield has been exceeded)

The above approach is simple and consistent with the techniques utilized in KRASH and, as such, has limitations. The incorporation of the stress check offers the advantage of being able to monitor selected elements to determine if they have reached a yield condition. Once the element has yielded the failure theories are invalid and, consequently, the most meaningful use of the stress data is to identify which elements yield and at what time during the crash analysis. The stress data can help assess the validity of results with regard to the data used in modeling some of the structure. However, the computed stresses should not be used to verify structural designs because they do not provide sufficiently accurate data with which to make critical design decisions. For example, the effect of stress concentrations, unique geometry shapes and detail attachment practices at joints, are not included. Furthermore, care should be exercised in using this option since many times a complex structure is idealized with beam properties.

4.4.6 Internal Computation of Nonlinear Curves

The determination of the exact nonlinear behavior of structural elements is very difficult, particularly when interaction of loads is involved. By the use of linear stiffness reduction curves, KR, different types of nonlinear behavior can be represented. It is shown in Reference 4 that by approximating the nonlinear behavior in this manner, while representing the proper failure load, responses which are sufficiently accurate for crash analysis purposes are obtained. Thus, carrying this approach one step further by preprogramming the typical nonlinear curve shapes, as shown in the following sketch, the need to input all KR tables is obviated.



A type 1 curve uses five data points (NP=5)*

A type 2 curve uses six data points (NP=6)*

A type 3 curve uses seven data points (NP=7)*

A type 4 curve uses eight data points (NP=8)*

A type 5 curve uses nine data points (NP=9)*

The input requirements to use the nonlinear curves consist of the identification of the member for which nonlinear behavior is desired, the deflection (LDP) at which inelastic behavior occurs, the direction of interest (3 translation and 3 rotations are possible), and the number of points (NP)

* Coding is self contained in KRASH

defining the curve. When $NP = 5, 6, 7$ or 8 or 9 , the program computes the nonlinear curve. When a 9 point curve is used the user also specifies the deflection corresponding to point b in the above sketch. When $NP \geq 10$ a series of KR versus deflection data points is required. This allows the user to retain the capability to define an arbitrary load-deflection curve. The relationship between KR versus deflection and load versus deflection is defined in the User's Manual (Reference 13, Section 3).

4.4.7 Provisions for Modeling Earth Scooping and Plowing

This modification is applied only to the masses which are identified as having an external spring. Following the principles outlined in Reference 12, the average scoop force acting on the airplane can be determined and approximated using a trapezoidal force-time history. Plow forces are computed in the same routine wherein crash forces and energies are obtained. Usage of this routine requires an input of average force at the appropriate mass location where scooping takes place.

4.4.8 Standardization of Terms

The purpose of using standardized terms is to simplify the input requirements for the user. Several areas where standardization is incorporated into program KRASH are described in Reference 4. The use of internally coded KR curves in this program is another example of standardization. The manner in which member damping is input into the program is altered to give the user more flexibility. The original version of KRASH requires one card of input data for each member. Thus, representing percent of critical damping for the particular member could require a maximum of 120 cards. KRASH is now coded that all members have a standard one (1) percent of critical damping. The user can use this standard value, give all members a different value, or give the members any combination of damping values. It is possible to run a 120 member analysis with as little as 1 damping card, instead of 120 damping cards.

4.4.9 Refinement of Damping Force Formulation

This change recodes the manner in which rotational velocities are

calculated which lead to the damping forces. Previously, negative damping terms could be developed which could hinder the analysis. Now, with judicious selection of damping coefficients and integration interval, this should no longer be a problem.

4.4.10 Addition of 'Model Parameter Data' Printout

This change provides a printout of vehicle c.g. coordinates, mass and inertia properties, member frequencies, and damping terms. This printout is valuable in the initial checkout of the math model to ascertain that the math model properly represents the vehicle properties. It also allows the user to detect any potential instability problem which could be associated with high frequencies or large damping terms.

4.4.11 Treatment of Beam Longitudinal Elongation

The manner in which the program treats beam longitudinal elongation due to large lateral translations and rotations is improved. The program previously utilized a method which led to inaccurate axial deflections under conditions of large lateral deflections or beam rotations. Now the current overall beam length is calculated, and incremental axial deflections are based on differences in beam lengths from one integration interval to the next.

4.4.12 Addition of External Spring Force and Compression Data

The program now prints out the external spring forces along with the spring compression in both ground and mass axis coordinates. The directions in which the forces act are identified. The added external spring force data is conveniently located with the external spring deflection data and provides useful information to help the user assess the results. The data allows the user to distinguish between crushing and friction forces.

4.4.13 Separation of Crushing and Friction Energy

The program now separates the crushing and friction energy terms. Previously both were included under the heading "crushing energy". The user can now assess the relative effect of the structure crushing and ground

friction employed in the analysis.

4.14.14 Revision to the KR Function Usage

The manner in which the KR function is used in the program has been revised. This change does not effect the input of data. The linear forces are multiplied by KR's to obtain reduced forces. Previously, the KR's reduced the linear deflections which, in turn, were multiplied by a linear stiffness matrix to obtain the reduced forces. The program is now coded such that, for the normally coupled beam motions (z, θ and y, ψ), the proportions of the total force and the moment due to deflection and rotation inherent in the linear system are preserved, while still accounting for the nonlinear load-deflection characteristics. It is desirable to retain this relationship in order to minimize the possibility of developing negative strain energy with large nonlinear responses.

4.14.15 Revisions to the Input Format

This change simplifies the data input requirements and organizes the print of data in a more orderly fashion. The data that is normally required (basic data) is now input initially in the following sequence:

- o control cards
- o mass coordinates and associated data
- o external member data
- o internal member data
- o options (volume, stress, DRI)
- o seldom used data (Euler angles, inertia cross products)

Section 2 of the KRASH User's Manual (Reference 13) describes and illustrates the revised input format.

4.4.16 Revisions to the Output Format

This change organizes the output data in a more orderly manner and provides additional information to facilitate the user's understanding and

evaluation of the results. Included in this change are the following:

- o The print-out of the input data is presented in a more organized manner such that standard mass and member data is easily delineated.
- o The unnecessary presentation of large zero matrices of data is eliminated.
- o The output data provides a print of member strain force and total forces. Previously only the member **strain** force was available. The difference between member total force and member strain force is the damping force contribution. Consequently, the user can assess the relative effect of the **stiffness** and damping data that contributes to these forces.
- o The output format contains expanded print for external spring forces and deflections which now includes ground contact point loads in ground (or slope) and mass axes.
- o Vehicle c.g. translational velocities in ground axes, based on system linear momentum considerations are presented at each print interval.

4.4.17 Miscellaneous Coding Changes

The program has been recoded to allow the use of large initial pitch angles (> 90 degrees), and to properly calculate forces resulting from negative external spring lengths (required for the inverted crash condition). This change eliminates the possibility of computing negative crushing energy.

The program has also been recoded to allow external springs to deflect beyond the maximum free length value that may be used as an input. This change eliminates one of the conditions which could result in negative external spring energy being developed in a math model.

4.4.18 Addition of Subroutine ECHO

This subroutine was added to the program to facilitate the user's task of evaluating the validity of the input data format. ECHO prints out the input in card image format which allows for a rapid assessment of any potential errors in data, input format, out of order cards and/or improper control cards.

4.4.19 Use of English Words

English words have been added in such a manner that they precede the printed symbols, which are retained. The English words clarify the meaning of the output while the symbols in many instances relate to the coding contained in the program.

SECTION 5

ASSESSMENT OF PROGRAM KRASH

5.1 PURPOSE AND METHOD

Program KRASH was verified using experimental data obtained from a full scale helicopter crash test involving a combined vertical and lateral impact velocity(Reference 3). There are many similarities in the requirements for the crash analysis of helicopters and general aviation airplanes, including:

- o exposure to multidirectional forces during a crash
- o comparable takeoff weights for certain classes of each
- o similar structure in many areas
- o multiple impacts for certain crash conditions
- o comparable crash durations

However, airplanes and helicopters have significant differences which affect the requirements for performing crash analysis. These differences involve:

- o design configurations
- o mass locations
- o seat systems
- o operational modes which will affect probable impact conditions

Furthermore, the results of the evaluation of airplane design characteristics, as well as the accident review and evaluation, led to the inclusion of additional capability for KRASH (discussed in previous section). Consequently, the development of KRASH, modified for general aviation airplane application, requires that some reasonable assessment of its capability be made prior to initiating fully instrumented full scale airplane crash tests in support of

the verification program of Task II.

Ideally, it is desirable to compare analytical results with controlled crash test data from test articles of comparable size, configuration, complexity and weight as the intended structural system. The availability of such test data for two different general aviation airplanes of current design and representing two probable accident conditions, provides a practical means of assessing program KRASH. The crash tests, while limited in the amount of measured quantitative structural response data, provided a significant quantity of high speed film and photographic coverage with which to assess KRASH's capability to predict structural deformation, multiple impacts and rigid-body large motion post-impact behavior. The tests also provide data with which to assess the validity of program modifications and to obtain information which can be utilized in the development of a KRASH User's Manual and Structural Design Guide (Reference 13). The crash tests represent impact conditions for typical general aviation airplane crashes in which multidirectional forces are involved. The mathematical models, crash test data, comparison of analysis and test results, and the assessment of KRASH are described in the following subsections.

5.2 GENERAL DESCRIPTION OF AIRPLANES

To demonstrate that program KRASH is potentially an acceptable analytical method with which to perform crash analysis for general aviation airplanes, two representative airplanes are selected to be modeled and the results of the analyses compared to the available test data. The airplanes designated Airplane A and Airplane B are shown in Figures 14 and 15 and are described below:

Airplane A

- o Category 1 (See Table 4)
- o single-engine, high-wing configuration
- o side by side seats (2 occupants)



Figure 14. Airplane A, High-Wing Single-Engine Type

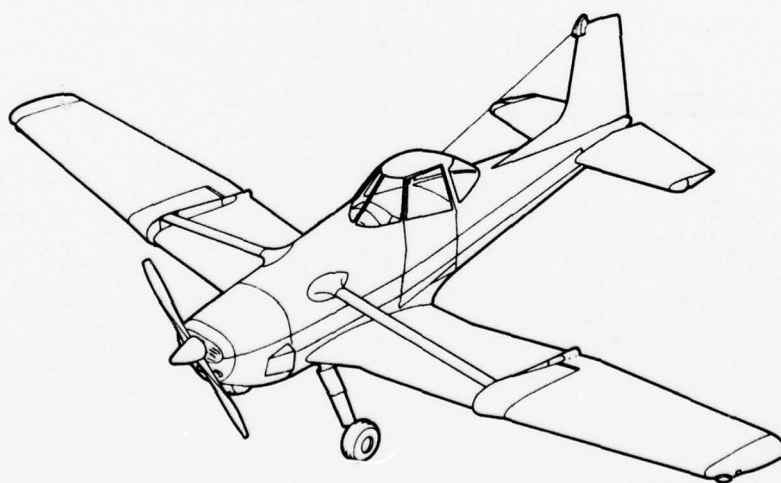


Figure 15. Airplane B, Low-Wing Single-Engine Type

Airplane A (Cont.)

- o used for training, sport and aerobatic (acrobatic) purposes
- o stall speed \leq 42 knots
- o cruise speed (75 percent power) \leq 102 knots
- o maximum takeoff weight, 1600 pounds
- o fuselage is of all semi-monocoque construction. The wing is a cantilever structure designed with two main spars and with a midspan braced strut. The landing gear is a non-retractable tricycle type. The tail is of cantilever design.
- o flight design load factors of: +4.4 g's and -1.76 g's (utility)
+6.0 g's and -3.00 g's (aerobatic)
- o overall dimensions are: wing span = 384 inches, length = 280 inches
- o the weight - c.g. envelope is shown in Figure 16

Airplane B

- o Category 3 (see Table 4)
- o single-engine, low-wing configuration
- o single seat
- o used for application of chemicals to or seeding crops
- o stall speed \leq 50 knots
- o cruise speed (75 percent power) \leq 122 knots
- o maximum takeoff weight = 3300 pounds (4000 pounds in restricted category)
- o Fuselage structure is a rectangular section, welded steel tube construction in the forward and cabin area and semi-monocoque construction in the rear. The wing is a cantilever structure designed with two main spars with a midspan braced strut. The landing gear is a non-retractable tail-wheel type. The tail is of cantilever design.
- o flight design load factors of: +3.8 g's and -1.52 g's
- o overall dimensions are: wing span = 474 inches, length = 273 inches
- o the weight-c.g. envelope is shown in Figure 17

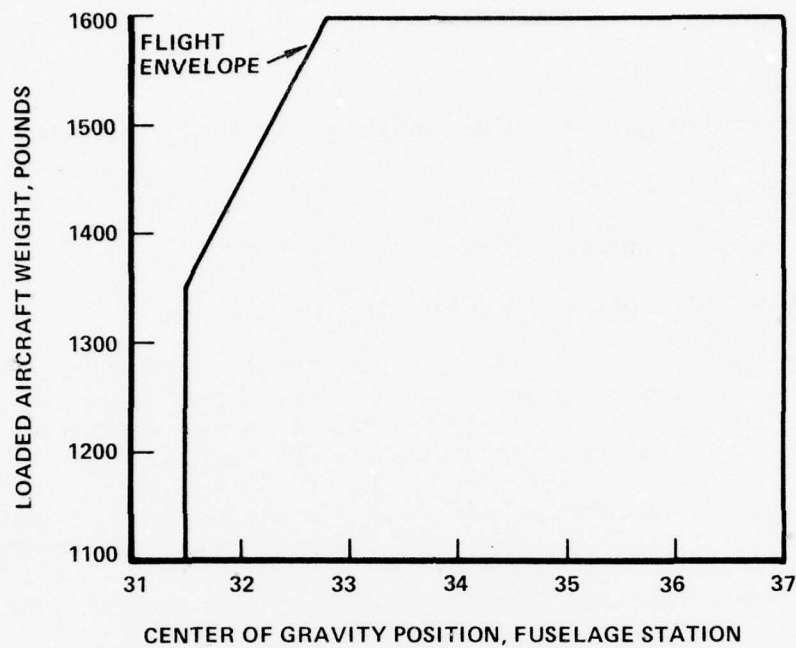


Figure 16. Weight - CG Flight Envelope for Airplane A

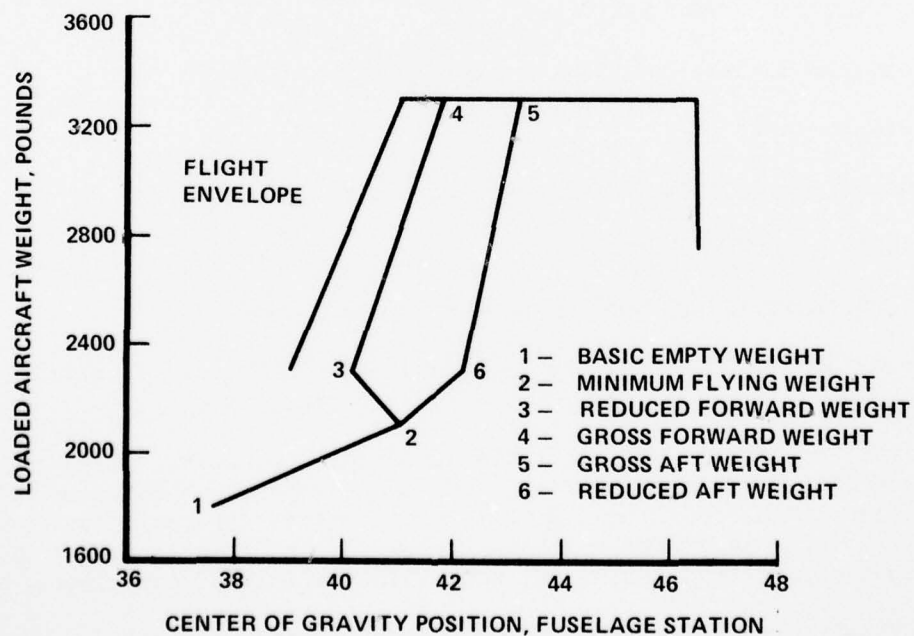


Figure 17. Weight - CG Flight Envelope for Airplane B

5.3 CRASH TEST DATA

5.3.1 Airplane A Stall-Spin Crash Test

5.3.1.1 Test Objectives

The test objectives were to:

- o check out the crash test facility and determine potential improvements for further tests
- o determine crash characteristics of the Category 1 airplane during a stall-spin crash
- o determine the chances of survival for the occupants during a stall-spin crash

This was the first full scale airplane crash test performed at a test site which consists of an asphalt track 20 feet wide and 600 feet long terminating in a dirt barrier that is readily shaped to simulate selected crash impact angles. A steel rail in the center of the track is used for control of the tow dolly during acceleration of the specimen. Propulsion is provided by an engine and winch applying direct power to the specimen tow dolly through a steel cable.

5.3.1.2 Test Setup and Procedure

The test specimen contained two instrumented dummies as occupants (95th percentile (pilot) and 50th percentile (co-pilot)). The accelerometers in the dummies were located at F.S. 44.0, W.L. -16.0, B.L. ±9.0 in the pelvises. and F.S. 48.0, W.L. +19.0, B.L. 9.0 for the pilot head and F.S. 47.0, W.L. +17.0, B.L. -9.0 for the co-pilot head. Accelerometers were located on the centerline of the floorboard (F.S. 56.7, W.L. -11.0, B.L. 0.0) and oriented in the vertical and longitudinal directions. One wing had lead secured in the fuel tank bay and the other fuel tank was filled with colored water representative of the fuel weight. Angular spoilers were attached to the leading edge upper surface of each wing to prevent lift off. The instrument panel was representative of the panel normally used in this particular airplane. The seats were standard 1969 versions. The left seat had the regular seat belt but the right seat restraint system included a seat belt, shoulder harness and attachments. The nose wheel was replaced with a wheel and dolly.

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A METHOD OF ANALYSIS FOR GENERAL AVIATION AIRPLANE STRUCTURAL C--ETC(U)
SEP 76 G WITTLIN, M A GAMON

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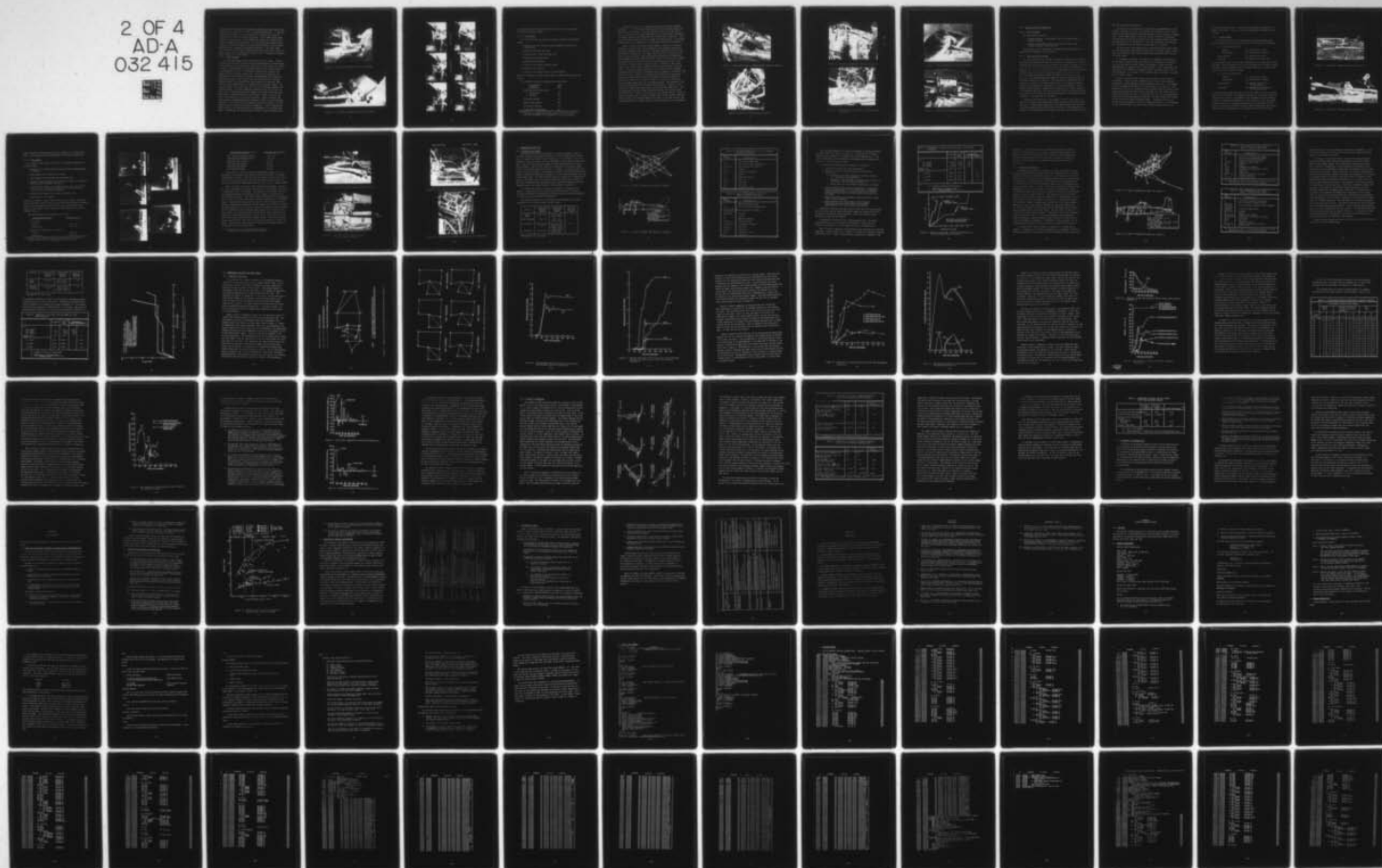
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The dolly and tow attachment incorporated a mechanical release system which caused both the dolly and tow cable to release simultaneously. A 'dead man' brake system consisting of an accumulator and solenoid valve connected directly to the ship's battery was installed. One 47 frame/second camera filmed the overall crash. One 64 frame/second camera with telephoto lens filmed the impact with the barrier. One 1000 frame/second camera filmed a close-up of the barrier impact (the poor lighting provided for this camera made the results unusable for engineering analysis). Two normal speed (18 frames/second) documentary cameras filmed the overall crash. Figure 18 shows a side view of the airplane in position prior to impacting the barrier with a velocity of 45 feet/second.

5.3.1.3 Crash Sequence

The nose wheel makes initial contact with the dirt barrier. Failure of the nose wheel strut aft does not significantly impede the forward motion of the airplane and the spinner and lower portion of the engine cowl contact the barrier approximately 30 milliseconds later, with a forward velocity of approximately 45 ft/sec. The forward fuselage, after impacting the barrier, rides up as high as three feet. The tail cone buckles at its attachment to the fuselage aft bulkhead at approximately 100 milliseconds after spinner impact. The co-pilot, who was restrained with a shoulder harness, appears to move forward and nearly impacts the instrument panel with his head at approximately 140 milliseconds after spinner impact. The co-pilot impacted the control wheel and his lower extremities impacted the instrument panel. The pilot apparently submarined under his lap belt (he did not have a shoulder harness) and impacted the control wheel with sufficient force to break the left grip of the wheel. Figure 19 shows a side view of the airplane in its post crash condition. Figure 20 depicts the crash sequence from approximately nose (spinner) impact to 180 milliseconds thereafter. The film analysis was performed during this program. The film analysis data and results are provided in Appendix C. The 47 frame/second film was used for the analysis, which is approximately 20 milliseconds per frame. Consequently, the sequence shown in Figure 20 may be delayed by up

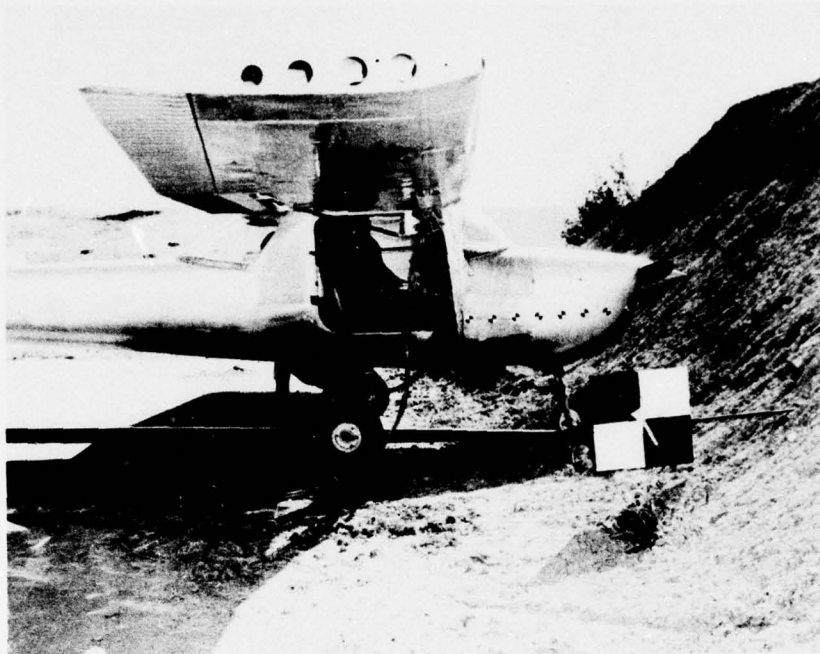


Figure 18. Side View of Airplane A Prior to Crash Test



Figure 19. Side View of Airplane A After the Crash Test



Time = 0



Time = .020 Seconds



Time = .060 Seconds



Time = .100 Seconds



Time = .140 Seconds



Time = .180 Seconds

Figure 20. Crash Test Sequence for Airplane A

to 20 milliseconds if the event noted at time zero is due to nose gear failure and not spinner impact.

5.3.1.4 Test Results

As a result of the test crash, the airplane sustained the following damage:

- o Failure of the left wing rear spar attachment (this was not a standard part)
- o Failure of the right door post
- o Buckling (aft) of the nose wheel strut
- o Buckling of the engine mounts
- o Buckling of the firewall
- o Bending of the control column and wheel
- o Denting of the nose cap
- o Wedging of the rudder to the full right position

There was no damage to the main gears, seats, occupant restraints and fuel system.

The summary of recorded accelerations is given below:

<u>Accelerometer *</u> <u>Location</u>	<u>Peak</u> <u>g's</u>
Floorboard over the main gear	
o longitudinal	121
o vertical	106
Pilot head vertical	100
Co-pilot head vertical	104
Pilot pelvis vertical	94
Co-pilot head longitudinal	113

* Presented in airplane coordinate system for the structure and body axis (see Figure 1-4, Reference 12) for the occupants

A composite of all the accelerometer traces indicated that the peak amplitudes all occurred simultaneously and they have approximately the same levels and waveforms. From past experience, there is a time lag between the fuselage and occupant responses as well as significant differences in response frequency which indicates that the data may be deficient. Only the floor response data was used to compare with KRASH results. The occupant response data is more applicable to occupant-seat-restraint system models.

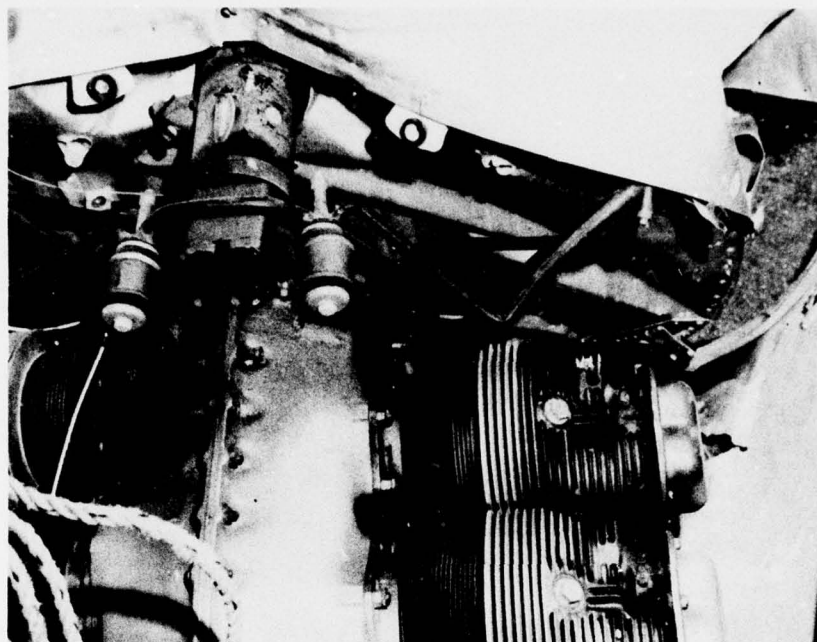
Figure 21 shows the forward fuselage damage, consisting of extensive crushing of the lower cowl, some deformation of the propeller spinner and very little damage to the upper cowl. The upper structure aft of the firewall failed in compression. The lower structure moved aft relative to the wing and upper structure. The lower fuselage structure has substantially less deformation than the upper structure. Figure 22 shows the cabin damage. The occupant (right side) with the seat belt and shoulder harness is restrained. Unlike the other occupant, he did not submarine. The volume change shown is less than the maximum distortion that occurred during the crash. The structure sprang back from 25 to 50 percent from its maximum deflected position, which is consistent with data reported in Reference 4 and findings by NASA. Analysis of the high speed camera data was performed during this program and the cabin volume behavior which was obtained is described in Section 5.5. Figure 23, which is a top view of the engine, shows the upper engine mounts in a buckled condition. The generator at the top aft portion impacted the severely buckled firewall. Figure 24 illustrates the buckled lower engine mounts and aft bent nose wheel strut. The top engine and nose strut support structure has been cut to allow access to the structure. Figure 25 shows the tail cone bending failure. Figure 26 shows the non-standard wing spar attachment shear failure described earlier. Unlike the cabin and fuselage damage, the failure of the tail cone and wing spar attachment did not pose a threat to the survivability of the occupants.



Figure 21. Three-quarter View of Forward Section Damage (Airplane A)



Figure 22. Side View of Cabin Damage (Airplane A)



↑
AFT

Figure 23. Top View of Engine Mount Damage (Airplane A)

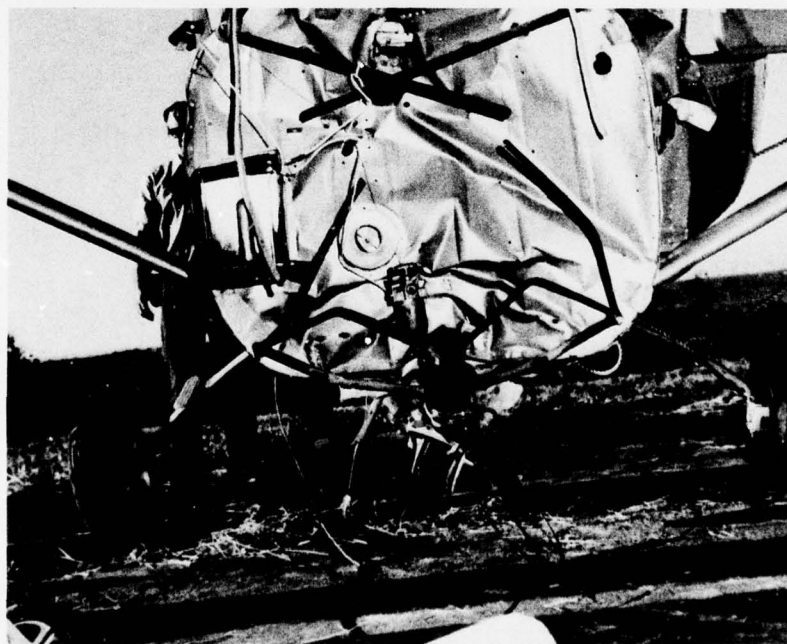


Figure 24. Front View of Engine Mount and Firewall Damage (Airplane A)

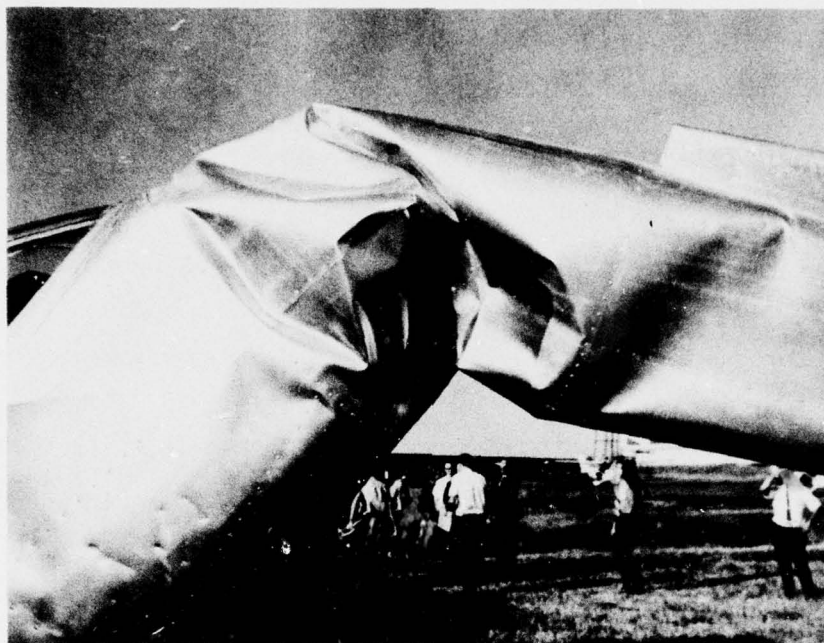


Figure 25. Side View of Tail Cone Damage (Airplane A)



Figure 26. Front View of Wing Damage (Airplane A)

5.3.2 Airplane B Turnover Crash Test

5.3.2.1 Test Objectives

The test objectives were to:

- o determine chances of survivability for the occupant during a turnover accident
- o determine acceleration levels on the structure and on the occupant during a turnover accident

The turnover test was performed at the same test facility that the stall-spin test (Airplane A) was conducted.

5.3.2.2 Test Setup and Procedure

The test specimen was an original engineering prototype and contained one 95th percentile instrumented dummy as an occupant. Accelerometers, oriented longitudinally and vertically, were located in the head of the dummy (F.S. 103, W.L. +50, B.L. 0.0) and on the structure near the airplane intermediate c.g. position (F.S. 41, W.L. +2.0, B.L. 19.0). Accelerometers were also located in a vertical position on the aft turnover structure (F.S. 110, W.L. 45.8, B.L. 0.0) and on the forward turnover structure (F.S. 84.6, W.L. 47.3, B.L. 0.0). The aircraft hopper was empty and the fuel tank was filled with 40 gallons of water (8.34 lbs/gal). The water added an additional load of 99 pounds in excess of the normal weight of fuel. The seat and restraint system for the airplane were standard for this type of airplane. The restraint system included a standard shoulder harness with a rolled lap belt to accommodate load cells. The load cells were located on the left and right hand sides of both the lap belt and shoulder harness. The instrument panel contained a full complement of instruments.

Batteries were installed in the airplane to power a wing (left side) mounted 1000 frame/second camera which filmed the occupant and cabin during the crash. Another camera operating at 1000 frames/second filmed the test run from a stationary position outside the airplane. Cameras operating at speeds of 24 frames/second and 64 frames/second were used to record the total

test run and monitor the turnover.

The airplane was accelerated by a tow engine to approximately 30.5 mph through a distance of 75 feet. The airplane was attached to the tow dolly system at the front wheels to enable the airplane to be towed along a straight line. A rear support dolly was provided to keep the tail of the airplane from descending during the tow phase of the test, thereby simulating a wheel landing condition. At a distance of 1 foot from the barrier, the airplane was disengaged from the tow dollies and proceeded as a free body.

The wheel brake system employed was the standard airplane brakes except for the replacement of the master cylinder with a 'dead man' system, consisting of an accumulator and a solenoid valve which was plumbed directly into the wheel brakes.

To accomplish a turnover, the brakes on the airplane were locked and the tow engine stopped for the final 28 feet to the barrier; the resulting drag load acting at the wheels caused the airplane to rotate nose down approximately 32.5 degrees from its towed position. After nose contact with the ground, the airplane did a complete turnover and came to rest in an inverted position. To simulate a field condition impact, the track was covered with 12 inches of dirt.

Prior to the actual test, several runs were made for the purpose of calibration. During the first calibration run, the tail of the airplane inadvertently rotated upwards caused by excessive cable slack. This mishap resulted in damage to the skin of the lower center of the tailcone. Calibration runs were used to determine starting distance from the barrier, brake application distance from the barrier, dead time and skid distance during braking, and linear velocities. During the first test run, the brake system failed and the airplane impacted the barrier. The main landing gear sheared off but there was no other structural damage. On another test run, the velocity was insufficient to result in a complete turnover. As a consequence of this aborted attempt, the engine mount assembly failed and had to be

welded before testing resumed. The test was accomplished finally with no further difficulties. Figure 27 shows the airplane test setup prior to the turnover.

5.3.2.3 Crash Sequence

Film analysis of the test indicates that the airplane forward cowl section initially contacts the ground with the following impact conditions:

c.g. velocity (ground axis)

vertical	19.5 inches/second (down)
longitudinal	259 inches/second (forward)
pitch attitude	38.5 degrees (nose down)
pitch rate	106 degrees/second (nose down)

The film analysis shows that it takes approximately 1.5 seconds after initial nose impact for the airplane to pitch over and impact on the forward turnover structure. When the airplane is in its inverted position, it contacts the ground under the following conditions:

c.g. velocity (ground axis)

vertical	102 inches/second (down)
longitudinal	45.5 inches/second (forward)
pitch attitude	19.6 degrees (nose down in inverted position)
Pitch rate	89.4 degrees/second (nose down in inverted position)

After the initial impact and prior to the second impact, the left wing made contact with the ground. The damage to the wing tip due to this contact is slight and the effect on the response of the fuselage, cabin structure and occupant is considered insignificant. After turning over onto the forward turnover structure, the airplane continues its nose-over motion and the vertical tail section contacts the ground before the airplane comes to rest. Figure 28 shows the airplane in its inverted position after the crash.

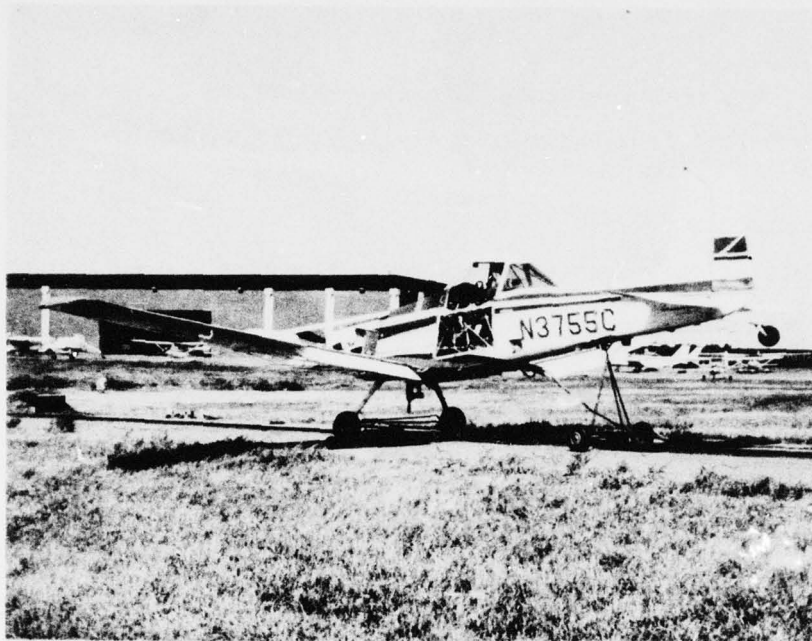


Figure 27. Side View of Airplane B Prior to the Crash Test



Figure 28. Side View of Airplane B After the Crash Test

Figure 29 shows the crash sequence from nose impact to 1.5 seconds thereafter. Data obtained from the film analysis is presented in Appendix C.

5.3.2.4 Test Results

As a result of the turnover crash test, the airplane sustained the following damage:

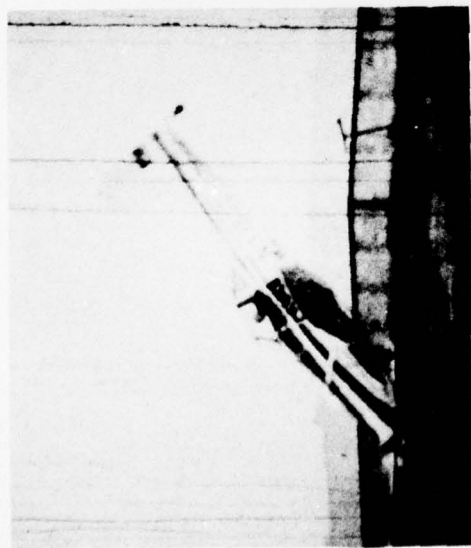
- o Failure of the forward turnover structure (downward approximately 2.5 inches)
- o Minor damage to the vertical tail section
- o Minor damage to the left wing tip and leading edge
- o Failure of the left engine mount in shear or tension at a position between the mount assembly and engine
- o Failure of the tubular mount assembly on the left side (location of failure is at the position where failure occurred during a test run and the structure was welded)
- o Extensive skin damage to the cowling and hopper area
- o Minor damage to the firewall

There was no damage to the main gears, tailcone, aft turnover structure, seat and restraint system, right wing, and right engine mounts and assembly. Based on the acceleration levels, tolerance curves and severity index analysis, the occupant was not expected to have experienced any brain or vertebrae injury.

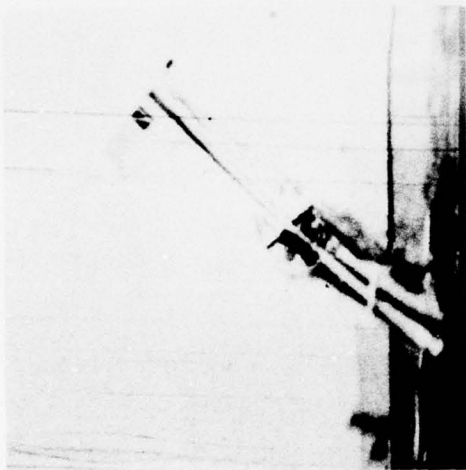
The peak response data is summarized as follows:

<u>Accelerometer Location*</u>	<u>Peak Load or g's</u>
Pilot's Head	
vertical	32.9 g's
longitudinal	20.1 g's
Proximity of Longitudinal C.G. Position	
vertical	21.24 g's
longitudinal	11.81 g's

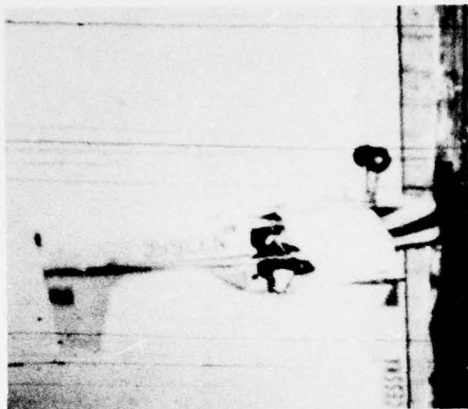
* Presented in the airplane coordinate system for the structure and body axis (see Figure 1-4, Reference 12) for the occupant



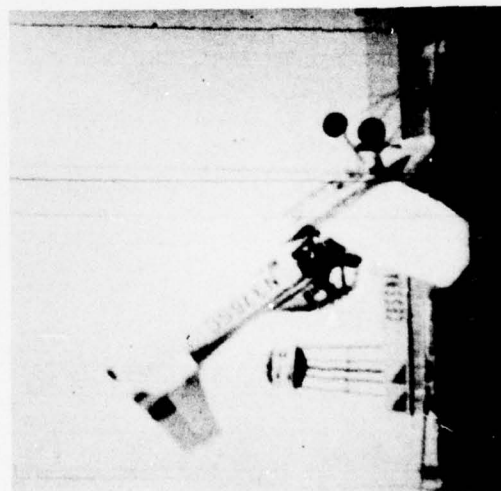
TIME = 0.0 SECONDS



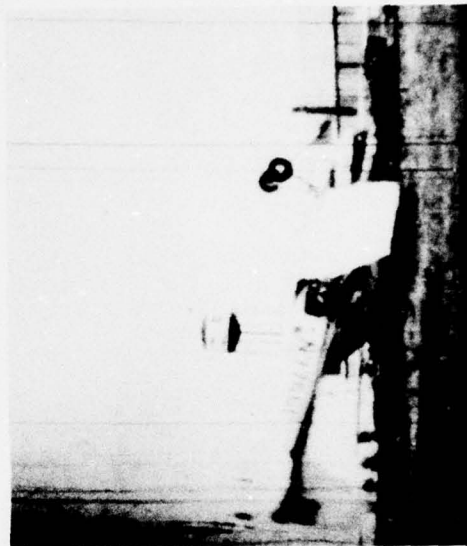
TIME = .083 SECONDS



TIME = .666 SECONDS



TIME = 1.25 SECONDS



TIME = 1.50 SECONDS

Figure 29. Crash Test Sequence for Airplane B

<u>Accelerometer Location*</u> (Cont.)	<u>Peak Load or g's</u> (Cont.)
Fwd. Turnover Structure Vertical	97.2 g's
Aft Turnover Structure Vertical	72.2 g's
Right Seat Belt (rolled)	399 lbs.
Left Seat Belt (rolled)	699 lbs.
Right Shoulder Harness	792 lbs.
Left Shoulder Harness	521 lbs.

During the test, the tape recorder malfunctioned causing a loss of definition of the response wave forms and times of occurrence of the peak accelerations and loads. While seat belt and harness load cell data may be useful in future evaluation of occupant-seat-restraint system models, the structural acceleration measurements were of little value in assessing KRASH.

Figure 30 shows a side view of the forward fuselage damage. Although the cowl is substantially deformed, the structure at the firewall and aft of it experienced little or no damage. The damage to the underside of the cowl was experienced during the preliminary tests. Figure 31 shows the pilot position after the crash. The forward turnover structure has been compressed and is buried in the dirt while the aft turnover structure had no noticeable damage. The structure surrounding the cabin and below it appears to have remained unchanged which indicates that the energy associated with the impact had been absorbed by the dirt and in crushing the forward turnover structure. While no quantitative data regarding volume change could be obtained from film analysis, the photographs during and after the crash indicate that no significant volume change occurred. Figures 32 and 33 show front and side views of the engine mount and mount assembly damage. The left side mounts failed during the test. The right side mounts were damaged in removing the engine. The left side mount assembly was damaged during pretest checkout and was welded for the turnover test.

*Presented in the airplane coordinate system

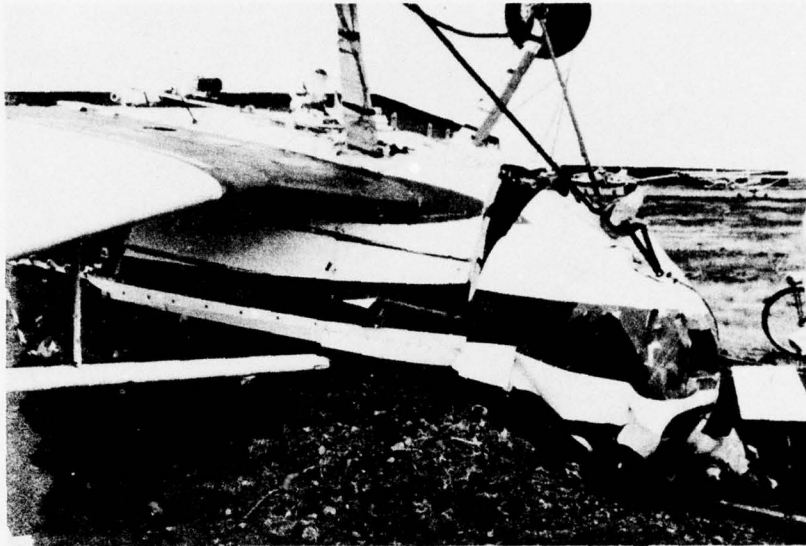


Figure 30. Side View of Forward Fuselage Damage (Airplane B)

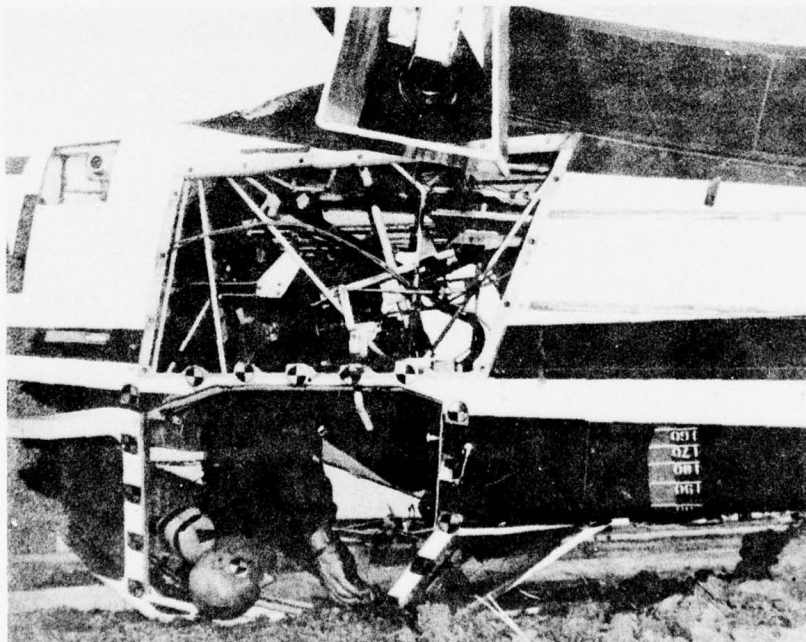


Figure 31. Side View of Cabin Area and Turnover Structural Damage (Airplane B)

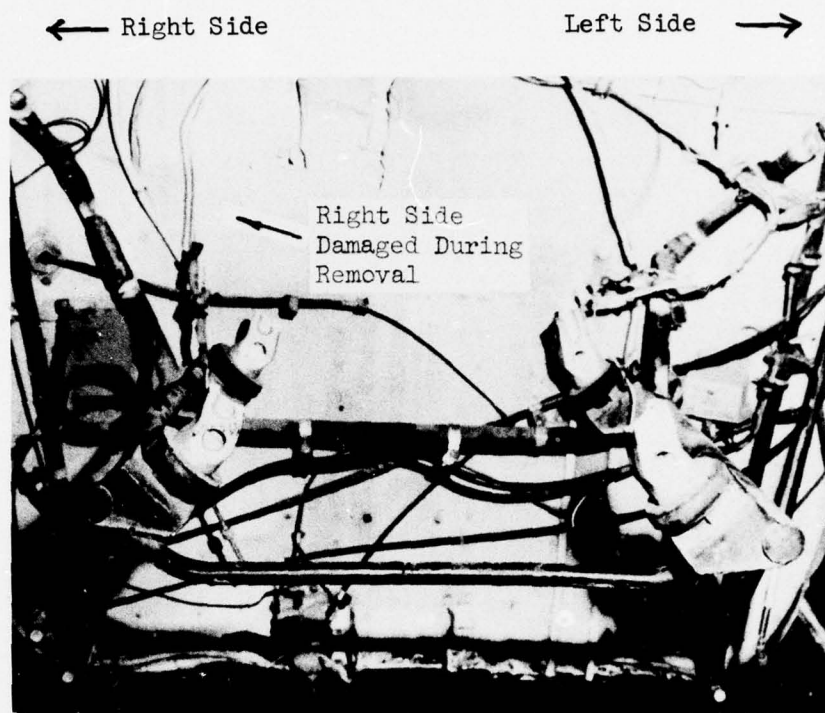


Figure 32. Front View of Engine Mount Failure, Left Side (Airplane B)



Figure 33. Side View of Engine Mount Failure, Left Side (Airplane B)

5.4 MATHEMATICAL MODEL DATA

5.4.1 Airplane A Math Model

The mathematical models for Airplane A are shown in Figures 34 and 35. The crash condition being analyzed involves a forward fuselage (nose) impact into a 45-degree dirt barrier with no initial yaw or roll angles. Due to the symmetry of the crash impact, and the availability of only side-view film coverage, a math model with a reduced number of masses and members can be used to good advantage. The model size reduction is obtained by utilizing a planar model of the fuselage (all masses in the $Y = 0$ plane). The smaller model size permits an initial checkout, to determine the portions of the model wherein more rigorous modeling requirements are needed, in a more economical manner than that of the larger model. The model shown in Figure 35 consists of 21 masses and 32 members. A description of the mass representations is provided in Table 10. The model coordinates, mass properties, inertia properties, member properties, damping factors, and initial conditions are presented in Appendix C.

The larger model, shown in Figure 34, consists of 35 masses and 69 members. A description of the mass representations is given in Table 11. The model coordinates, mass properties, inertia properties, member properties and damping values are presented in Appendix C.

The internal elements in the math models are represented with linear properties at all locations except as noted below:

Location	21 Mass Model Nonlinear Members	35 Mass Model Nonlinear Members	Type of* Nonlinear Curve(s)
Engine Mount	9-13, 10-13	9-13, 10-13, 11-13, 12-13	5
Fwd. Fuselage	7-10, 6-9	7-10, 6-9, 12-17, 11-16	5
Mid Cabin	4-5, 4-6, 6-7, 7-8, 5-8.	4-5, 4-6, 5-20, 18-20, 19-20, 16-18, 16-19, 6-15, 15-16.	3, 4, 5
Tail Cone	11-17, 12-17	30-32, 31-32, 21-32, 22-32	3

*See page 66 for curve types

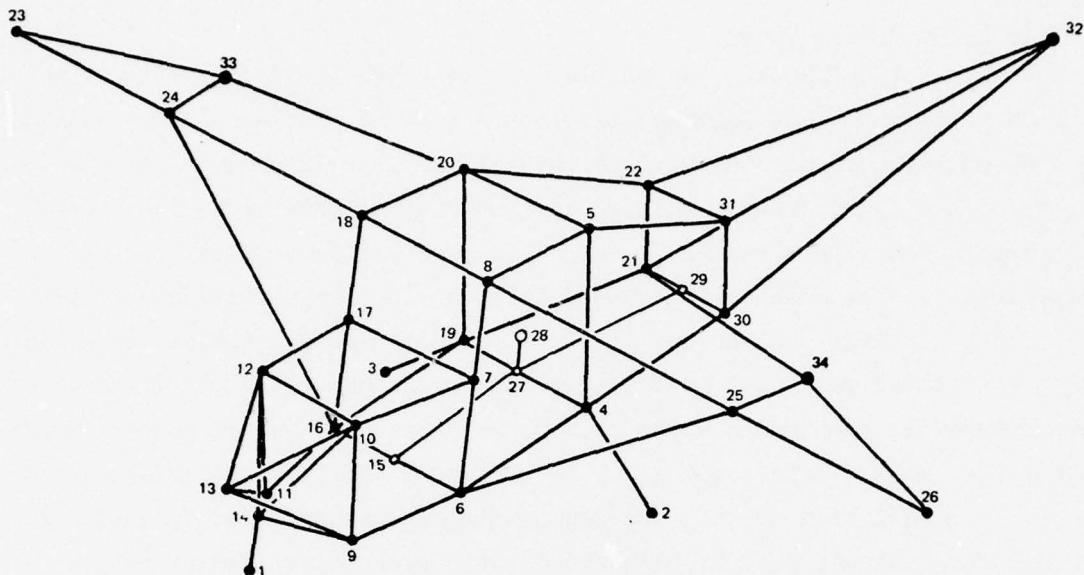


Figure 34. 35 Mass, 69 Member Math Model for Airplane A

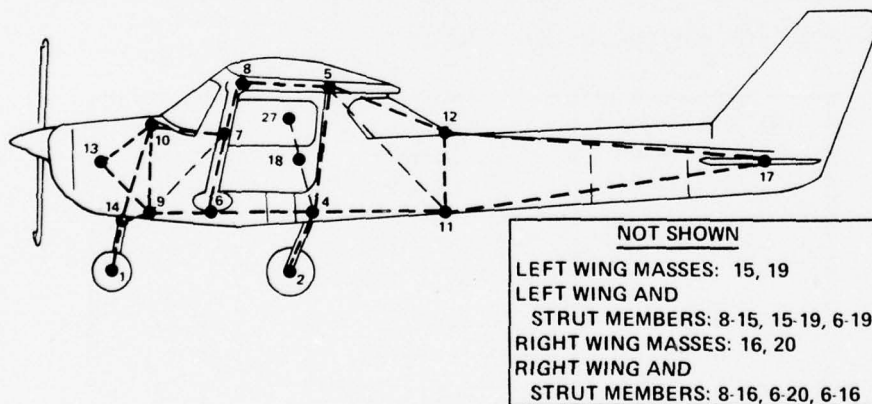


Figure 35. 21 Mass, 32 Member Math Model for Airplane A

TABLE 10. MASS IDENTIFICATION FOR 21 MASS, 32 MEMBER
AIRPLANE A MATH MODEL

Mass Point(s)	Representation
1	Nose Gear Unsprung Mass
2,3	Main Landing Gear Unsprung Mass
4,5,6,7,8	Mid Fuselage Cabin Region
9,10	Firewall
11,12	Fuselage Aft Bulkhead
13	Engine
14	Nose Gear Trunnion
15,19	Left Wing
16,20	Right Wing
17	Tail Unit
18,21	Occupant and Seat

TABLE 11. MASS IDENTIFICATION FOR 35 MASS, 69
MEMBER AIRPLANE A MATH MODEL

Mass Point(s)	Representation
1	Nose Gear Unsprung Mass
2,3	Main Landing Gear Unsprung Mass
4,5,6,7,8,16 17,18,19,20	} Mid Fuselage Cabin Region
9,10,11,12	Firewall
13	Engine
14	Nose Gear Trunnion
15,27,29	Floor Structure
21,22,30,31	Fuselage Aft Bulkhead
25,26,33	Left Wing
23,24,34	Right Wing
28,35	Occupant and Seat
32	Tail Unit

The nonlinear properties are based on estimates of buckling strengths, available design load data and/or test data. Procedures for obtaining input data are described in the KRASH User's Manual (Reference 13). The standard nonlinear curves incorporated in program KRASH, and described in Section 4.4 of this report, are used.

The procedure for performing the analysis is as follows:

1. Establish both small and large linear models
2. Using the 'model parameter' printout data described in Section 4.4:
 - a) determine if the model accurately reproduces airplane C.G. and vehicle mass properties,
 - b) determine if the stiffness and damping factor values will potentially cause instability problems, and
 - c) refine model mass and stiffness properties, if required.
3. Using the smaller model, initiate analysis for a limited time duration (approximately 20 to 40 milliseconds) and determine energy flow distribution. Use initial estimate of external force-deflection curve with initial impact velocities, rates and angles.
4. Refine the smaller model nonlinear representations and perform longer duration checkouts.
5. Perform checkout with larger model, using nonlinear representations based on the results of the smaller model analysis, for a short duration time period.

Preliminary analytical runs were made to verify that the nose gear fails and in so doing does not absorb significant energy nor change the attitude at impact of the spinner with the barrier. The initial spinner impact velocity was based on film analysis.

A description of the use of the 'model parameter data', the energy distribution printout, the external force-deflection curves, and how failure loads are estimated is presented in Section 3 of Reference 13.

Table 12 shows a comparison of the Airplane A and math model C.G. and mass properties. The math model C.G. is within 0.6 inches of the estimated fuselage station and within 2 inches of the waterline, respectively, compared to the

TABLE 12. COMPARISON OF AIRPLANE A AND MATH MODEL C.G. AND MASS PROPERTIES

	Airplane A	Math ^(a) Model	Difference ^(b)	
			Inches	Percent
C.G.				
FS, inches	36.9	36.32	.58	
BL, inches	.28	0.0	.28	
WL, inches	1.85	3.77	1.92	
Weight, lb.	1600	1600		0
Moment of inertia, lb.-in.-sec. ²				
I _x (roll)	9000	9243		2.7
I _y (pitch)	9657	10186		5.5
I _z (yaw)	16192	16366		1.1
(a) average of small and large model				
(b) $\frac{\text{model value} - \text{airplane value}}{\text{airplane value}} \times 100$				

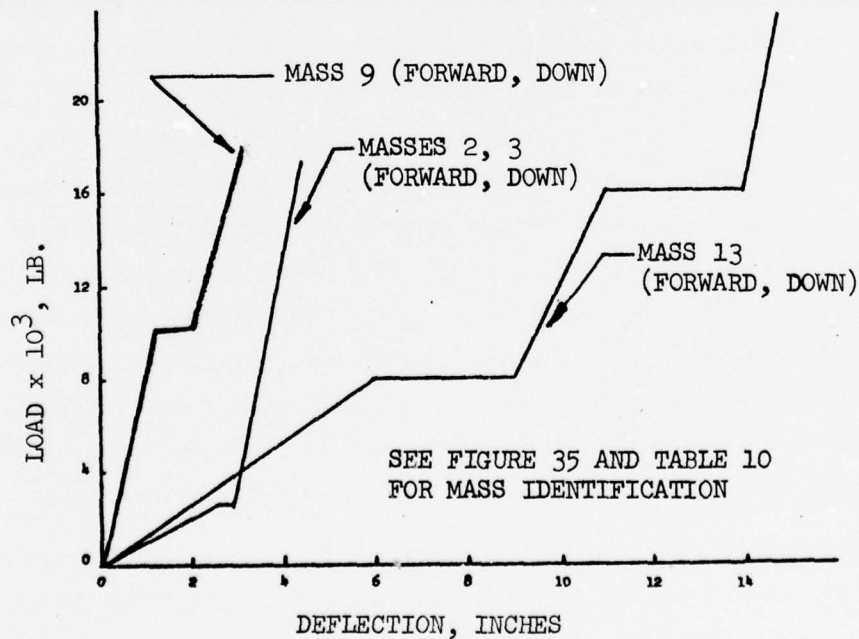


Figure 36. External Spring Load - Deflection Characteristics Used in the Math Model For Airplane A

airplane C.G. The math model inertia properties are within at least 5.5 percent of the estimated airplane values. Actual airplane inertia properties for the test configuration are not available. The external load-deflection characteristics used for Airplane A are shown in Figure 36. The results of the analysis and comparison with test data are given in Section 5.5.1.

5.4.2 Airplane B Math Model

The mathematical models for Airplane B are shown in Figures 37 and 38. The crash condition being analyzed involves an airplane moving at a forward velocity while pitching and rotating nose down. The forward section of the airplane digs into the dirt and the airplane rotates tail over onto its turnover structure. The time duration of the complete crash is approximately 1.7 seconds which is an order of magnitude longer than the significant portion of a typical crash. For most of that time no significant damage occurs. Consequently, this type of accident is idealized as two separate impacts. The damage sustained during the initial impact is included in the model when treating the second impact condition. The technique of using two models (small and large) for each impact is adopted for this crash analysis for the same reasons as that of the analysis of Airplane A. The models developed for the initial forward fuselage impact are similar to the models needed to analyze the second impact (overturn) except for some minor changes such as location of external contact springs and the representation of structure that is damaged during the initial impact. The model shown in Figure 38 consists of 25 masses and 38 members. A description of the mass representations is provided in Table 13. The mass coordinates, mass properties, inertia properties, member properties, damping factors, and initial conditions are presented in Appendix C. Differences in the modeling of the two separate impacts during the turnover are noted in Figure 38 and Table 13.

The larger model, shown in Figure 37, consists of 44 masses and 81 members. A description of the mass representations is presented in Table 14. The mass coordinates, mass properties, inertia properties, member properties,

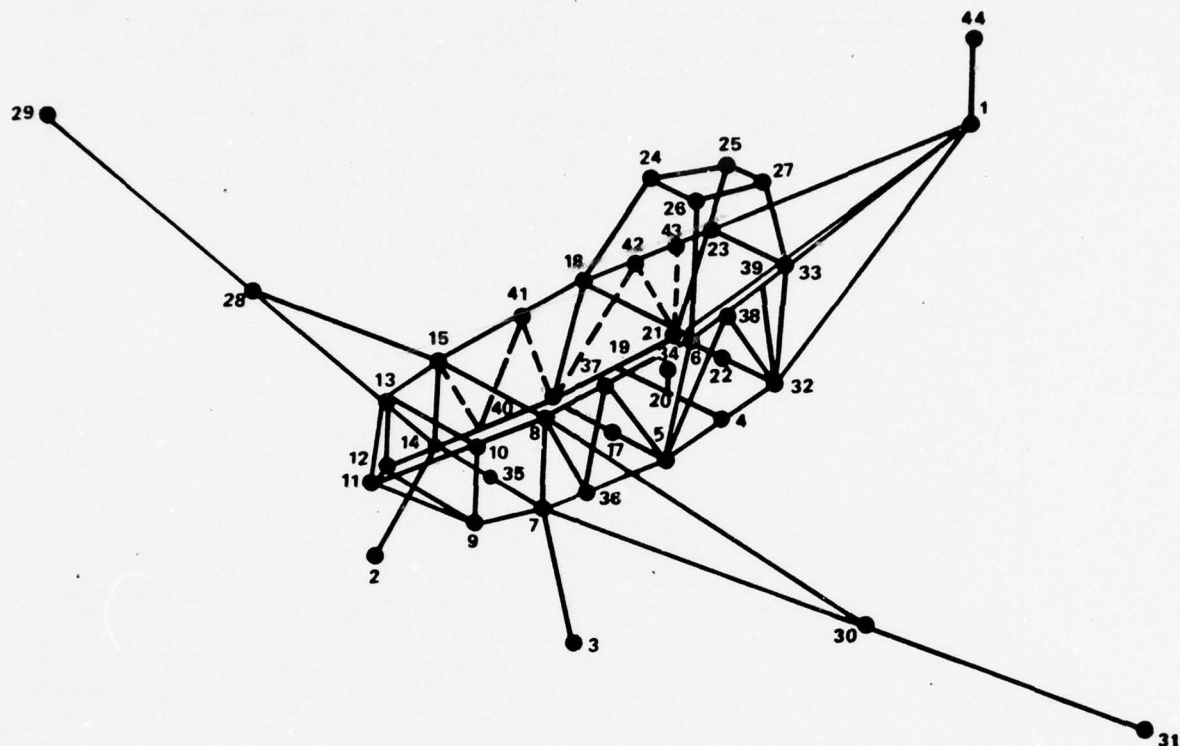


Figure 37. 44 Mass, 81 Member Math Model for Airplane B

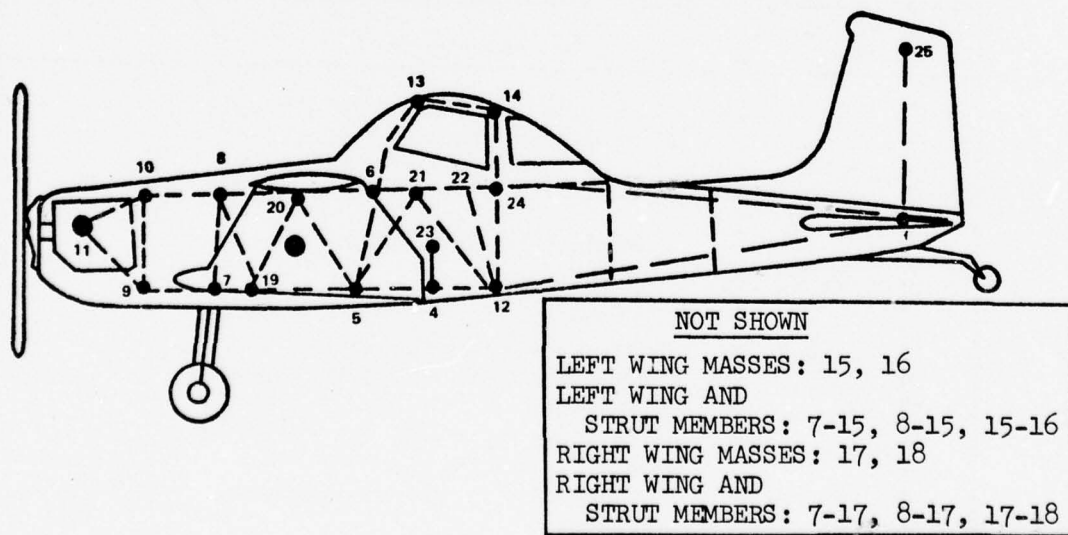


Figure 38. 25 Mass, 38 Member Math Model for Airplane B

TABLE 13 . MASS IDENTIFICATION FOR 25 MASS, 38
MEMBER AIRPLANE B MATH MODEL

Mass Point(s)	Representation
1	Tail Unit (including tail wheel)
2,3	Main Landing Gear Unsprung Mass
4	Floor Structure Mid Fuselage
5,6,7,8	Fuselage, Hopper Region
9,10	Firewall
11	Engine
12,24	Fuselage Aft Bulkhead
13,14	Forward and Aft Turnover Structure
15,16	Left Wing
17,18	Right Wing
19,20,21,22	Fuselage Welded Tube Structure
23	Occupant and Seat
25 (a)	Vertical Tail Unit
(a) This mass is used for the turnover impact only. It is included with mass 1 for the initial impact.	

TABLE 14 . MASS IDENTIFICATION FOR 44 MASS, 81
MEMBER AIRPLANE B MATH MODEL

Mass Point(s)	Representation
1	Tail Unit (including tail wheel)
2,3	Main Landing Gear Unsprung Mass
14,17,19, 20,22,35	Floor Structure, Forward and Mid Fuselage
5,6,7,8,14	Fuselage, Hopper Region
15,16,18	Firewall
9,10,12,13	Engine
11	Fuselage Aft Bulkhead
21,23,32,33	Forward and Aft Turnover Structure
24,26,25,27	Right Wing
28,29	Left Wing
30,31	Occupant and Seat
34	Fuselage Welded Tube Structure
36 thru 43	Vertical Tail
44 (a)	
(a) This mass is used for the turnover impact only. It is included with mass 1 for the initial impact.	

damping factors, and initial conditions are presented in Appendix C. The data shown in Figure 37 and Table 14 are used for both impacts during the turnover crash, except where noted.

As discussed in the presentation of the test data (Section 5.3.2.4), there is relatively little structural deformation in the initial impact except for the engine cowlings, and the applicable acceleration response data is limited. Consequently, of prime concern in the modeling of the turnover test is the requirement to reproduce the airplane large rigid body motions and the multiple impacts that occur. The forward fuselage impact is modeled using external springs. The ground is represented, in the locality of the impact point, as a mound of dirt with a face at 90 degrees to the ground plane having a coefficient of friction of 1.0, so that the line of action of the resultant forces acts on the airplane to slow down its motion as it approaches a vertical position. Other than the external springs that represent the crushing of the structure and ground plowing, the only nonlinear elements are the engine mounts (Figure 39). The wing tips and tail impacts and subsequent deformations are considered to have a minor effect on the resultant airplane motions and, accordingly, are represented as linear elements. Table 15 shows a comparison of the Airplane B and math model C.G. and mass properties. The math model C.G. is within 0.33 inches of the estimated airplane value. The inertia properties are within 12.8 percent of the estimated airplane properties. Actual airplane inertia properties for the test configuration are not available. The nonlinear curves used for the turnover crash test are shown in Figure 39. The procedure for performing the turnover crash analysis is the same as that described in the previous section for the stall-spin crash analysis.

Linear internal elements are used in the math models at all locations except as noted on the following page.

Location	25 Mass Model Nonlinear Members	44 Mass Model Nonlinear Members	Type of* Nonlinear Curve(s)
Engine Mount	9-11, 10-11	9-11, 10-11, 11-12, 11-13	3,4
Turnover Structure	6-13, 14-22 13-14	18-24, 6-26, 23-25, 27-33, 24-25, 26-27	3

*See page 66 for curve types

The nonlinear properties are based on the estimates of buckling strengths, available design load data and test data. Procedures for obtaining input data are described in the KRASH User's Manual (Reference 3). The standard nonlinear curves contained in KRASH (Section 4.3) are used. The results of the analysis and comparisons with test data are presented in Section 5.5.2.

TABLE 15. COMPARISON OF AIRPLANE B AND MATH MODEL C.G. AND MASS PROPERTIES

	Airplane B	Math ^(a) Model	Difference ^(b)	
			Inches	Percent
C.G.				
FS, inches	41.	41.33	0.33	-
BL, inches	.12	-.122	.142	-
WL, inches	2.0	2.248	.248	-
Weight, lb.	2475	2475	-	0
Moment of inertia, lb.-in.-sec. ²				
I _x (roll)	19700	17185	-	-12.8
I _y (pitch)	23250	25804	-	11.0
I _z (yaw)	38450	38680	-	0.6
(a) average of small and large model				
(b) $\frac{\text{model value} - \text{airplane value}}{\text{airplane value}} \times 100$				

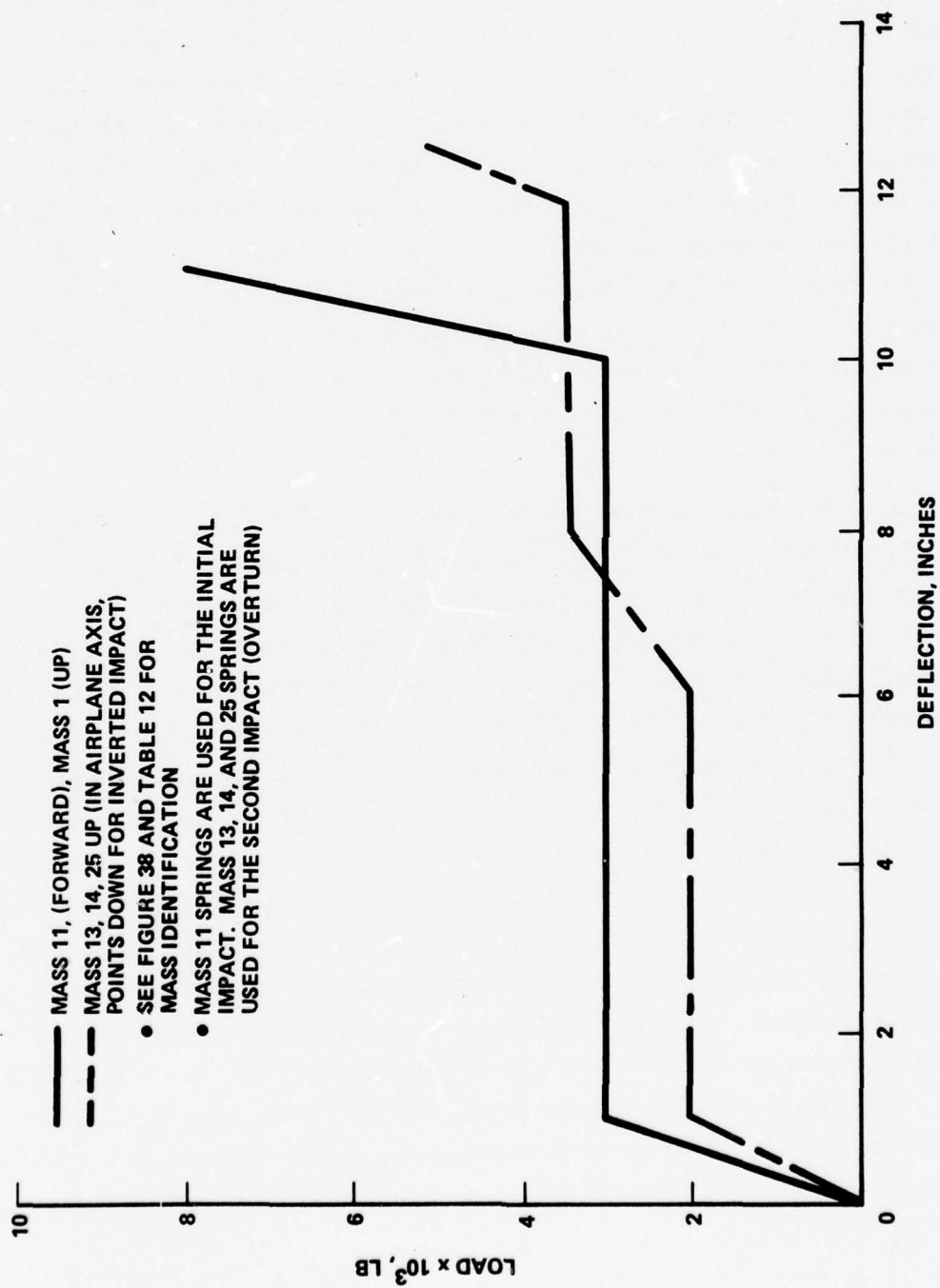


Figure 39. External Spring Load - Deflection Characteristics
Used in the Math Model for Airplane B

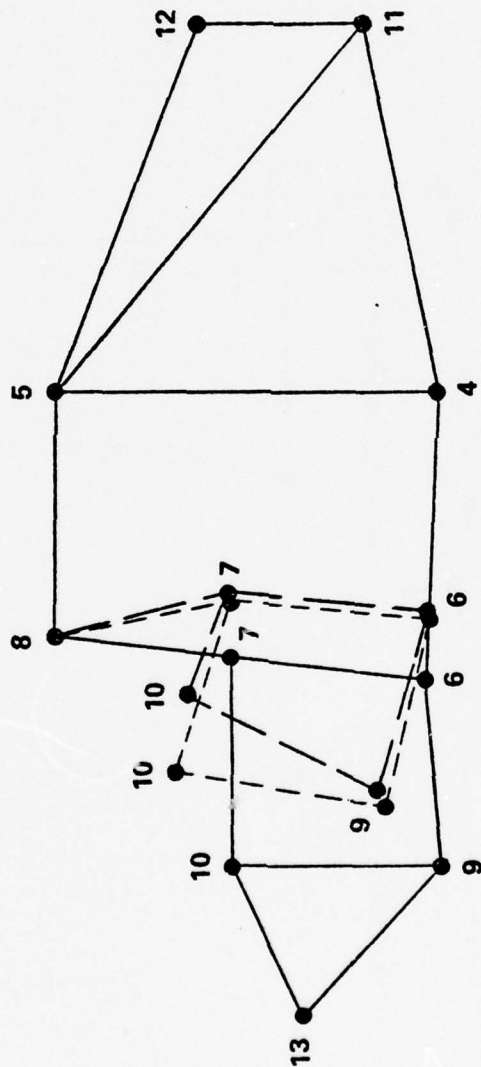
5.5 COMPARISON OF ANALYSIS AND TEST RESULTS

5.5.1 Airplane A Comparison

The crash condition analyzed consists of a longitudinal approach velocity of 45 feet per second into a 45 degree earthen slope. In the actual test, the nose gear fails aft immediately without appreciably altering the kinetic energy of the airplane. Preliminary analysis is performed to show that the nose gear fails in this manner and thereafter the analysis commences with the spinner impacting the slope. From inspection of Figures 21 through 26, it can be seen that the most significant vehicle damage is the crushing of the structure forward of and below the engine, and the subsequent rearward deflection and upward rotation of the engine. The upper engine mounts buckle and the forward cabin area deflects rearward substantially. Also highly visible, but not too significant from the occupant safety viewpoint, is the failure of the aft fuselage.

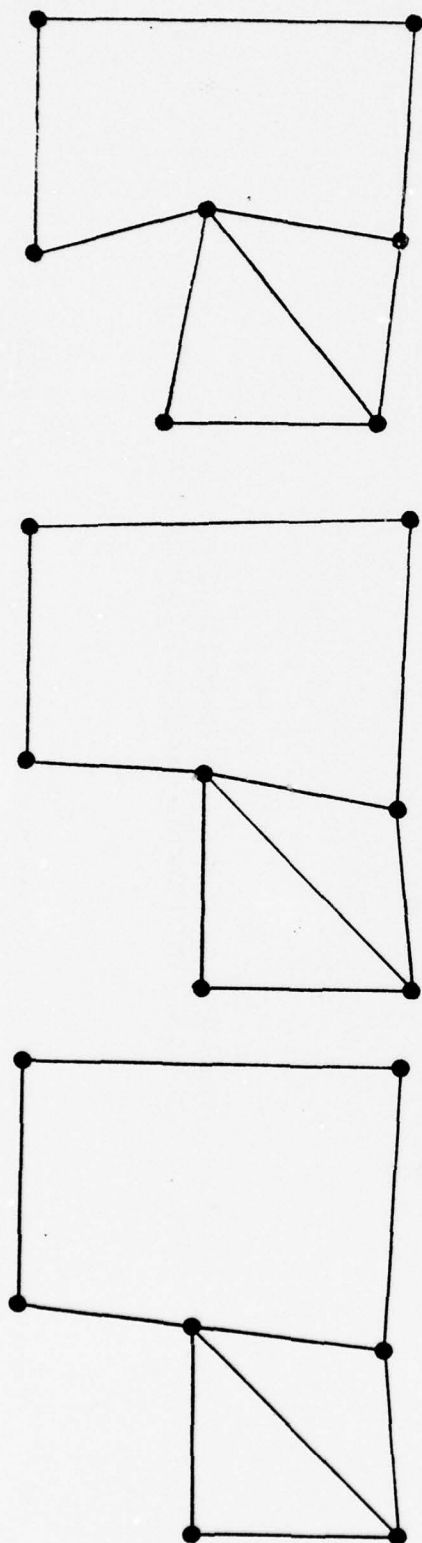
Figure 40 shows a comparison between test and analytical results of the post test deflected position of the engine and cabin structure. The test results are based on measurements made from photographs. The analyses results are based on the math model shown in Figure 35. Figure 40 demonstrates good overall agreement between test and analysis for the engine deflection and rotation and the cabin deformation. The analytically obtained deflected position corresponds to the end of the analysis at 0.16 seconds after spinner impact. Figure 41 presents the sequence of the vehicle deformations. The rearward deflection of the center of the forward door post (mass 7) and the shortening of the cabin floor (beam 4-6) occur quite early in the crash. The buckling of the engine mounts and the full deflection and rotation of the engine and upper cowl structure take a longer time to develop. The phasing of the significant internal beam element deflections is given in Figures 42 and 43. All the beam elements shown in Figures 42 and 43 utilize nonlinear KR curves that incorporate restiffening after the structural elements have been exposed to substantial deflection in the post failure region at low loads. The restiffening

————— = INITIAL POSITION
 - - - - - = POST-TEST CONFIGURATION
 - - - - - = FINAL ANALYTICAL POSITION (TIME = .160 SECONDS)



NOTE: (1) DIAGONAL ELEMENT 7-9 OMITTED FOR CLARITY
 (2) MASS 13 NOT SHOWN IN DEFLECTED POSITIONS FOR CLARITY

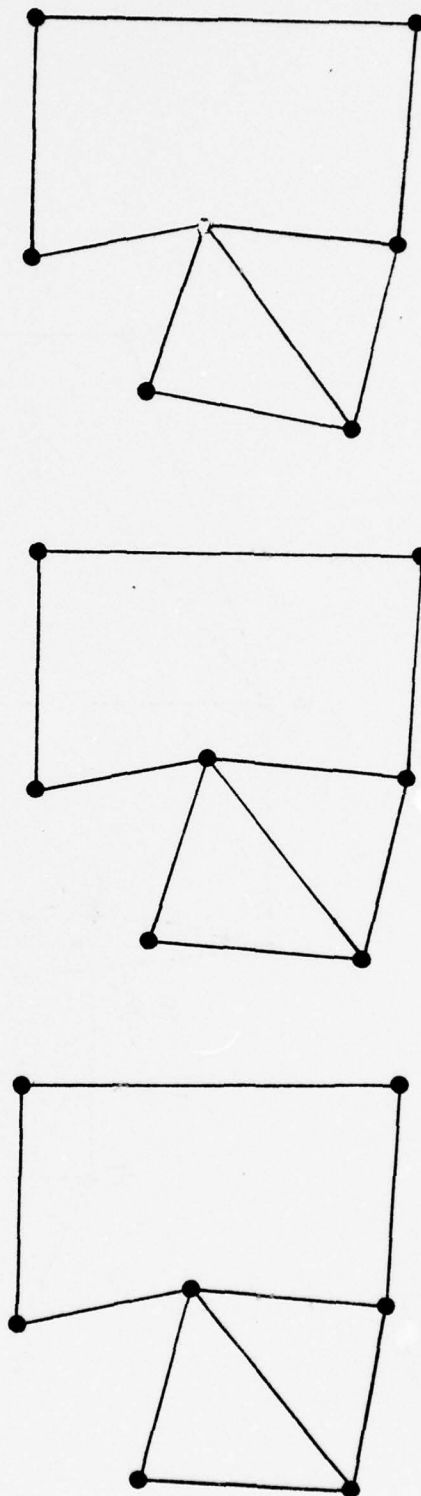
Figure 40. Comparison of Test and Analytical Airplane Deformations (Airplane A).



TIME = 0 SECONDS

TIME = .030 SECONDS

TIME = .054 SECONDS



TIME = .078 SECONDS

TIME = .108 SECONDS

TIME = .160 SECONDS

Figure 41. Sequence of Cabin Deformation Obtained from Analysis (Airplane A).

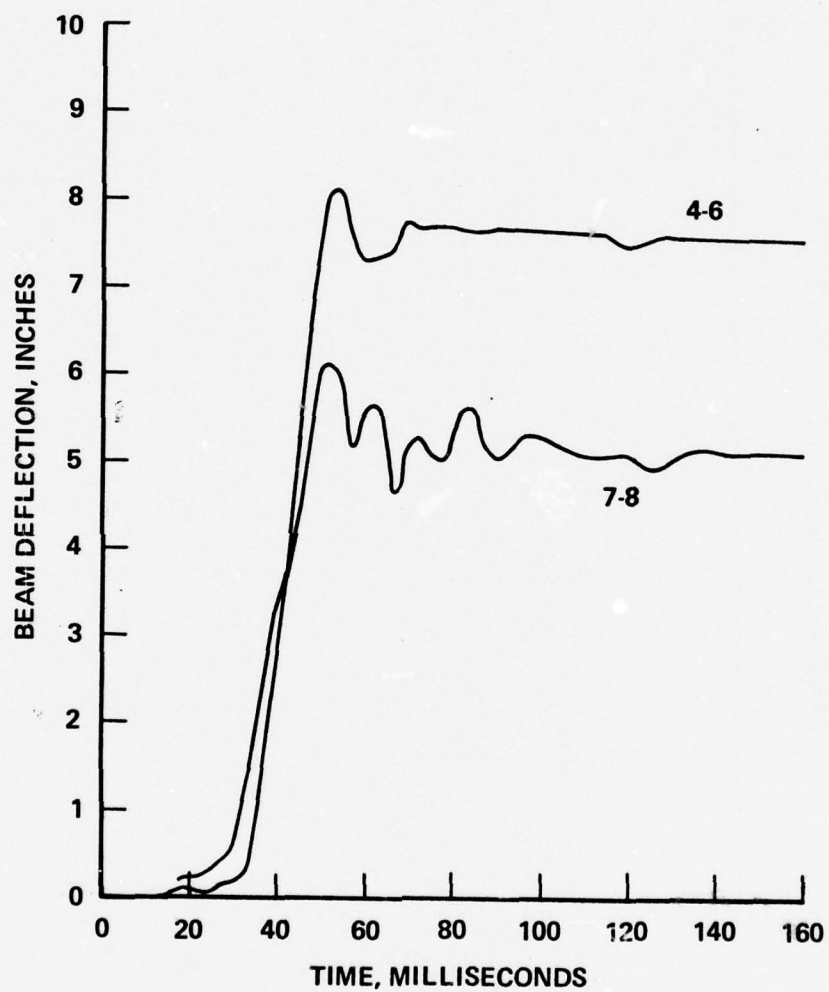


Figure 42. Internal Beam Deflection Time Histories Obtained from Analysis, Cabin Area (Airplane A)

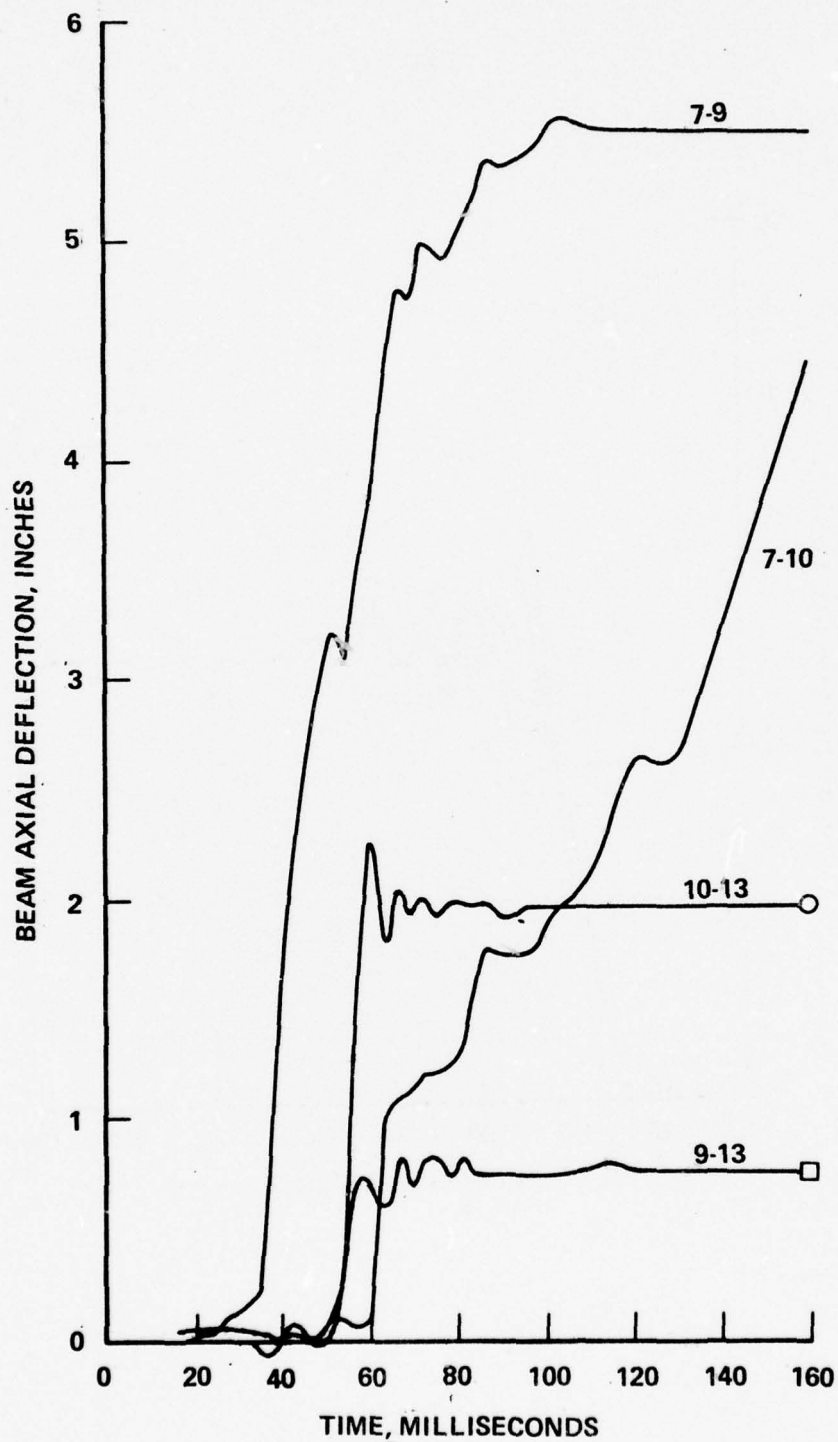


Figure 43. Internal Beam Deflection Time Histories, Forward Fuselage Structure and Engine Mounts Obtained from Analysis (Airplane A)

represents the crushing of structure in a confined region. Test data from Reference 4 shows this phenomenon and the observations from those tests combined with the geometry associated with the airplane structure are used to determine when restiffening can occur. All the internal structural elements shown in Figures 42 and 43 have reached the restiffening deflections except the upper cowl structure (beam 7-10). However, from the trend of the history of the axial deflection of element 7-10 (Figure 43), it is evident that its restiffening deflection of approximately 9 inches would be reached by 0.25 second after spinner impact. This additional deflection would further improve the correlation between the test and the analysis final deflected position shown in Figure 40.

Figure 44 shows a comparison of analytical and test results for cabin deformation, consisting of the rearward deflection of the forward door post. The correlation at WL 19.1, which is near the top of the door frame, is quite good. At WL 2.4, near the center of the door, the correlation is good in the initial loading region, but the test results indicate a peak deflection of around 10 inches at 140 milliseconds, with a final deflection of 9 inches, while the analysis predicts about 7 inches constant beyond 100 milliseconds. This is consistent with the results shown in Figure 40, which indicate that the analytical aft deflection of mass 7 is less than the test results.

Figure 45 shows the time histories of the external spring deflections. Springs 13-1 and 13-3 (Figure 36) represent the airplane structure forward of and below the engine. Also incorporated in the load-deflection curves for these springs is an approximation of the compliance or softness of the ground. The springs at mass 9 are much shorter and absorb far less energy than those at mass 13. From Figure 45 it can be seen that the external springs at mass 13 develop their peak loads within 35 milliseconds and then unload gradually during the remainder of the run having a secondary peak at 90 milliseconds. The springs at mass 9 contact later but also reach an initial peak at 35 milliseconds, and then reload later to a second peak at 90 milliseconds.

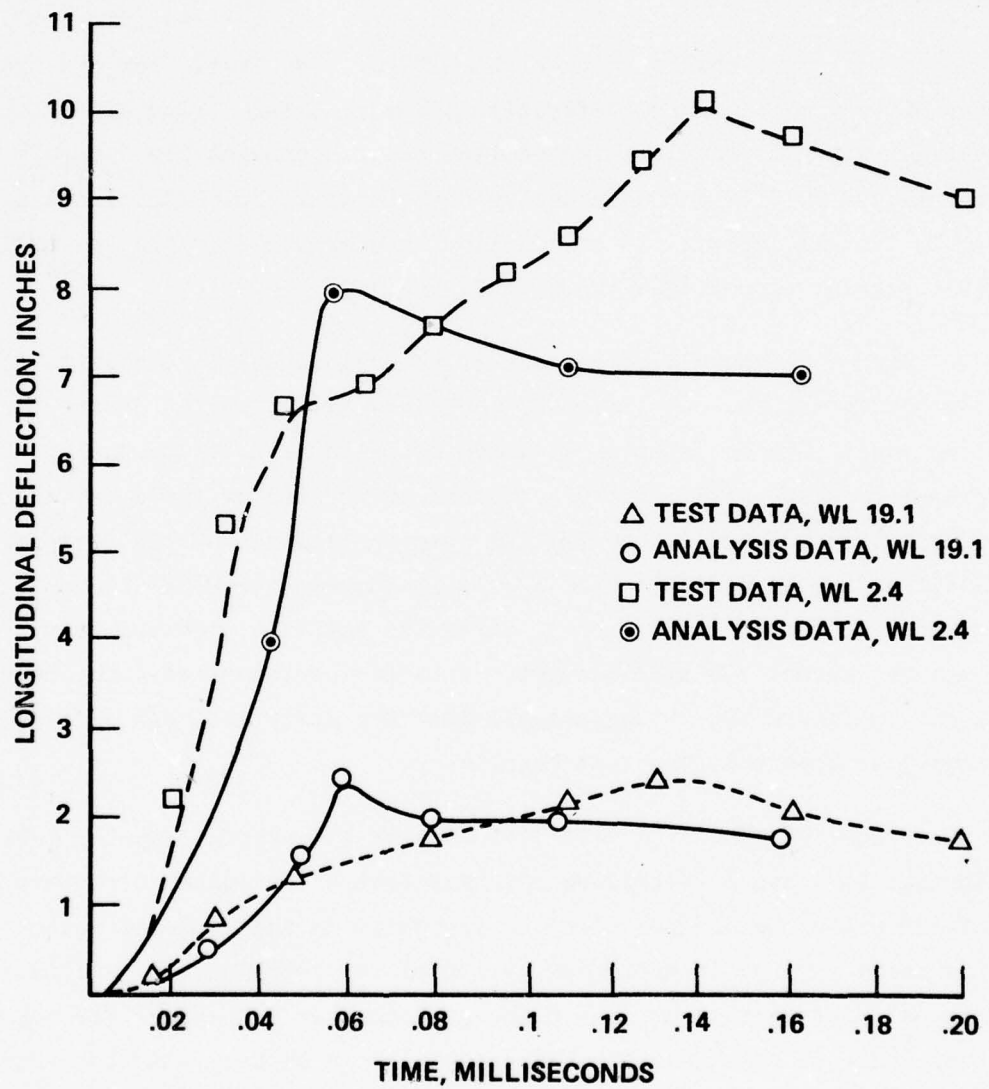


Figure 44. Comparison of Analysis and Test Data for Cabin Deformation (Airplane A)

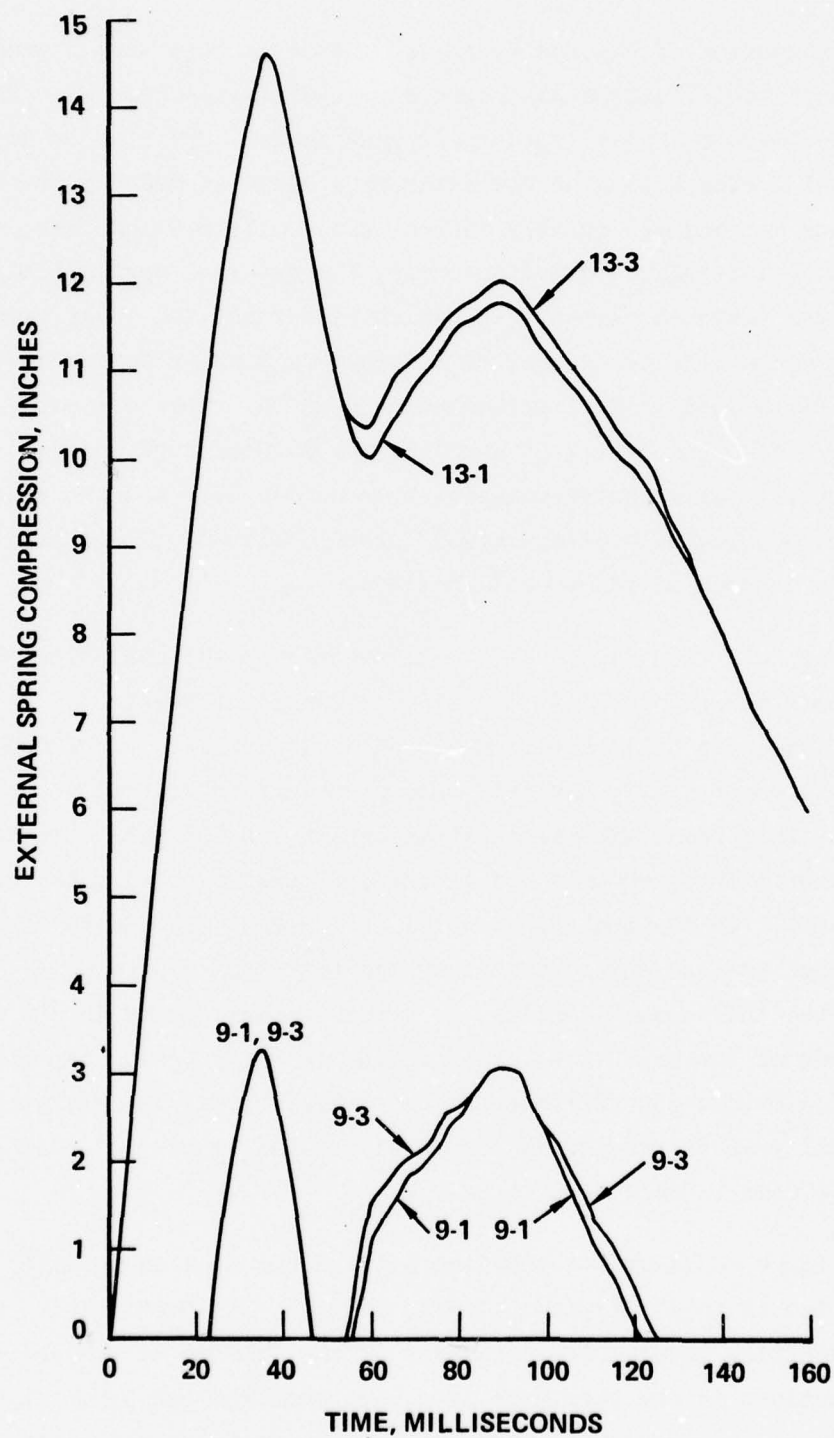


Figure 45. External Spring Deflection Time Histories Obtained from Analysis (Airplane A)

Inspection of Figures 42 and 43 indicates that the internal element structural deformations all begin after 30 milliseconds when the external springs have nearly developed their peak loads. The line of action of the external forces acting on the external springs at mass 13 is such that elements 4-6 and 7-8 quickly deflect aft, while 6-9 and 7-10 retain their integrity initially. Simultaneously, the external spring loads at mass 9 cause the diagonal element 7-9, which represents the shear capability of the fuselage side structure, to deform. Only after this element has deflected almost to its maximum value does the upper element 7-10 begin to shorten. Once 7-9, 7-8, and 4-6 have all deformed sufficiently to reach their restiffening regions, both member 7-10 and the upper engine mount 10-13 begin to deform significantly, with 10-13 buckling rather quickly between 50 and 60 milliseconds.

The tail cone fails at 75 milliseconds in the analytical model, with the lower element 11-17 failing in compression (buckling). At the time of failure, the tail section has bent downward just over 2 inches. After the failure of 11-17, the tail cone structure is reduced to only element 12-17. This beam fails in vertical bending at 108 milliseconds. The tail cone failure sequence and timing are consistent with the crash test film data. In the analytical model, no attempt is made to simulate the very large deflections and rotations of the tail cone observed in the crash test. While the tail cone "flapping" is a predominant motion in the motion pictures of the crash test, this motion is not of great importance to the question of occupant survivability. Therefore, in the analytical model, the tail cone is treated as completely failed (ruptured) once the buckling failure mode is well established.

Figure 46 shows a comparison between the test and analytical time histories of total airplane kinetic energy. The test results are based on velocities deduced from analysis of the film data. Minor velocity fluctuations in the test data have been smoothed out prior to calculating the kinetic energy. The agreement between analysis and test results shown in Figure 46 is quite good, and indicates that the energy absorption in the analytical model is very reasonable. Two percent structural damping was used for all the members.

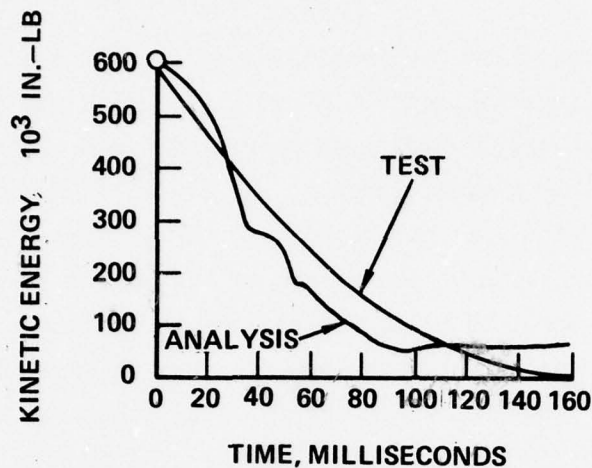


Figure 46. Comparison of Test and Analytical Kinetic Energy Time Histories (Airplane A)

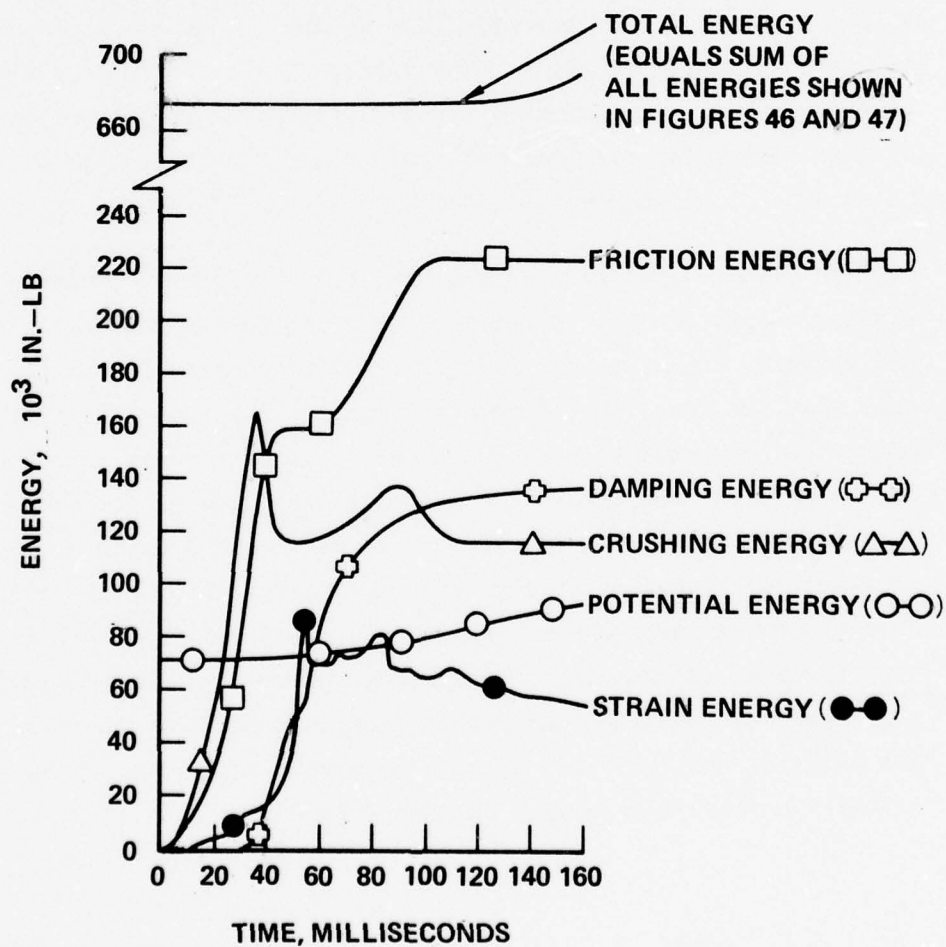


Figure 47. Time Variation of Analytical Energy Components (Airplane A)

Figure 47 illustrates the time variation of the various energy terms which account for the reduction of the kinetic energy in the analytical model. The terms shown are the friction energy (FE) and crushing energy (CE) associated with the external springs, the strain energy (SE) and damping energy (DE) of the internal beams, and the potential energy (PE) of the vehicle. Figure 47 shows the nature of the energy absorption in the system. Prior to about 40 milliseconds, the entire energy absorption is due to the friction and crushing energies of the external springs. From 40 to 60 milliseconds the strain energy of the internal beams increases from virtually zero to its peak value. The damping energy also increases rapidly during this time span, but continues to increase significantly during the remainder of the analysis. There is a slight increase in the potential energy during the run that results from the vehicle riding up the earthen slope. The energy absorption results of Figure 47 are consistent with the deflection time histories observed earlier; initially the external springs are compressed, driving the internal beams which respond somewhat later.

In Figure 47 it can be seen that both the friction energy and the damping energy are monotonically increasing quantities, while the strain and crushing energies peak and fall. This behavior is attributed to the fact that the friction and damping energies are both dissipative; the energy is converted to heat and cannot be reintroduced into the system. The behavior of the strain and crushing energies, on the other hand, results from energy storage in structural elements which are partially elastic, and therefore part of the peak energy absorbed is reintroduced into the system when the members unload elastically. The flat portion of the friction and crushing energy curves between 45 and 60 milliseconds and beyond 115 milliseconds result from the fact that in these regions all external springs have unloaded to a zero load level; between 60 and 115 milliseconds the springs on mass 9 have reloaded.

At the end of 160 milliseconds of analysis the total energy has increased by only 2.5 percent from its original time = 0 value which indicates that the math model is behaving in a stable manner.

Also available from the output of program KRASH is the spatial distribution of the strain energy at each time print. Table 16 is a

TABLE 16. STRAIN ENERGY SPATIAL DISTRIBUTION, AIRPLANE A ANALYSIS									
	Percentages of Total Strain Energy								
	Engine Mounts		Firewall & Fuselage Structure Aft of the Firewall				Mid Cabin		
Beam Time	9-13	10-13	6-9	7-9	7-10	9-10	4-6	6-7	7-8
.012	22.8	16.5	6.3	0	4.5	2.28	19.3	13.4	11.3
.018	7.6	9.6	1.8	0.2	6.2	1.66	16.1	28.0	20.1
.024	2.3	12.0	0.4	0.8	8.7	1.11	6.3	37.1	24.2
.030	0.2	2.8	3.8	6.4	2.5	0.24	19.6	31.4	25.7
.036	9.0	5.2	5.3	8.2	0.9	1.32	25.6	3.2	30.3
.042	4.0	1.6	23.1	6.1	7.6	1.86	17.6	1.9	16.0
.048	2.1	2.0	20.3	3.7	9.5	0.78	9.4	3.0	23.7
.054	3.2	2.6	12.0	2.5	6.8	0.52	20.0	14.1	19.8
.060	8.6	19.8	11.2	1.6	10.5	4.72	7.4	1.6	9.7
.066	4.0	14.9	15.2	1.5	16.3	3.20	6.3	1.6	9.6
.072	11.7	7.6	18.3	1.7	16.7	1.99	6.9	4.4	8.2
.078	8.7	6.2	13.2	2.0	16.3	4.14	7.2	4.9	14.1
.084	7.4	8.1	15.8	1.5	15.1	2.23	4.2	6.5	11.1
.090	6.8	11.0	18.5	1.9	18.6	3.30	5.2	4.1	10.1

summary of the time variation of the percentages of the total strain energy accounted for by the internal beams that absorb most of the energy. Figure 48 is a plot of the data from Table 16, where the percentages from the individual beam elements in each airplane region have been added. While the oscillations in Figure 48 are complex, the essential trends are that the strain energy is initially concentrated primarily in the cabin region, and during the crash the strain energy concentration shifts to the fuselage structure aft of the firewall (members 6-9, 7-9, 7-10). The percentage of the total strain energy in the cabin region reduces from a peak of 75 percent at 30 milliseconds to 20 percent at 90 milliseconds. During the same time span the strain energy associated with the fuselage aft of the firewall has risen from approximately 12 percent to 40 percent of the total strain energy. During this time period the strain energy associated with the engine mounts has oscillated about a fairly constant value of 25 percent of the total strain energy. The energy attributed to cabin deformation is greater than the contribution from the fuselage or engine structure deformation up until 60 milliseconds after impact. This result is consistent with the analytical results shown in Figures 41 through 44.

While it might be expected that the strain energy concentration will start near the impact region and flow rearward during the crash, the actual concentration pattern depends on the relative stiffnesses of the various regions of the airplane. For this particular airplane the film analysis indicates that structural buckling occurs in several regions at or shortly after impact. For example, from Figure 20, which provides a partial sequence of the crash event, at approximately 20 to 60 milliseconds after impact there is noticeable damage in the cabin and the structure forward and aft of the cabin. At 100 milliseconds after impact the deformation has progressed significantly. Thereafter, the damage to the fuselage structure aft of the firewall and forward of the cabin continues to develop to a much greater extent than in the cabin area itself. The film analysis shows the maximum cabin deformation has been passed while the fuselage structure aft of the firewall continues to deform. While the computer analysis shows that the maximum cabin deformation transpires earlier than

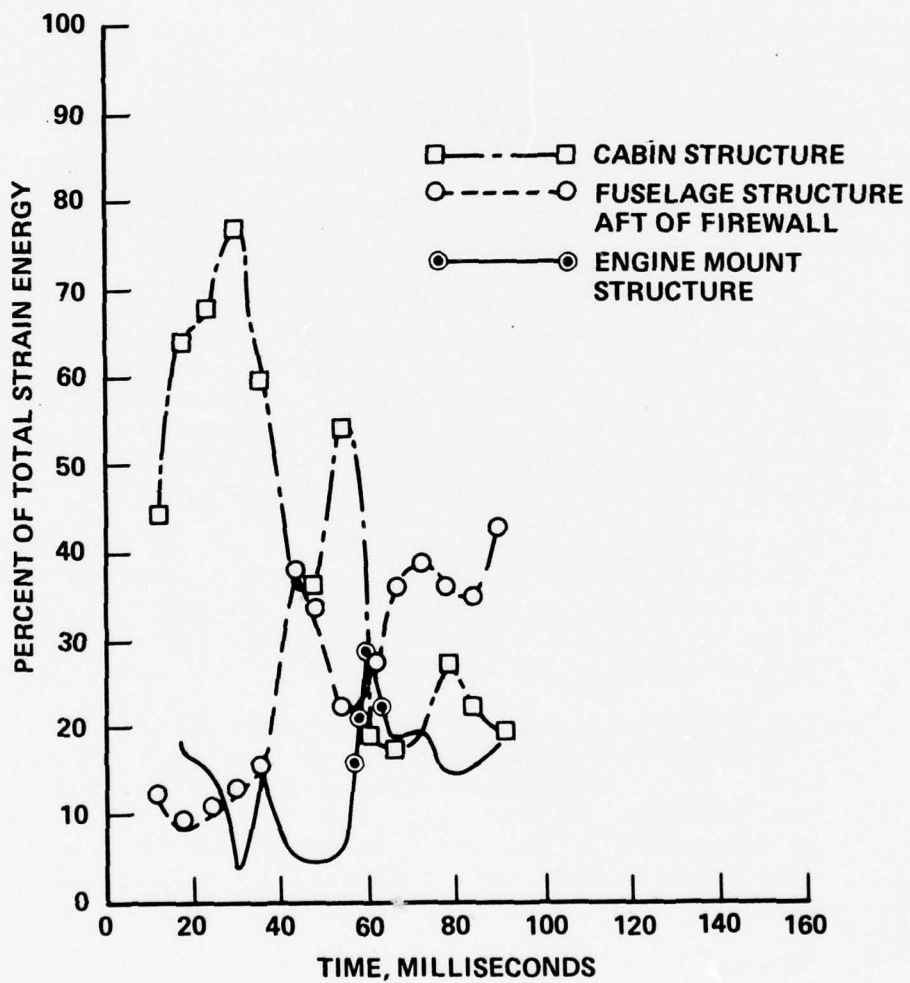


Figure 48. Time Variation of Strain Energy by Region Obtained from Analysis (Airplane A)

the film analysis indicates, it appears that the math model shows a reasonably good relationship between the sequence of events as depicted by the concentration of energies.

Figures 49 and 50 show the cabin floor longitudinal and vertical acceleration histories, both analytical and test results. The analytical results are for mass 4. In both cases, the test results reach their peak in 12 milliseconds, whereas the analytical peaks occur from 50 to 75 milliseconds. Figures 49 and 50 indicate a large discrepancy between test and analytical accelerations. However, examination of the test sequence and related data indicates that the measured test results are most likely not valid for the following reasons.

1. As discussed in Section 5.3.1.4 all the accelerometer signals appear to be activated simultaneously. Considering that the accelerometers measured vertical and longitudinal responses for the structure and occupant (pelvis and head) at different locations and directions and with different individual frequency responses, it is highly improbable that the peak responses for all would occur at the same time and with the same pulse shape.
2. The measured test peak acceleration occurs at approximately 12 milliseconds after impact while the sequence of the crash test (Figure 20) indicates that a maximum response might occur at or after 40 to 60 milliseconds. The analysis shows peak responses between 50 and 75 milliseconds.
3. If, in fact, the measured test responses are valid, it would represent a very localized response appropriate to a very small mass. If the test acceleration pulse acted on the entire vehicle, the initial forward velocity of 45 ft/sec would be stopped in 20 milliseconds. From the film data it appears that the forward velocity is stopped in approximately 160 milliseconds, at an overall average rate of deceleration of about 8.7 g's.
4. Data presented in Reference (12), showing the magnitude of impact velocities and acceleration pulses for a 95th percentile accident condition for light fixed-wing aircraft, supports the analytical results. The 95th percentile longitudinal velocity is given as 50 ft/sec and the associated peak acceleration pulse is 30 g's and 24 g's in the cockpit and passenger compartment, respectively. Furthermore, the duration of the pulse is given as over 100 milliseconds. While the results obtained in this analysis consist of five or six individual separate cycles, the envelope of these cycles has a duration of about 100 milliseconds.

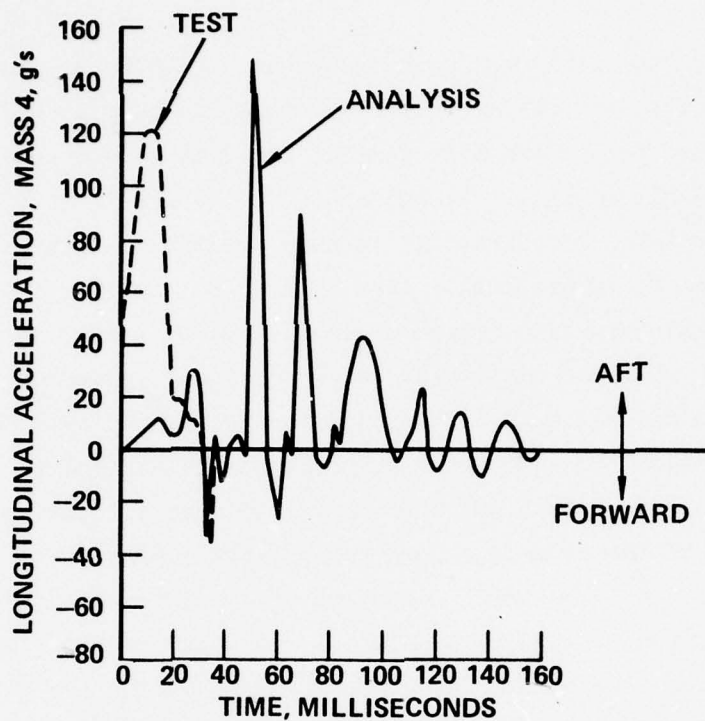


Figure 49. Cabin Floor Longitudinal Acceleration (Airplane A)

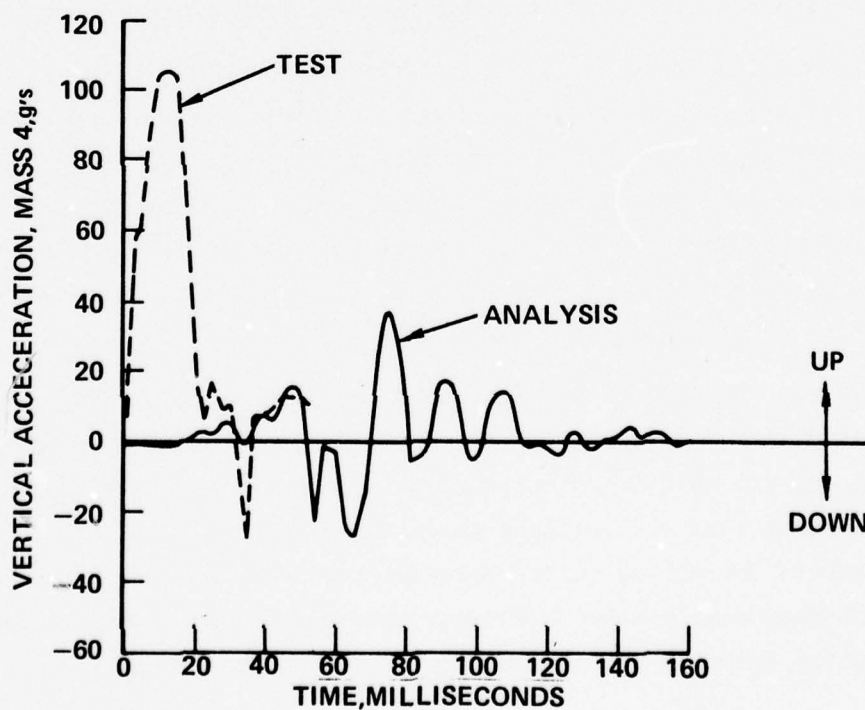


Figure 50. Cabin Floor Vertical Acceleration (Airplane A)

In Figure 49, the first two sharp peaks at 51 and 69 milliseconds result from the bottoming of internal beam 4-6. If the peak acceleration values at these two points are disregarded, the peak acceleration then becomes 43 g's longitudinally. It appears that the restiffening process for beam 4-6 is modeled too abruptly; a more gradual restiffening would lower these peaks to substantially less than 20-30 g's. If this were done, the envelope of the resulting responses would be about 30-40 g's peak with a duration of 100 milliseconds, which is in reasonable agreement with the data contained in Reference 12. The restiffening element type used for beam 4-6 is a standard NP = 9 curve (see section 4.4.6), and at present is internally coded such that the bottoming stiffness is equal to the linear stiffness of the element. Furthermore, the element behavior is similar to an NP = 8 curve until bottoming occurs. The results of the airplane A comparison between test and analysis indicate that these limitations are too inhibiting. Consequently, the coding for this type of curve will be changed for the Task II effort to allow the user more flexibility in modeling this type of behavior. In particular the user will be able to define as input data the post-failure load-deflection behavior and the stiffening after structural confinement occurs.

The vertical acceleration at mass 4 (Figure 50) indicates a peak acceleration of approximately 38 g's with a long term response of approximately 70 milliseconds (40 to 110). The vertical acceleration pulse is in response to a longitudinal impact, thus it is difficult to relate this data to that given in Reference 12 which describes a vertical response to vertical impact. In that situation the Reference 12 data indicates a peak acceleration of 48 g's for 54 milliseconds duration.

The responses noted in Figures 49 and 50 are indicative of structure responding with a frequency in the 50-60 Hz range. The type of structure used in general aviation aircraft fuselage design is relatively light and stiff and may very well respond as shown by the analysis. It is also important in the evaluation of occupant survival to recognize that the occupant responds in a low frequency mode (6-12 Hz.). Thus pulses with frequencies above 25 Hz. have little effect on the occupant.

5.5.2 Airplane B Comparison

The Airplane B crash sequence is depicted in Figure 51 from initial impact (time = 0) to final position (time = 1.66 seconds). The modeling of the initial impact is performed for the first 80 milliseconds for the airplane positions shown in Figure 51 (a) and 51 (b). For the second impact, the sequences shown in Figure 51 (e) and 51 (f) are used. In the initial impact the ground is modeled with a 90 degree slope in the local region where the forward fuselage impacts. The forward fuselage has two external springs, one along the longitudinal axis of the airplane, and the other normal to the airplane longitudinal axis. Both external springs emanate from the engine mass (mass 11, Figures 37, 38) and represent the characteristics of the confined terrain deformation and spinner and cowl structure crushing. While the external spring is symbolized by a point contact it in fact represents a much broader area of contact. In this particular case, both the contact area and the region making ground contact change as the airplane rotates about the nose. The analytical model reproduces the initial crushing of the forward section of the fuselage with the longitudinal spring and also the subsequent contact of the upper cowl with the top of the slope as the airplane rotates over onto its top side. The analytical results show that the upper engine mount buckled. As stated in Section 5.3.2.4, the upper left engine mount failed during the test. However, since this mount had been previously repaired, the actual strength of the mount is not known. Outside of extensive damage to the upper cowl and hopper skins during the test, no other damage or failure was noted that could be attributed to the initial impact. In this respect the analytical model results agree with the test results.

Table 17 presents a comparison of analytical and test results for the initial impact of the forward fuselage section with the terrain. The test results are based on analysis of the motion pictures taken during the test. The film analysis is based on a 24 frame/second film speed. This film speed provides only one frame of data for every 40

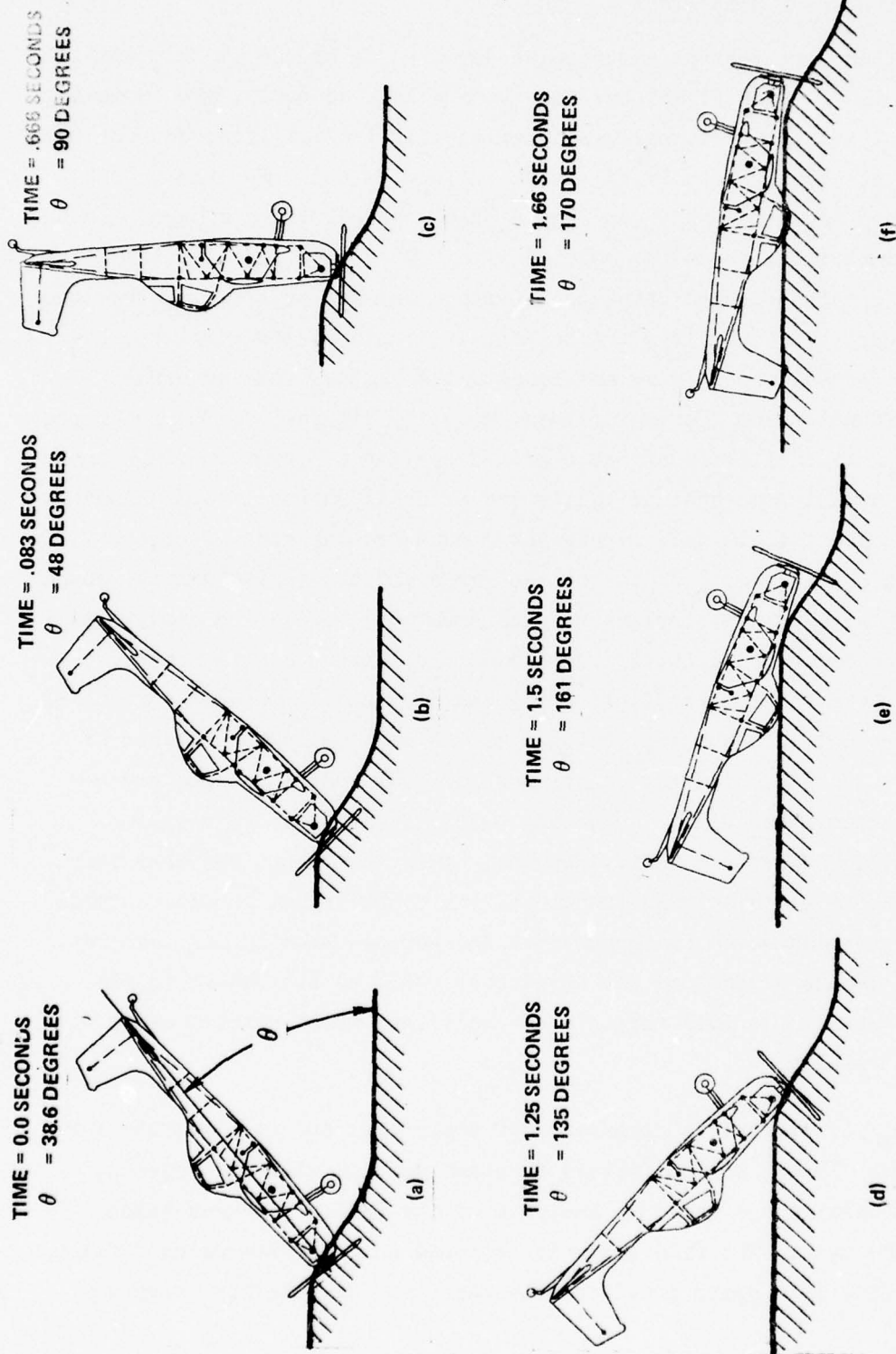


Figure 51. Crash Test Sequence of Airplane B as Determined from Photographs

milliseconds of motion, which is an order of magnitude slower than normally used in crash analysis. Normally, if available, 200 to 500 frame/second film speed is used to determine the details of a crash test. The results of the film analysis for the test sequence is presented and described in Appendix C. From Table 17 it can be seen that the rigid body rotational motion of the airplane is depicted with good accuracy (less than 1.5 percent) when compared to the results of the test film analysis for the 40 milliseconds involved in the initial impact. The energy that is absorbed, is mostly in crushing and friction. The kinetic energy obtained from the analysis is within 8 percent of the estimated kinetic energy at 40 milliseconds. At approximately 70 milliseconds after the impact the analysis indicates a buckle failure of the upper engine mount. At this time the c.g. longitudinal acceleration (average of masses 5, 6, 7 and 8, Figure 38) is computed to be 18.4 g's which is higher than the test peak value of 11.8 g's. Higher c.g. airplane axis vertical accelerations (20 g's) noted in the test results are not obtained by the analysis. The analysis shows vertical acceleration values less than the longitudinal results. This situation seems appropriate considering the orientation of the airplane for the first 80 milliseconds. As the airplane rotates onto the overturn structure (Figure 51 (c) and 51 (d)) higher c.g. airplane axis vertical acceleration may occur. At this point the energy absorbed by the airplane structure and ground obtained from the analysis is substantially higher than indicated by the data from the film analysis, although overall rotation of the airplane is within 1.5 percent of the estimated test value. It would appear that the test results, if adequate accuracy is assumed, would indicate closer agreement in energy and less agreement in motion than shown. The lack of definition of acceleration pulses (shape, duration and phasing) from the test results makes it difficult to quantify the comparison between analysis and test beyond the type and extent of structural damage and airplane motion.

The analytical results are influenced by the manner in which the deformation of the terrain is modeled using external springs. If the ground contact surface were concrete instead of soft dirt, there would be no

TABLE 17. COMPARISON OF AIRPLANE B ANALYTICAL AND TEST RESULTS FOR THE INITIAL IMPACT CONDITION

	Test	Analysis	Percent Difference (a)
Initial Rotation, θ (Degrees)	38.6	38.6	-
Initial Rotational Velocity, $\dot{\theta}$ (Degrees/Sec.)	106.	106.	-
Rotation, θ , at Time = .040 Sec. (Degrees)	42.8	42.7	.23
Kinetic Energy prior to Impact, Time = 0 (in.-lbs)	2.611×10^5	2.607×10^5	.15
Kinetic Energy at Time = .040 Sec. (in.-lb)	2.42×10^5	2.234×10^5	7.7
(a) (Test Value - Analytical Value) X 100/Test Value			

TABLE 18. COMPARISON OF AIRPLANE B ANALYTICAL AND TEST RESULTS FOR THE TURNOVER INVERTED IMPACT

	Test	Analysis	Percent Difference (a)
Initial Rotation, θ (Degrees)	162.	162.	-
Initial Rotational Velocity, $\dot{\theta}$ (Degrees/Sec.)	89.	89.	-
Rotation, θ , at Time = .040 Sec. (Degrees)	165.7	165.6	0.06
Change in Rotation, $\Delta\theta$, at Time = .040 Sec. (Degrees)	3.7	3.6	2.7
Kinetic Energy Prior to Impact, Time = 0 (in.-lbs.)	7.19×10^4	7.106×10^4	1.17
Kinetic Energy at Time = .040 Sec. (in.-lbs.)	5.18×10^4	5.901×10^4	-13.9
(a) (Test Value - Analytical Value) X 100/Test Value			

appreciable interaction between the ground and the structure. The analysis provides for the structure to penetrate the earth as much as 10 inches, wherein the earth is modeled softer than the structure. Thereafter the spinner and cowl structure influence the stiffness of the external spring that is used. The interaction between the terrain and the structure is difficult to define, which is further complicated by the fact that the area of contact is changing as the airplane penetrates and rotates. Analytical studies described in Reference 4 in which program KRASH was used to assess the effect of load-deflection variations on the response indicate that the results are most sensitive to the modeling of structure wherein confined crushing takes place. Generally, when crushing occurs the stiffness of the structure (or terrain) increases rapidly as it is compressed.

The impact of the turnover structure with the ground is modeled as depicted in the sequences shown in Figure 51 (e) and 51 (f). For the second impact, Figure 51 (e) represents the airplane position at time zero. In this condition, external springs are applied at masses 13, 14 and 25 as shown in Figure 38 (masses 24, 25, 26, 27, and 44, Figure 37). From Table 18 it can be seen that the analytical results compare favorably with test results for the period of time over which the high speed film could be analyzed. The rotation and the kinetic energy obtained by analysis are shown to be within 2.7 percent and 13.9 percent, respectively, of the test results obtained from film analysis. The analysis further shows that at 80 milliseconds after time zero, for the inverted impact, the kinetic energy has been reduced to approximately 23 percent of the kinetic energy available in this impact. The analysis further indicates that failure of the forward turnover structure, member 6-13, Figure 38 occurs. The test results indicate that a failure of the forward structure occurred during the test. While test data is not available for making a quantitative evaluation of cabin volume change, the films of the test and the photographs of the post test airplane condition (see Figure 31), indicate that little or no cabin volume change occurred which is consistent with the results of the analysis.

In addition to providing data for assessing the capabilities of the analysis to predict the behavior of an airplane during a multiple impact with large rigid body rotations, the tests also provide data concerning airplane/soil interaction. The test and analytical results agree in that the major energy absorption occurs in the action of the ground and the structure in contact with the ground. The lack of distortion of structure and minimal structural failure indicate very little (almost negligible) dissipation of energy as a result of permanent strain.

The analysis of this crash test, as well as the airplane A crash test, indicates that estimating the proper terrain representation, other than hard surfaces such as concrete and asphalt, is difficult because of the lack of terrain and airframe interaction data. While KRASH has provisions (external linear and nonlinear springs, generalized impact surface and ground friction) to utilize available terrain data, it should be recognized that terrain and airplane interaction is a complex phenomenon, which at best can only be approximated in KRASH at this time.

Of interest is the economics of running small models, if appropriate. Table 19 shows a comparison of results for the 43 mass and 24 mass models used for the initial impact. Since the crash in this particular case is symmetrical, the smaller model can be used to an economic advantage, if the accuracy of results is acceptable. As can be observed in Table 19 the results agree within 6 percent while the larger model requires more than twice the time (and cost) to perform the same analysis.

TABLE 19. COMPARISON OF RESULTS FOR THE 43 MASS
AND 24 MASS AIRPLANE B MODELS

	24 Mass 37 Member Model (a)	43 Mass 80 Member Model (a)	Percent Difference (b)
Incremental Rotation (Degrees)	4.12	3.90	-5.6
Kinetic Energy (in.-lbs.)	2.23×10^5	2.187×10^5	-2.0
External Spring Deflection (inches)			
Longitudinal	8.93	9.07	1.5
Vertical	7.00	7.42	5.7
Computer Time (hrs)	.0455	.097	53.1
(a) Time = .040 seconds			
(b) (Large Model Value - Small Model Value)X 100/Large Model Value			

5.6 ASSESSMENT OF PROGRAM KRASH

In addition to performing comparison studies between analytical and test data using two general aviation airplanes, other portions of the Task I effort directly and indirectly provide information for assessing the capabilities of program KRASH to assist in establishing the crash-worthiness of general aviation airplanes. These related efforts include the determination of the general aviation industry's computer capability, improvements in the ease and cost of operating the program, as well as the availability of structural data and the methods to be used for obtaining data.

The comparisons of two different general aviation airplane configurations subjected to two probable accident conditions along with a previous correlation using full scale crash test data (Reference 3) and accident results (Reference 15) have shown that program KRASH can provide satisfactory data to:

- o Facilitate an evaluation of occupant injury assessment by providing the floor pulse to the occupant seat, describe structural deformation in and around the occupiable region, and provide a Dynamic Response Index (DRI) reading,
- o Meet the general aviation airplane design requirements by providing multidirectional force, acceleration, velocity and deflection data,
- o Account for large nonlinear behavior of different types of structure including failure modes, loss of structure, and an evaluation of member directional stresses,
- o Treat probable crash conditions taking into account impact velocities, attitude, angular rates, terrain and position of the aircraft relative to the terrain,
- o Describe different general aviation airplane configurations including low-wing, high-wing, single-engine and twin-engine types,
- o Simulate significant portions of a crash wherein multiple impacts are involved, and
- o Describe the temporal and spatial distribution of energy throughout the crash including mass kinetic and potential energy, member strain and damping energy and structural crushing and the ground friction associated energy.

In addition KRASH has been modified to standardize many parameters, simplify input data requirements and clarify output data with the use of English symbols where appropriate. All modifications are briefly described in Section 4 of this report and comprehensively detailed in Section 1 of Reference 13.

The program has demonstrated its capability to treat a wide variety of vehicles and crash situations. However, as is the situation with any analytical approach, the accuracy that can be achieved depends to a large extent on the understanding of the program limitations and the manner in which the program is utilized. Fundamental to using KRASH effectively is to recognize that the program is best at describing vehicle general structural behavior and may employ simplified representation of large structural sections in some areas. While the program allows for a definition of a wide range of nonlinear behavior, it only approximates

post-failure behavior. However, the results of sensitivity studies using KRASH are described in Reference 4, and they show that acceptable accuracy commensurate with the requirements for this type of analysis can be obtained with this approach as long as the peak failure load and deflection are satisfactorily represented.

Although program KRASH provides inputs to help assess occupant's chances of survival it does not, by itself, provide a measure of more than one injury type (DRI) which is limited to describing vertebrae compression. The program does supply a multidirectional pulse at the seat attach point along with an overall description of the behavior of the occupiable space for use in a detailed occupant, seat and restraint system model that would provide potential injury information.

As described in the modeling of the overturn accident, this type of crash would normally require an order of magnitude more computer time than a normal crash sequence. Considering that very little structural damage occurs and that no significant loads act on the occupants during most of the sequence, the use of a numerical integration scheme with a fine integration interval is a very inefficient approach. Consequently, KRASH, complemented with rigid body analysis, should be used to model only significant portions of a crash.

In some respects the program is limited by the availability of data. This limitation applies to all current analytical techniques. In particular, it is difficult to substantiate combined loading and/or unloading and ground-structure interaction, because of the lack of measured data in these areas, for many types of situations that apply to airplane structure and crash conditions. If measured data and/or proven analytical techniques become available, they can be readily used with program KRASH. As noted in Reference 4 the use of simplified techniques to obtain data as input to KRASH are practical.

SECTION 6

TASK I RESULTS

The following discussion presents a summary of the results of the Task I effort.

6.1 REVIEW AND EVALUATION OF GENERAL AVIATION AIRPLANE CHARACTERISTICS

A review and evaluation of 61 light fixed-wing airplane models, produced by the major domestic general aviation airplane manufacturers was performed. The evaluation takes into consideration airplane configuration, usage, operational characteristics, and structural characteristics.

Included in the review and evaluation of general aviation airplane characteristics are:

- o a matrix of airplane configuration, maximum takeoff weight and usage,
- o a description of structural design characteristics of current general aviation airplanes,
- o a description of the various general aviation airplane types, and
- o a categorization of airplanes as a function of configuration, maximum takeoff weight, stall speed, cruise speed, usage and accommodations.

The results of the study show that:

- (a) There are four basic airplane configurations; single-engine low-wing, single-engine high-wing, twin-engine low-wing and twin-engine high-wing.
- (b) With the exception of the agricultural airplane most airplanes have multiple uses.

- (c) There is a trend, insofar as usage, accommodations, weight and speed characteristics are involved which leads to a logical grouping of the airplanes by categories.
- (d) While there are many manufacturers and airplane models and the design details of the structure may vary, there are only two basic structural designs: monocoque and tubular.

A plot of airplane maximum cruise and flaps down stall speeds as a function of maximum takeoff weight for the different airplane models reviewed during this effort, is presented in Figure 52. The envelope reflects a practical range of velocities that would encompass most crash conditions which will aid in establishing the crash environment.

6.2 REVIEW AND EVALUATION OF ACCIDENT DATA

Accident data from CAMI, NTSB and referenced reports were obtained, reviewed and evaluated. Included in the accident evaluation are:

- o results of 18 CAMI accident records showing (a) the frequency of occurrence by phase of operation, type of accident, angle of impact roll/yaw attitude, and terrain, (b) the distribution by degree of cabin damage, structural damage, and injury types and (c) the occurrence of seat and seat belt failures and occupant impact with controls and instrument panels;
- o the description of a computer program, developed during this task, to sort and process selected pertinent crashworthiness accident data from NTSB data tapes; and
- o results of 1971 through 1973 NTSB accident records, encompassing 8491 accidents, obtained from the accident computer program employing the airplane categories established during this task.

The results of the NTSB accident data evaluation indicate that:

- (a) The impact angle in a crash is predominantly ≤ 45 degrees.
- (b) Stall, collisions with ground/water and collisions with obstacles are the prevalent types of accidents which result in serious or fatal injuries.
- (c) In accidents wherein injuries are involved, light weight single-engine airplanes have a greater number of stall accidents than accidents involving collision with ground/water or obstacles. Conversely, heavier weight single-engine and twin-engine airplanes experience more accidents involving collision with the ground.

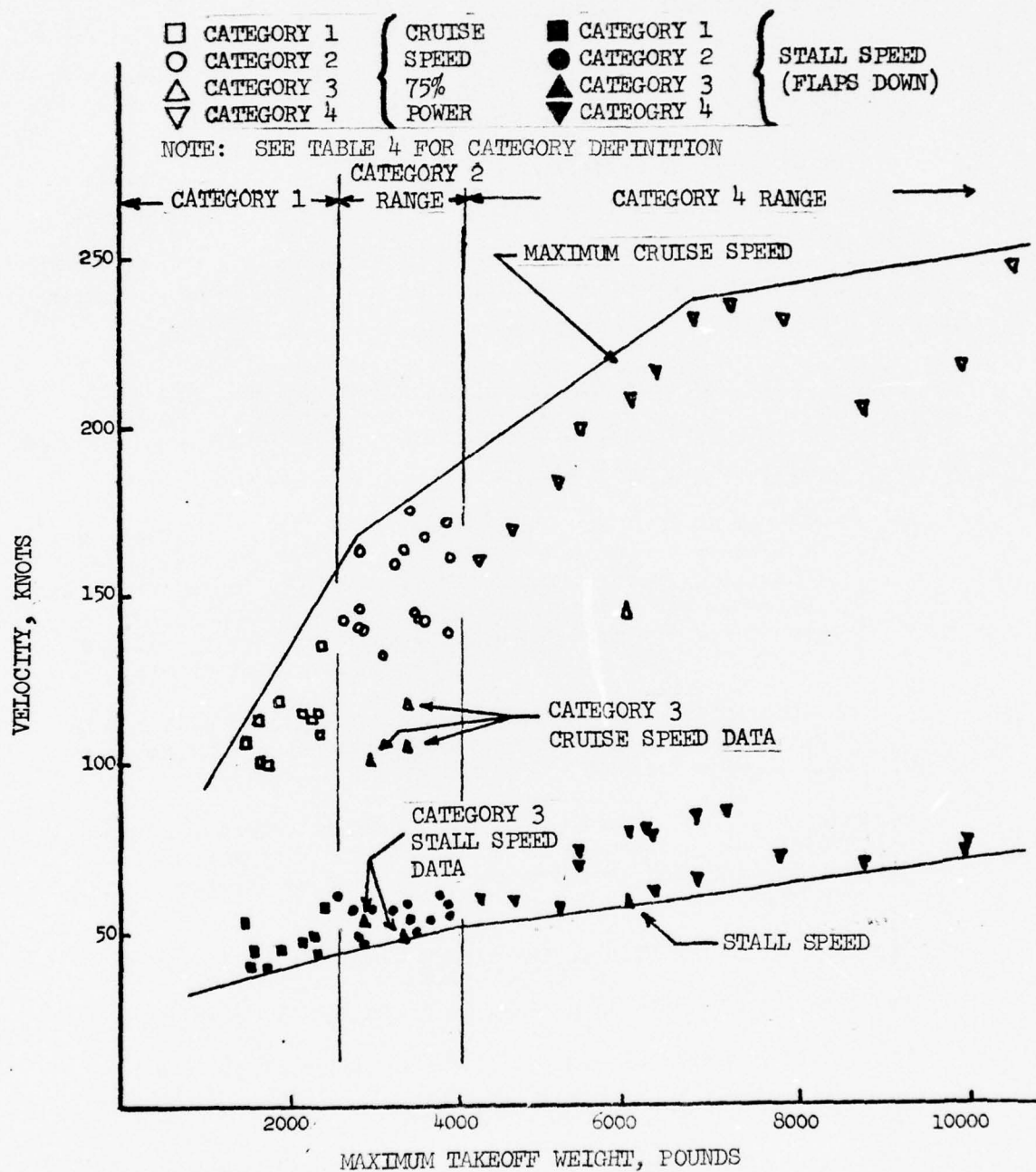


Figure 52. Operational Velocity/Weight Envelope for Current General Aviation Airplanes

- (d) The personnel involved in agricultural type airplane accidents, wherein injuries occur, experience less fatalities per occupant in all types of accidents.
- (e) The ratio of fatalities to number of occupants, for accidents involving injuries, is generally lower for the single-engine airplane than the corresponding ratio for twin-engine airplanes for the same type of accident.

6.3 MATHEMATICAL MODELING REQUIREMENTS

Seven members of the General Aviation Manufacturer's Association (GAMA) were sent an inquiry regarding their current and anticipated computer capability. Their responses indicate that the industry computer capability as a whole will, by 1977, be sufficient to utilize reasonably large ($\approx 500,000$ bytes) computer programs. However, based on the lack of current standard plotting capability within the industry, no attempt should be made to have a plot package compatible with any particular routine.

Based on the results of the review of industry computer capability and evaluation of general aviation airplane designs and accident statistics, a mathematical model, to be of benefit to the industry, should have the capability described in Section 4.2.

A brief description of program KRASH, which is the basis of the analytical method for the development of a general aviation airplane mathematical computer program is presented. The modifications to program KRASH to improve its modeling capability, add flexibility and versatility, and to facilitate its usage by the industry are described. Program KRASH, as modified for this program, contains many features not available in other current analytical techniques. A summary of program KRASH modifications, briefly stating their advantages and noting associated current restraints is presented in Table 20. The restraints do not inhibit the program's use, but serve to indicate to a potential user that program KRASH, like any analytical procedure, has certain limitations in its application. An understanding of the program's capabilities will enhance its usage and, consequently, the benefits that can be obtained therefrom.

TABLE 20. MODIFICATIONS TO KRASH

Modification	Advantage(s)	Current Restrictions
Generalized Surface	<ul style="list-style-type: none"> Adds modeling flexibility and versatility and requires only one additional input term Treats slope angle $> 0^\circ$ and $< 90^\circ$ 	<ul style="list-style-type: none"> Surface can only slope upward Surface is rigid
Standard Non-Linear Curves	<ul style="list-style-type: none"> Five (5) standard load-deflection shapes Ease of input Representative of structural behavior Facilitates parametric studies 	<ul style="list-style-type: none"> Approximate technique Requires user selection based on available guidelines
Member Directional Stress	<ul style="list-style-type: none"> Detects potential failure for selected members Tests against two (2) yield criteria 	<ul style="list-style-type: none"> Primarily of use in linear range Excludes effects of stress concentrations and detail design practices
Cabin Volume Change	<ul style="list-style-type: none"> Detects potential danger to occupants in occupiable region 	<ul style="list-style-type: none"> Describes motion of mass points only
Linear Stiffness Matrix	<ul style="list-style-type: none"> Input E, A, G, I, I_z member properties and program computes member J_z stiffness matrix Doesn't alter basic response computations User still has option to input member stiffness, if available User can identify joint attachment Reduces input to one card per member instead of 6 cards per member 	<ul style="list-style-type: none"> Each internal member is represented by only a 6×6 stiffness matrix which is related to a set of properties (E, A, G, I_z, J_z, length)
Model Parameter Data	<ul style="list-style-type: none"> Program computes from the input data: (a) vehicle mass and inertia properties, C.G. location and position relative to the ground contact point and (b) element stiffness, frequency and damping values 	<ul style="list-style-type: none"> Element frequency and damping values are based on K&S&S formulation and are "relative" terms. Guidelines for interpreting this data are available
Flow Effects	<ul style="list-style-type: none"> Represents drag force as a constant average force acting over a time span Can use ground friction with external springs to model piling effects 	<ul style="list-style-type: none"> Depends on the availability of applicable data Detailed interaction with soft earth not modeled
Acceleration Pulse	<ul style="list-style-type: none"> Includes provisions for specifying an acceleration pulse (location, direction, time history) acting on a mass or masses 	<ul style="list-style-type: none"> Restricted in number of masses to which the pulse can be applied
Damping Terms	<ul style="list-style-type: none"> Standard member damping internally coded can reduce input card to 1 for whole model instead of 1 for each member Revised damping force computation reduces the chance for instability 	<ul style="list-style-type: none"> Damping is only related to percent critical structural values. Incompatible damping value and/or integration interval can cause numerical instability. (User's Manual provides guidelines for proper selection of values)
Miscellaneous Coding Change	<ul style="list-style-type: none"> Treatment of beam longitudinal elongation is improved Computation of external spring forces and energies is improved Relationship between coupled force moment terms is preserved 	<ul style="list-style-type: none"> Nonlinear relationship for coupled forces and moments depends on nonlinear characteristics which is input data
Input and Output Format	<ul style="list-style-type: none"> New format is more consistent and uniform Expanded print of input and output terms to facilitate understanding and usage Substantially less input data cards required ($> 2/3$ reduction can be achieved) 	

6.4 ASSESSMENT OF KRASH

KRASH, as modified during this effort, is used to model two different general aviation airplane models for which controlled crash test data is available. The data was obtained from controlled crash tests which represented a stall spin and an overturn accident. The assessment of KRASH encompasses the following.

- o Descriptions of the two crash tests including purpose, sequence, instrumentation, photographic coverage, failures and photographs of the airplanes in the pretest and post test conditions.
- o Descriptions of the mathematical models that are developed to represent each of the airplanes for the particular crash conditions.
- o Comparisons of test and analysis results were performed for the following three impact conditions.
 - (a) 45 ft/sec longitudinal velocity impact into a 45 degree dirt barrier
 - (b) c.g. velocity of 19.5 inches/second (down), 259 inches/second (forward) pitch attitude of 38.5 degrees (nose down)
 - (c) c.g. velocity of 102 inches/second (down), 45.5 inches/second (forward) pitch attitude of 19.6 degrees (nose down in inverted position) pitch rate of 89.4 degrees/second (nose down in inverted position)

The results of the assessment indicate that Program KRASH meets the general aviation airplane crash analysis requirements as noted in Section 4.2. In particular, program KRASH has been shown to be capable of defining:

- o spatial and temporal energy distribution including mass kinetic and potential, member strain and damping, structural crushing, and ground friction;
- o large nonlinear behavior into the post-failure region including occupiable cabin deformations;

- o acceleration pulses at the floor in regions where occupants are located for the purpose of determining occupant response using an available occupant-seat-restraint system math model;
- o forces, accelerations, velocities and deflections resulting from multidirectional impacts;
- o structural behavior for a wide range of structural element types associated with general aviation airplane design;
- o large motion rigid-body behavior wherein ground contact forces can be defined; and
- o mathematical model requirements for two different airplane configurations (high-wing, low-wing).

Program KRASH has also been shown to have some limitations with regard to modeling certain impact conditions such as terrain-structure interaction and coupling of nonlinear loading and unloading behavior. The limitations associated with KRASH are at present applicable to all other analytical techniques. In some instances the development of additional analytical techniques or the acquisition of additional experimental data may alleviate these limitations.

Table 21 summarizes program KRASH's capability with regard to meeting the mathematical model requirements. Included are pertinent comments that indicate areas wherein the user should have a good understanding of KRASH's limitations with regard to input data as well as the output that is obtained.

TABLE 21. ASSESSMENT OF KRASH'S CAPABILITY

Requirement	KRASH Capability	Comments
Assessment of Occupant Survival	<ul style="list-style-type: none"> o Provides acceleration pulses (magnitude, shape, and duration), DRI, volume change and penetration data o Describes structural behavior which can influence occupant survival 	<ul style="list-style-type: none"> o Present occupant, seat and restraint systems are not modeled rigorously o Detail volume change is dependent on the number of masses representing a region o DRI is a measurement of only one type of injury
Multidirectional Forces	<ul style="list-style-type: none"> o Provides accelerations, forces, velocities and displacements for translations (3) and rotations (3) 	<ul style="list-style-type: none"> o Difficult to obtain test data to substantiate combined loading interaction
Structural Behavior, Deformation and Failure	<ul style="list-style-type: none"> o Represents linear and nonlinear load-deflection characteristics o Provides member directional stresses o Provides forces, velocities, and deflections o Represents crushing of structure and friction due to ground forces o Provides temporal and spatial energy distribution 	<ul style="list-style-type: none"> o Approximate representations of post-yield load-deflection behavior o May require simplified representation of large section structural characteristics o Stresses alone are inadequate measures of structural behavior and/or failure
Airplane Configurations	<ul style="list-style-type: none"> o Treats all configurations including single-engine, twin-engine, low-wing, high-wing, and light and heavy-weight airplanes o Treats welded tube and semi-monocoque fuselages, tubular and keel engine mount designs, and cantilever wing and tail units 	<ul style="list-style-type: none"> o Obtains vehicle gross behavior, thus number and location of nodes are to be selected and represented based on suggested guidelines
Multiple Impacts	<ul style="list-style-type: none"> o Determines significant portions of a crash utilizing the generalized surface routine to represent contact surface 	<ul style="list-style-type: none"> o Not economical for performing entire crash sequence (supporting rigid body analysis can define subsequent impact conditions)
Crash Environment	<ul style="list-style-type: none"> o Can treat probable crash conditions (velocity, impact angle, attitude, initial rates) and terrain with the use of external springs, plow term, generalized surface and specification of initial conditions 	<ul style="list-style-type: none"> o Depends on available data regarding terrain characteristics and effects of interaction with structure o Capabilities would be improved with addition of a flexible ground surface
Practical and Economical	<ul style="list-style-type: none"> o Utilizes available data and approximates structural behavior o Emphasizes peak force transmittal and energy absorption o Performs crash analysis using numerical integration o Uses English symbols to define input and output o Contains standardized data o Particularly effective in preliminary design 	<ul style="list-style-type: none"> o Potential refinements include <ul style="list-style-type: none"> a) variable time step integration scheme b) symmetrical model coding c) restart capability d) additional standardization of data e) increase modeling flexibility

SECTION 7.0

CONCLUSIONS

1. Based on the results of the correlation studies made, program KRASH, modified as described in this report, is a satisfactory method of performing structural crashworthiness analysis of general aviation airplanes during probable accident conditions.
2. Program KRASH is most appropriate for use during preliminary design, wherein it is desired to determine approximate airframe response to crash conditions to aid in incorporating crashworthy features in an economical manner.
3. The crash environment is influenced by airplane operating characteristics such as usage, stall and cruise speed, and mode of operation; and, by airplane configuration such as weight, and number of engines.
4. Typical crashes involving light fixed-wing aircraft indicate that the behavior of structure in some regions of the aircraft, during a crash, can have a significantly greater influence on occupant survivability than other regions. Consequently, simplified representations of structure in noncritical regions can be used in crash analysis.
5. A computer program developed by Cessna provides the basis by which NTSB accident data can be compiled and evaluated with regard to airplane configuration and/or usage as a function of accident types, terrain, injuries and/or fatalities to aid in determining crash environment design criteria.

SECTION 8
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APPENDIX A
ACCIDENT COMPUTER PROGRAM

A.1 OBJECTIVE

The purpose of this program is to summarize and to provide individual record print-outs of selected fields of selected makes and models of aircraft contained on the National Transportation and Safety Board (NTSB) data files for the years 1971, 1972, and 1973.

A.2 GENERAL INFORMATION

Minimum System Requirements

Core - 92K
Disk Space - 3800 tracks of IBM 3330
Tape Drives - 3
Printer - 1 IBM 1403
Card Reader - 1
Paper - 14" x 11"
Carriage Tape - 88 lines/page
Language - Cobol level G
Operating System - DOS/VS
Machine - IBM 370/158
Code - EDCDIC

Typical Run Time

MTSB0002 - 3 Minutes/Tape
SMTSB02 - 2 Minutes
1325020D - 12 Minutes
MTSB0001 - 2 Minutes
Print Time - 15 Minutes/Tape (Approximately 15000 lines/tape)

Manuals and Input Files

Before this program is exercised the user must acquire the manuals listed below:

Manuals

For a complete description of the input record, refer to the NTSB documents numbered 1, 2 and 3 below. Item number 4 refers to a manual associated with an NTSB program and data tape.

1. Tape Positions and Subject Matter, Aircraft Accident Files, U.S. Civil Aviation.

2. Manual of Aircraft and Engine Code Classifications.
3. Manual of Code Classifications, Aircraft Accidents & Incidents.
4. User Instructions ADP Programs - Automated Aircraft Accident and Incident Information System.

The NTSB files and manuals may be obtained by writing:

National Transportation Safety Board
Department of Transportation
Washington, D.C. 20591

You must ask specifically for each of the items listed above. If you have a problem interpreting the manuals, call:

Dave Kelly
1-202-426-3976

in Washington, D.C. He and his office have been very helpful in Cessna's work with the files.

Input Files

Full Print Header Files

A tape file which contains the Full Print Headers to be used by MTSB0001.

Record Layout for the Accident Record

This file resides on our source statement library and is copied into MTSB0002 and MTSB0001.

Accident Data Files

These files contain the actual accident record. The years 1963 thru 1974 are currently available.

In summary, the input which must be available to these programs as they exist now is as follows:

1. Accident Data Files - input to MTSB0002.
2. English Meaning Header File - input to 1-325-020-D.
3. Data Record Book on a Source Statement Library - Input to MTSB0001 and MTSB0002.

How to Execute the System

- Step 1 - Obtain a copy of the program, Job Control and Data Tape from Lockheed Aircraft.

This tape will contain the programs necessary to process all the input data, the job control required to execute the programs and the Full Print Header File in that order. See Section A.8 for a discussion of this tape.

- Step 2 - Compile and catalog all the programs on the tape and put the Accident Data File input record description on your source statement library.

- Step 3 - Make a magnetic tape labeled "NTSB Headers" as noted in the JCL listing which contains the Full Print Headers.

- Step 4 - Execute the system. Mount the input tapes as called for in the machine room setup sheets. You may mount the Accident Data Files in any order. It is suggested that the user write a small program to read each accident data file before processing the entire job because the tapes have been known to produce data checks.

If a user should find it necessary to change the screening in the programs to meet objectives different than those of the existing system, certain program changes will be necessary. See the individual program description in this report for information on how to carry out changes.

A.3 PROGRAM DESCRIPTION

Program MTSB0002 - Record selector by make and model code and model number.

This program selects accidents from as many NTSB accident data files as desired and writes them to a separate tape file. A tape file is selected to eliminate the necessity for rerunning this program each time a run on MTSB0001 is made.

It should be noted that the table for selection of airplanes is built directly into the program. Any user would need to change the table if years other than 1971, 1972, 1973 or 1974 are to be used to satisfy different requirements. The table, named MK-MOD-01, must be in ascending order Col 46 thru 56. The table content is:

Card Col	Content
46-48	Make Code
49-50	Model Code
51-56	Model Name

See a current manual of Aircraft and Engine Code Classifications for a complete description of the content.

It is suggested that a user write a program, to search the accident data tapes on the make and model codes and model numbers which are needed and let the program punch the table. This will prevent the lengthy research necessary to determine exactly how the model name was entered in the accident records. The selected records should be listed, sorted, duplicates eliminated, then punched. The list can be edited and selected models may be removed from the table of punched cards. This, then, will be the final table used in MTSB0002. All the accident data files to be processed by MTSB0002 should be used in the creation of the make and model table. It should also be noted that the model names contain some error. For example, Cessna has Model 150 names entered as 150 and 150. Also, the names may not always be left justified in the field. By writing a program to pre-edit and punch the three fields, all the fielding and punching errors can be easily found and used.

Input

Selected NTSB accident data tapes. As of this writing 1963-1974 are available with 1975 soon to be released. See Appendix A for sample input record.

Output

A tape file which contains NTSB accident records is selected by make and model codes and model name.

Console Messages

IF THIS IS THE LAST FILE ENTER LAST
IF NOT THEN MOUNT NEXT TAPE AND ENTER NEXT

YOU GOOFED
REENTER YOUR RESPONSE

Operator Response

Enter NEXT or Last

Enter Correctly spelled
response

Program SMTSB002

This is a sort which sorts the selected records on make and model code. See the SORT FIELDS record in the sort for exact fielding and sort hierarchy.

Input

Tape created by MTSB0002 which contains selected accidents.

Output

Tape file which contains sorted accident records.

Program 1-325-020-D

This program creates a direct access Full Print Header file to be used by MTSB0001.

Input

Tape file which contains the English meaning Full Print Headers. These headers are on the program and data tape.

Output

A direct access file of Full Print Headers.

Program MTSB0001

This program further selects accidents based upon the following criteria:

- a. Certain Aircraft Types.
- b. Certain Major Operational Phases.
- c. Certain Minor Operational Phases within Major Phases C, D, or E.
- d. Terrain Types
- e. Cause - Factors

If the aircraft accident is of type D, E, F, L, P, R, O, 1, 2, 4, 5 and 7, the accident is not processed further. These types are in the variable named TYPES - 77 and moved to TYPES - 01.

The major operational phase summary at top of Page 2 summarizes all major phases. However, thereafter, if the major phase is not Code C, D or E, i.e., takeoff, inflight or landing respectively, the information is not tallied and the accident is rejected entirely except for its tally in total accidents surveyed and the grand total accidents surveyed.

All minor operational phases are surveyed except the 'Other' categories under major phases C, D and E.

If the terrain type, cause-factors or certain minor phases were not acceptable, processing continues to obtain tallies in other applicable areas.

Input

A file which contains the NTSB records is selected and sorted by MTSB0002 and SMTSB002 respectively.

Output

Printed output which consists of:

1. Individual record print-outs if the accident reported

- a) impact angle
- b) impact velocity
- c) stopping distance
- d) seat failure
- e) seat belt failure
- f) attitude at impact

This does not constitute a complete record print-out, only selected portions.

There are no codes printed. The information is either taken directly from the record or the code is used to retrieve a header from the header file created by program 1-325-020-D.

2. Five pages of summary data which summarizes a make and model for all years are entered into MTSB0002.

The discussion of each page that follows deals only with those outputs which are not self-explanatory.

First Page Summary - General Information

The aircraft model is an aircraft model code because the summary is for all selected specific models in all the years processed.

The total number of accidents surveyed is a count of all those accidents, in a make and model code, on the input file.

The total applicable accidents surveyed is a count of those accidents of an acceptable type.

The total number of occupants is a summation of all the aircraft occupants in the applicable accidents.

The average number of occupants is the rounded quotient of the division of number of occupants by number of applicable accidents.

The sum of all entries in the Totals of Seriousness of Injuries table should equal the total number of occupants.

Second Page Summary - Flight Conditions

The major phase summary at top of the page summarizes all accidents on the input file of acceptable type.

The second summary on minor phase of operation summarizes only upon meeting type, major phase and minor phase requirement. No 'Other' category minor phases were summarized here. Which means that the total number of accidents will always be equal to or less than the total applicable accidents.

The third summary on types summarizes only upon meeting type and major phase requirements. The total number of accidents here should equal the total applicable accidents.

Third Page Summary - Impact Conditions

The 90+, 120+ and 360+ include 90, 120 and 360 respectively in their tallies.

The occupant injury table cannot be depended upon to record all injuries because not all the accident records contain an entry in the damage severity field. Summation was done only if a damage severity was recorded.

Fourth Page Summary - Aircraft Cabin Accommodations

The Impact Area summary percentages should total to nearly 100%. If they do not, then it can be attributed to round-off error. The list is sorted in descending order by percent.

Program Areas Which a User May Wish to Change

All the major operational phases are built into the procedure division.

The program areas which must be changed are:

1. The page layout for Page 2 which begins at Statement Number 055400. This will probably change the number of array elements in Statement Number 065300.
2. The screen is at Statement Number 105200.
3. If the number of array elements for Page 2 has changed then the PERFORM at Statement Number 213700 must be changed to equal the number of array elements used in No. 1 above.

he minor phases used for screening are contained in an array named OP-PH-01. The codes contained in this array must be in ascending order. A change in the number of codes means that this OCCURS clause at Statement Number 088600 must change and also the number in the MOVE in Statement Number 168900.

The terrain types are in a 77 level data named TERRAIN - 77. The items in this array must be in ascending order. A change in the number of items means the picture size must change in Statement Number 019700 and the values in Statement Number 024000, 040900, 041000, 186300, and 186400 must change to equal the picture size in 019700.

The cause-factors are contained in an array named CAUSE-FACTOR-01. No change need be made in the occurs clause until more than 500 cause-factor codes are used. Currently 494 are used. It should be noted that due to a few errors in the original key punching of the table, certain duplication of codes were introduced in order to avoid repunching the entire table. This will cause no problem in the searching of the table. If the number of array elements is changed then MOVE in Statement Number 191600 must change to correspond.

```
* ** JOB MTSB001 SUMNER
** PPT 0.14P1.1..100000000000000000000000C076
// JOB MTSB0001 SUMMARIZE AND LIST SELECTED AIRCRAFT
// OPTION CATAL,SYM
// PHASE TMTSR001,*
// EXEC FCOBOL
/*
// LBLTYP NSD(04)
// EXEC LNKEDT
/*
// EXEC FGPPAGE
SUMNER
/*
//
/* ** EQJ
// JOB MTSB0002 SELECT AIRCRAFT FROM NTSB FILES
// OPTION CATAL
// PHASE TMTSR002,*
// EXEC FCOBOL
/*
// LRLTYP NSD(04)
// EXEC LNKEDT
/*
// EXEC FGPPAGE
SUMNER
/*
//
// JOB R325020D FULL PRINT HEADERS TO DIRECT ACCESS DISK
// OPTION CATAL
// PHASE R325020D,*
// EXEC FCOBOL
/*
// LRLTYP NSD(04)
// EXEC LNKEDT
/*
// EXEC FGPPAGE
SUMNER
/*
//
/* ** JOB MTSB0002 SELECT AIRCRAFT FROM NTSB FILES
// JOB MTSB0002
// ASSIGN SYS018,X'T01'
// ASSIGN SYS019,X'T02'
// LBLTYP NSD(04)
// EXEC TMTSR002
/*
// EXEC FGPPAGE
SUMNER
/*
//
/* ** EQJ
// JOB SORT SELECTED AIRCRAFT
// ASSIGN SYS001,X'T03'
// ASSIGN SYS002,X'T02'
// ASSIGN SYS003,X'WK1'
// DLRL SORTWK1,'MTSB0001',72/001,SD
// EXTENT SYS003,,1,0,0019,1850
// ASSIGN SYS004,X'WK2'
// DLRL SORTWK2,'MTSB0001',72/001,SD
// EXTENT SYS004,,1,0,0019,1850
// EXEC SORT
SORT FIELDS=(82,5,BI,A),WORK=2
RECORD TYPE=F,LENGTH=1600
OPTION LABEL=(U,U,S)
END
/*
// MTC RUN,SYS002
//
/* ** JOB 1325020D FULL PRINT HEADERS TO DIRECT ACCESS DISK
** PPT 0.14P1.1..100000000000000000000000C056
```


A.5 PROGRAM LISTING

1 IBM DOS AMERICAN NATIONAL STANDARD COBOL VERSION 3 REL3.2 PP NO. 5736-CB2

```

CBL CLIST,LIBR=YES,LIBREF=STREF.
00001 000100 ID DIVISION.
00002 000200 PROGRAM-ID. MTSB0002.
00003 000300 AUTHOR. J. A. SUMNER.
00004 000400 INSTALLATION. THE CESSNA AIRCRAFT COMPANY.
00005 000500 DATE-WRITTEN. 9-20-75.
00006 000600 DATE-COMPILED. 04/09/76.
00007 000700 SECURITY. NOT CLASSIFIED.
00008 000800 REMARKS.
00009 000900 THIS PROGRAM SELECTS CERTAIN AIRCRAFT FROM THE NTSB MASTER
00010 001000 FILES TO BE SUMMARIZED BY MTSB0001.
00011 001100 ENVIRONMENT DIVISION.
00012 001200 CONFIGURATION SECTION.
00013 001300 SOURCE-COMPUTER. IBM-370.
00014 001400 OBJECT-COMPUTER. IBM-370.
00015 001500 INPUT-OUTPUT SECTION.
00016 001600 FILE-CONTROL.
00017 001700 SELECT NTSB ASSIGN SYS018-UT-2400-S.
00018 001800 SELECT NTSB-TAPE ASSIGN SYS019-UT-2400-S.
00019 001900 DATA DIVISION.
00020 002000 FILE SECTION.
00021 002100 FD NTSB
00022 002200 LABEL RECORDS ARE OMITTED
00023 002300 RECORDING MODE IS F
00024 002400 DATA RECORD IS NTSB-REC.
00025 002500 01 NTSB-REC COPY NTSBMSTR REPLACING REC BY NTSB-REC.
00026 C 000270 01 NTSB-REC.
00027 C 000280 02 F001.
00028 C 000290 03 F00101 PICTURE 99.
00029 C 000300 03 F00102 PICTURE XX.
00030 C 000310 03 F00103 PICTURE XX.
00031 C 000320 02 F002 PICTURE X(6).
00032 C 000330 02 F003 PICTURE X(10).
00033 C 000340 02 F004.
00034 C 000350 03 FILLER PICTURE X(5).
00035 C 000360 03 F00401 PICTURE X.
00036 C 000370 02 AF004 REDEFINE F004.
00037 C 000380 03 AF00401 PICTURE 99.
00038 C 000390 03 AF00402 PICTURE XX.
00039 C 000400 03 AF00403 PICTURE XX.
00040 C 000410 02 F005.
00041 C 000420 03 F00501 PICTURE X.
00042 C 000430 03 F00502.
00043 C 000440 04 FILLER PICTURE X(16).
00044 C 000450 04 F0050201 PICTURE X.
00045 C 000460 02 F006 PICTURE X(11).
00046 C 000470 02 F007 PICTURE X(6).
00047 C 000480 02 F008.
00048 C 000490 03 FILLER PICTURE X(9).
00049 C 000500 03 F00801 PICTURE X.
00050 C 000510 02 F009.
00051 C 000520 03 FILLER PICTURE XXX.
00052 C 000530 03 F00901 PICTURE X.
00053 C 000540 02 FILLER PICTURE X.
00054 C 000550
00055 C 000560
00056 C 000570
00057 C 000580
00058 C 000590
00059 C 000600 03 F010 PICTURE X.
00060 C 000610 03 F011 PICTURE XX.
00061 C 000620 03 F012 PICTURE XXX.
00062 C 000630 03 F013 PICTURE XX.
00063 C 000640 03 F014 PICTURE XX.
00064 C 000650 03 F015 PICTURE XX.
00065 C 000660 03 F016 PICTURE X.
00066 C 000670 03 F017 PICTURE X.
00067 C 000680 03 F018 PICTURE X.
00068 C 000690 03 F019 PICTURE X.
00069 C 000700 03 F020 PICTURE X.
00070 C 000710 03 F021 PICTURE X.
00071 C 000720 03 F022 PICTURE X.
00072 C 000730 03 F023.
00073 C 000740 04 F02301 PICTURE X.
00074 C 000750
00075 C 000760
00076 C 000770
00077 C 000780
00078 C 000790
00079 C 000800
00080 C 000810
00081 C 000820
00082 C 000830
00083 C 000840
00084 C 000850
00085 C 000860
00086 C 000870
00087 C 000880
00088 C 000890
00089 C 000900
00090 C 000910
00091 C 000920
00092 C 000930
00093 C 000940
00094 C 000950
00095 C 000960
00096 C 000970
00097 C 000980
00098 C 000990
00099 C 001000
00100 C 001010
00101 C 001020
00102 C 001030
00103 C 001040
00104 C 001050
00105 C 001060
00106 C 001070
00107 C 001080
00108 C 001090
00109 C 001100
00110 C 001110
00111 C 001120
00112 C 001130
00113 C 001140
00114 C 001150
00115 C 001160
00116 C 001170
00117 C 001180
00118 C 001190
00119 C 001200
00120 C 001210
00121 C 001220
00122 C 001230
00123 C 001240
00124 C 001250
00125 C 001260
00126 C 001270
00127 C 001280
00128 C 001290
00129 C 001300
00130 C 001310
00131 C 001320
00132 C 001330
00133 C 001340
00134 C 001350
00135 C 001360
00136 C 001370
00137 C 001380
00138 C 001390
00139 C 001400
00140 C 001410
00141 C 001420
00142 C 001430
00143 C 001440
00144 C 001450
00145 C 001460
00146 C 001470
00147 C 001480
00148 C 001490
00149 C 001500
00150 C 001510
00151 C 001520
00152 C 001530
00153 C 001540
00154 C 001550
00155 C 001560
00156 C 001570
00157 C 001580
00158 C 001590
00159 C 001600
00160 C 001610
00161 C 001620
00162 C 001630
00163 C 001640
00164 C 001650
00165 C 001660
00166 C 001670
00167 C 001680
00168 C 001690
00169 C 001700
00170 C 001710
00171 C 001720
00172 C 001730
00173 C 001740
00174 C 001750
00175 C 001760
00176 C 001770
00177 C 001780
00178 C 001790
00179 C 001800
00180 C 001810
00181 C 001820
00182 C 001830
00183 C 001840
00184 C 001850
00185 C 001860
00186 C 001870
00187 C 001880
00188 C 001890
00189 C 001900
00190 C 001910
00191 C 001920
00192 C 001930
00193 C 001940
00194 C 001950
00195 C 001960
00196 C 001970
00197 C 001980
00198 C 001990
00199 C 002000
00200 C 002010
00201 C 002020
00202 C 002030
00203 C 002040
00204 C 002050
00205 C 002060
00206 C 002070
00207 C 002080
00208 C 002090
00209 C 002100
00210 C 002110
00211 C 002120
00212 C 002130
00213 C 002140
00214 C 002150
00215 C 002160
00216 C 002170
00217 C 002180
00218 C 002190
00219 C 002200
00220 C 002210
00221 C 002220
00222 C 002230
00223 C 002240
00224 C 002250
00225 C 002260
00226 C 002270
00227 C 002280
00228 C 002290
00229 C 002300
00230 C 002310
00231 C 002320
00232 C 002330
00233 C 002340
00234 C 002350
00235 C 002360
00236 C 002370
00237 C 002380
00238 C 002390
00239 C 002400
00240 C 002410
00241
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00073 C	000740	04 F02302	PICTURE X.	RON
00074 C	000750	03 F024	PICTURE X.	RON
00075 C	000760	03 F025		RON
00076 C	000770	04 F02501	PICTURE X.	RON
00077 C	000780	04 F02502	PICTURE X.	RON
00078 C	000790	03 F026	PICTURE XX.	RON
00079 C	000800	03 F027	PICTURE X.	RON
00080 C	000810	03 F028		RON
00081 C	000820	04 F02801	PICTURE X.	RON
00082 C	000830	04 F02802	PICTURE X.	RON
00083 C	000840	03 F029		RON
00084 C	000850	04 F02901	PICTURE X.	RON
00085 C	000860	04 F02902	PICTURE X.	RON
00086 C	000870	03 F030		RON
00087 C	000880	04 F03001	PICTURE X.	RON
00088 C	000890	04 F03002	PICTURE X.	RON
00089 C	000900	03 F031		RON
00090 C	000910	04 F03101	PICTURE X.	RON
00091 C	000920	04 F03102	PICTURE X.	RON
00092 C	000930	03 F032		RON
00093 C	000940	04 FILLER	PICTURE X(4).	RON
00094 C	000950	04 F03201	PICTURE X.	RON
00095 C	000960	03 F033		RON
00096 C	000970	04 FILLER	PICTURE X(4).	RON
00097 C	000980	04 F03301	PICTURE X.	RON
00098 C	000990	03 F034		RON
00099 C	001000	04 FILLER	PICTURE XX.	RON
00100 C	001010	04 F03401	PICTURE X.	RON
00101 C	001020	03 F035		RON
00102 C	001030	04 FILLER	PICTURE X(13).	RON
00103 C	001040	04 F03501	PICTURE X.	RON
00104 C	001050			RON
00105 C	001060			RON
00106 C	001070	02 EMGCY-CUND.		RON
00107 C	001080			RON
00108 C	001090	03 F036	PICTURE X.	RON
00109 C	001100	03 F037		RON
00110 C	001110	04 F03701	PICTURE X.	RON
00111 C	001120	04 F03702	PICTURE X.	RON
00112 C	001130	03 F038	PICTURE X.	RON
00113 C	001140	03 F039	PICTURE X.	RON
00114 C	001150	03 F040		RON
00115 C	001160	04 F04001	PICTURE X.	RON
00116 C	001170	04 F04002	PICTURE X.	RON
00117 C	001180			RON
00118 C	001190			RON
00119 C	001200	02 WEATHER.		RON
00120 C	001210			RON
00121 C	001220	03 F041	PICTURE X.	RON
00122 C	001230	03 F042	PICTURE X.	RON
00123 C	001240	03 F043	PICTURE X.	RON
00124 C	001250	03 F044	PICTURE X.	RON
00125 C	001260	03 F045	PICTURE X.	RON
00126 C	001270	03 F046	PICTURE X.	RON
00127 C	001280	03 F047	PICTURE X.	RON
00128 C	001290			RON
00129 C	001300			RON
00130 C	001310	02 AIRPORT.		RON
00131 C	001320			RON
00132 C	001330	03 F048	PICTURE X.	RON
00133 C	001340	03 F049	PICTURE X.	RON
00134 C	001350	03 F050	PICTURE X(5).	RON
00135 C	001360	03 F051	PICTURE X.	RON
00136 C	001370	03 F052	PICTURE X(17).	RON
00137 C	001380	03 F053	PICTURE X(5).	RON
00138 C	001390	03 F054	PICTURE X.	RON
00139 C	001400	03 F055	PICTURE X.	RON
00140 C	001410	03 F056		RON
00141 C	001420	04 F05601	PICTURE X.	RON
00142 C	001430	04 F05602	PICTURE X.	RON
00143 C	001440	03 F057	PICTURE X.	RON
00144 C	001450	03 F058	PICTURE X.	RON
00145 C	001460	03 F059	PICTURE X.	RON

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00146 C	001470	03 F060	PICTURE X(5).	RON
00147 C	001480			RON
00148 C	001490			RON
00149 C	001500	02 ITINERARY.		RON
00150 C	001510			RON
00151 C	001520	03 F061.		RON
00152 C	001530	04 F06101	PICTURE X.	RON
00153 C	001540	04 FILLER	PICTURE X(20).	RON
00154 C	001550	03 F062.		RON
00155 C	001560	04 F06201	PICTURE X.	RON
00156 C	001570	04 FILLER	PICTURE X(20).	RON
00157 C	001580	03 F063.		RON
00158 C	001590	04 F06301	PICTURE X.	RON
00159 C	001600	04 FILLER	PICTURE X(20).	RON
00160 C	001610			RON
00161 C	001620	02 ACC-SITE.		RON
00162 C	001630			RON
00163 C	001640			RON
00164 C	001650	03 F064.		RON
00165 C	001660	04 FILLER	PICTURE X(4).	RON
00166 C	001670	04 F06401	PICTURE X.	RON
00167 C	001680	03 F065	PICTURE X.	RON
00168 C	001690			RON
00169 C	001700	02 MISC.		RON
00170 C	001710			RON
00171 C	001720			RON
00172 C	001730	03 F066	PICTURE X.	RON
00173 C	001740	03 F067	PICTURE X.	RON
00174 C	001750	03 FILLER	PICTURE X.	RON
00175 C	001760			RON
00176 C	001770	02 PILOT-DATA.		RON
00177 C	001780			RON
00178 C	001790			RON
00179 C	001800	03 F068.		RON
00180 C	001810	04 F06801	PICTURE X.	RON
00181 C	001820	04 F06802	PICTURE X.	RON
00182 C	001830	03 F069.		RON
00183 C	001840	04 F06901.		RON
00184 C	001850	05 F0690101.		RON
00185 C	001860	06 FILLER	PICTURE X(4).	RON
00186 C	001870	06 F069010101	PICTURE X.	RON
00187 C	001880	05 FILLER	PICTURE X.	RON
00188 C	001890	04 F06902.		RON
00189 C	001900	05 F0690201.		RON
00190 C	001910	06 FILLER	PICTURE X(4).	RON
00191 C	001920	06 F069020101	PICTURE X.	RON
00192 C	001930	05 FILLER	PICTURE X.	RON
00193 C	001940	03 F070.		RON
00194 C	001950	04 F07001.		RON
00195 C	001960	05 F0700101.		RON
00196 C	001970	06 FILLER	PICTURE X(4).	RON
00197 C	001980	06 F070010101	PICTURE X.	RON
00198 C	001990	05 FILLER	PICTURE X.	RON
00199 C	002000	04 F07002.		RON
00200 C	002010	05 F0700201.		RON
00201 C	002020	06 FILLER	PICTURE X(4).	RON
00202 C	002030	06 F070020101	PICTURE X.	RON
00203 C	002040	05 FILLER	PICTURE X.	RON
00204 C	002050	03 F071.		RON
00205 C	002060	04 F07101.		RON
00206 C	002070	05 F0710101.		RON
00207 C	002080	06 FILLER	PICTURE X.	RON
00208 C	002090	06 F071010101	PICTURE X.	RON
00209 C	002100	05 FILLER	PICTURE X.	RON
00210 C	002110	04 F07102.		RON
00211 C	002120	05 F0710201.		RON
00212 C	002130	06 FILLER	PICTURE X.	RON
00213 C	002140	06 F071020101	PICTURE X.	RON
00214 C	002150	05 FILLER	PICTURE X.	RON
00215 C	002160	03 F072.		RON
00216 C	002170	04 F07201.		RON
00217 C	002180	05 F0720101	PICTURE X.	RON
00218 C	002190	05 FILLER	PICTURE X.	RON

00219 C	002200	04	F07202.			RON
00220 C	002210	05	F0720201	PICTURE X.		RON
00221 C	002220	05	FILLER	PICTURE X.		RON
00222 C	002230	03	F073.			RON
00223 C	002240	04	F07301.			RON
00224 C	002250	05	F0730101	PICTURE X.		RON
00225 C	002260	05	FILLER	PICTURE X.		RON
00226 C	002270	04	F07302.			RON
00227 C	002280	05	F0730201	PICTURE X.		RON
00228 C	002290	05	FILLER	PICTURE X.		RON
00229 C	002300	03	F074.			RON
00230 C	002310	04	F07401.			RON
00231 C	002320	05	F0740101	PICTURE X.		RON
00232 C	002330	05	FILLER	PICTURE X.		RON
00233 C	002340	04	F07402.			RON
00234 C	002350	05	F0740201	PICTURE X.		RON
00235 C	002360	05	FILLER	PICTURE X.		RON
00236 C	002370	03	F075.			RON
00237 C	002380	04	F07501.			RON
00238 C	002390	05	F0750101	PICTURE X.		RON
00239 C	002400	05	FILLER	PICTURE X.		RON
00240 C	002410	04	F07502.			RON
00241 C	002420	05	F0750201	PICTURE X.		RON
00242 C	002430	05	FILLER	PICTURE X.		RON
00243 C	002440	03	F076.			RON
00244 C	002450	04	F07601.			RON
00245 C	002460	05	F0760101	PICTURE X.		RON
00246 C	002470	05	FILLER	PICTURE X.		RON
00247 C	002480	04	F07602.			RON
00248 C	002490	05	F0760201	PICTURE X.		RON
00249 C	002500	05	FILLER	PICTURE X.		RON
00250 C	002510	03	F077			RON
00251 C	002520					RON
00252 C	002530					RON
00253 C	002540	02	DUM1.			RON
00254 C	002550					RON
00255 C	002560	03	FILLER	PICTURE X(20).		RON
00256 C	002570					RON
00257 C	002580					RON
00258 C	002590	02	CAUSE-FACTOR.			RON
00259 C	002600					RON
00260 C	002610	03	F078	OCCURS 17 TIMES.		RON
00261 C	002620	04	F07801	PICTURE XX.		RON
00262 C	002630	04	F07802	PICTURE X.		RON
00263 C	002640	04	F07803.			RON
00264 C	002650	05	F0780301	PICTURE X.		RON
00265 C	002660	05	F0780302	PICTURE X.		RON
00266 C	002670					RON
00267 C	002680					RON
00268 C	002690	02	INJRY.			RON
00269 C	002700					RON
00270 C	002710	03	F079	PICTURE X.		RON
00271 C	002720	03	F080A.			RON
00272 C	002730	04	F08001A	OCCURS 3 TIMES.		RON
00273 C	002740	05	F0800101A	OCCURS 6 TIMES	PICTURE XXX.	RON
00274 C	002750	04	FILLER	PICTURE X(7).		RON
00275 C	002760	03	F080B	OCCURS 4 TIMES.		RON
00276 C	002770	04	F08001B	OCCURS 3 TIMES.		RON
00277 C	002780	05	F0800101B	OCCURS 6 TIMES	PICTURE XXX.	RON
00278 C	002790	04	FILLER	PICTURE X(8).		RON
00279 C	002800	03	F081.			RON
00280 C	002810	04	F08101	OCCURS 6 TIMES	PICTURE XXX.	RON
00281 C	002820	04	FILLER	PICTURE X(8).		RON
00282 C	002830					RON
00283 C	002840	02	RMRKS.			RON
00284 C	002850					RON
00285 C	002860					RON
00286 C	002870	03	F082.			RON
00287 C	002880	04	F08201	PICTURE X.		RON
00288 C	002890	04	F08202	PICTURE X(49).		RON
00289 C	002900	03	FILLER	PICTURE X(11).		RON
00290 C	002910					RON
00291 C	002920					RON

00292 C	002930	02 CAUSE.		RON
00293 C	002940			RON
00294 C	002950	03 F083.		RON
00295 C	002960	04 F08301	OCCURS 50 TIMES PICTURE X.	RON
00296 C	002970	03 FILLER	PICTURE X(11).	RON
00297 C	002980			RON
00298 C	002990			RON
00299 C	003000	02 DUM2.		RON
00300 C	003010			RON
00301 C	003020	03 FILLER	PICTURE X(20).	RON
00302 C	003030			RON
00303 C	003040			RON
00304 C	003050	02 E-P-DATA.		RON
00305 C	003060			RON
00306 C	003070	03 F084	PICTURE X.	RON
00307 C	003080	03 F085	PICTURE X.	RON
00308 C	003090	03 F086	PICTURE X.	RON
00309 C	003100	03 F087	PICTURE X.	RON
00310 C	003110	03 F088	PICTURE X.	RON
00311 C	003120	03 F089	PICTURE X.	RON
00312 C	003130			RON
00313 C	003140			RON
00314 C	003150	02 OVERHAUL.		RON
00315 C	003160			RON
00316 C	003170	03 F090.		RON
00317 C	003180	04 FILLER	PICTURE X(4).	RON
00318 C	003190	04 F09001	PICTURE X.	RON
00319 C	003200	03 F091.		RON
00320 C	003210	04 F09101	OCCURS 4 TIMES.	RON
00321 C	003220	05 FILLER	PICTURE XXX.	RON
00322 C	003230	05 F0910101	PICTURE X.	RON
00323 C	003240	03 F092.		RON
00324 C	003250	04 F09201	OCCURS 4 TIMES.	RON
00325 C	003260	05 FILLER	PICTURE XXX.	RON
00326 C	003270	05 F0920101	PICTURE X.	RON
00327 C	003280	03 F093.		RON
00328 C	003290	04 FILLER	PICTURE X(5).	RON
00329 C	003300	04 F09301	PICTURE X.	RON
00330 C	003310	03 F094.		RON
00331 C	003320	04 F09401	PICTURE X.	RON
00332 C	003330	04 FILLER	PICTURE X(11).	RON
00333 C	003340	03 FILLER	PICTURE X.	RON
00334 C	003350			RON
00335 C	003360			RON
00336 C	003370	02 WEATHER-SITE.		RON
00337 C	003380			RON
00338 C	003390	03 F095	PICTURE X.	RON
00339 C	003400	03 F096.		RON
00340 C	003410	04 FILLER	PICTURE X(4).	RON
00341 C	003420	04 F09601	PICTURE X.	RON
00342 C	003430	03 F097	PICTURE X.	RON
00343 C	003440	03 F098.		RON
00344 C	003450	04 F09801	PICTURE X.	RON
00345 C	003460	04 F09802	PICTURE X.	RON
00346 C	003470	03 F099	PICTURE X.	RON
00347 C	003480	03 F100	PICTURE X.	RON
00348 C	003490	03 F101	PICTURE XX.	RON
00349 C	003500	03 F102	PICTURE X(4).	RON
00350 C	003510	03 F103.		RON
00351 C	003520	04 F10301	PICTURE X.	RON
00352 C	003530	04 F10302	PICTURE X.	RON
00353 C	003540	04 F10303	PICTURE X.	RON
00354 C	003550	03 F104	PICTURE XXX.	RON
00355 C	003560	03 F105	PICTURE XXX.	RON
00356 C	003570	03 F106.		RON
00357 C	003580	04 FILLER	PICTURE XX.	RON
00358 C	003590	04 F10601	PICTURE X.	RON
00359 C	003600			RON
00360 C	003610			RON
00361 C	003620	02 AAA.		RON
00362 C	003630			RON
00363 C	003640	03 F107	PICTURE X.	RON
00364 C	003650	03 F108	PICTURE X.	RON

00365 C 003660	03 F109	PICTURE X.	RON
00366 C 003670	03 F110	PICTURE X.	RON
00367 C 003680	03 F111	PICTURE X.	RON
00368 C 003690	03 F112	PICTURE X.	RON
00369 C 003700	03 F113	PICTURE X.	RON
00370 C 003710	03 F114	PICTURE X.	RON
00371 C 003720	03 F115	PICTURE X.	RON
00372 C 003730	03 F116	PICTURE X.	RON
00373 C 003740	03 F117	PICTURE X.	RON
00374 C 003750	03 F118	PICTURE X.	RON
00375 C 003760	03 F119	PICTURE X.	RON
00376 C 003770			RON
00377 C 003780			RON
00378 C 003790	02 DUM3.		RON
00379 C 003800	03 FILLER	PICTURE X(20).	RON
00380 C 003810			RON
00381 C 003820			RON
00382 C 003830	02 FLIGHT-DATA.		RON
00383 C 003840	03 F120.		RON
00384 C 003850	04 FILLER	PICTURE XXX.	RON
00385 C 003860	04 F12001	PICTURE X.	RON
00386 C 003870	03 F121.		RON
00387 C 003880	04 FILLER	PICTURE XXX.	RON
00388 C 003890	04 F12101	PICTURE X.	RON
00389 C 003900	03 F122	PICTURE XXX.	RON
00390 C 003910	03 F123	PICTURE XX.	RON
00391 C 003920	03 F124.		RON
00392 C 003930	04 FILLER	PICTURE XXX.	RON
00393 C 003940	04 F12401	PICTURE X.	RON
00394 C 003950	03 F125.		RON
00395 C 003960	04 F12501.		RON
00396 C 003970	05 FILLER	PICTURE X.	RON
00397 C 003980	05 F1250101	PICTURE X.	RON
00398 C 003990	04 F12502.		RON
00399 C 004000	05 FILLER	PICTURE XX.	RON
00400 C 004010	05 F1250201	PICTURE X.	RON
00401 C 004020	04 F12503.		RON
00402 C 004030	05 FILLER	PICTURE XX.	RON
00403 C 004040	05 F1250301	PICTURE X.	RON
00404 C 004050	03 F126.		RON
00405 C 004060	04 FILLER	PICTURE X.	RON
00406 C 004070	04 F12601	PICTURE X.	RON
00407 C 004080	03 F127.		RON
00408 C 004090	04 FILLER	PICTURE X.	RON
00409 C 004100	04 F12701	PICTURE X.	RON
00410 C 004110	03 F128	PICTURE XX.	RON
00411 C 004120	03 F129.		RON
00412 C 004130	04 FILLER	PICTURE X(16).	RON
00413 C 004140	04 F12901	PICTURE X.	RON
00414 C 004150	03 F130.		RON
00415 C 004160	04 FILLER	PICTURE X(9).	RON
00416 C 004170	04 F13001	PICTURE X.	RON
00417 C 004180	03 FILLER	PICTURE X(4).	RON
00418 C 004190			RON
00419 C 004200			RON
00420 C 004210	02 HUMAN-FACTORS.		RON
00421 C 004220	03 F131.		RON
00422 C 004230	04 F13101	PICTURE X.	RON
00423 C 004240	04 F13102	PICTURE X.	RON
00424 C 004250	04 F13103	PICTURE X.	RON
00425 C 004260	04 F13104	PICTURE X.	RON
00426 C 004270	03 F132	PICTURE XX.	RON
00427 C 004280	03 F133.		RON
00428 C 004290	04 F13301	PICTURE X.	RON
00429 C 004300	04 F13302.		RON
00430 C 004310	05 FILLER	PICTURE X.	RON
00431 C 004320	05 F1330201	PICTURE X.	RON
00432 C 004330	03 F134	PICTURE X.	RON
00433 C 004340	03 F135	PICTURE X.	RON
00434 C 004350	03 F136.		RON
00435 C 004360			RON
00436 C 004370			RON
00437 C 004380			RON

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00438 C	004390	04 FILLER	PICTURE XXX.	RON
00439 C	004400	04 F13601	PICTURE X.	RON
00440 C	004410	03 F137.		RON
00441 C	004420	04 F13701	PICTURE X.	RON
00442 C	004430	04 F13702	PICTURE X.	RON
00443 C	004440	04 F13703	PICTURE X.	RON
00444 C	004450	04 F13704	PICTURE X.	RON
00445 C	004460	04 F13705	PICTURE X.	RON
00446 C	004470	03 F138.	PICTURE X.	RON
00447 C	004480	03 F139.		RON
00448 C	004490	04 FILLER	PICTURE XX.	RON
00449 C	004500	04 F13901	PICTURE X.	RON
00450 C	004510	03 F140.		PON
00451 C	004520	04 FILLER	PICTURE XX.	PON
00452 C	004530	04 F14001	PICTURE X.	PON
00453 C	004540	03 F141.		RON
00454 C	004550	04 FILLER	PICTURE XX.	RON
00455 C	004560	04 F14101	PICTURE X.	RON
00456 C	004570	03 F142.	PICTURE X.	RON
00457 C	004580	03 F143.	PICTURE X.	RON
00458 C	004590	03 F144.	PICTURE X.	RON
00459 C	004600	03 F145.	PICTURE X.	RON
00460 C	004610	03 F146.	PICTURE X.	RON
00461 C	004620	03 F147.	PICTURE X.	RON
00462 C	004630	03 F148.		KON
00463 C	004640	04 F14801	PICTURE X.	RON
00464 C	004650	04 F14802	PICTURE X.	RON
00465 C	004660	04 F14803	PICTURE X.	RON
00466 C	004670	04 F14804	PICTURE X.	RON
00467 C	004680	03 F149.		RON
00468 C	004690	04 F14901.		RON
00469 C	004700	05 FILLER	PICTURE XX.	RON
00470 C	004710	05 F1490101	PICTURE X.	RON
00471 C	004720	04 F14902.		RON
00472 C	004730	05 FILLER	PICTURE XX.	RON
00473 C	004740	05 F1490201	PICTURE X.	RON
00474 C	004750	03 F150.	PICTURE X.	RON
00475 C	004760	03 F151.		RON
00476 C	004770	04 F15101	PICTURE X.	RON
00477 C	004780	04 F15102	PICTURE X.	RON
00478 C	004790	04 F15103	PICTURE X.	RON
00479 C	004800	03 F152.		RON
00480 C	004810	04 FILLER	PICTURE XX.	RON
00481 C	004820	04 F15201	PICTURE X.	RON
00482 C	004830	03 F153.	PICTURE X.	RON
00483 C	004840	03 FILLER	PICTURE X(7).	RON
00484 C	004850			RON
00485 C	004860			RON
00486 C	004870	02 FIRE-INFO.		RON
00487 C	004880			RON
00488 C	004890	03 F154.	PICTURE X.	RON
00489 C	004900	03 F155.	PICTURE X.	RON
00490 C	004910	03 F156.	PICTURE X.	RON
00491 C	004920	03 F157.	PICTURE X.	RON
00492 C	004930	03 F158.		RON
00493 C	004940	04 F15801	PICTURE X.	RON
00494 C	004950	04 F15802.		RON
00495 C	004960	05 F1580201	PICTURE X.	RON
00496 C	004970	05 F1580202	PICTURE X.	RON
00497 C	004980	04 F15803.		RON
00498 C	004990	05 F1580301	PICTURE X.	RON
00499 C	005000	05 F1580302	PICTURE X.	RON
00500 C	005010	03 F159.	PICTURE X.	RON
00501 C	005020	03 F160.	PICTURE X.	RON
00502 C	005030	03 F161.		RON
00503 C	005040	04 F16101	PICTURE X.	RON
00504 C	005050	04 F16102	PICTURE X.	RON
00505 C	005060			RON
00506 C	005070			RON
00507 C	005080	02 EQUIP.		RON
00508 C	005090			RON
00509 C	005100	03 F162.	PICTURE X.	RON
00510 C	005110	03 F163.	PICTURE X.	RON

00511 C	005120	03 F164.			RON
00512 C	005130	04 F16401	PICTURE X.		RON
00513 C	005140	04 F16402	PICTURE X.		RON
00514 C	005150	03 F165	PICTURE X.		RON
00515 C	005160	03 F166	PICTURE X.		RON
00516 C	005170				RON
00517 C	005180				RON
00518 C	005190	02 W-B-DAMAGE.			RON
00519 C	005200				RON
00520 C	005210	03 F167	PICTURE X.		RON
00521 C	005220	03 F168	PICTURE X.		RON
00522 C	005230	03 F169	PICTURE X.		RON
00523 C	005240	03 F170	PICTURE X.		RON
00524 C	005250	03 F171	PICTURE X.		RON
00525 C	005260	03 F172	PICTURE X.		RON
00526 C	005270	03 F173	PICTURE X.		RON
00527 C	005280	03 F174.			RON
00528 C	005290	04 F17401	PICTURE X.		RON
00529 C	005300	04 F17402	PICTURE X.		RON
00530 C	005310	03 F175	PICTURE X.		RON
00531 C	005320	03 F176	PICTURE X.		RON
00532 C	005330	03 F177.			RON
00533 C	005340	04 F17701	PICTURE X.		RON
00534 C	005350	04 F17702	PICTURE X.		RON
00535 C	005360	03 F178	PICTURE X.		RON
00536 C	005370	03 F179	PICTURE X.		RON
00537 C	005380	03 F180	PICTURE X.		RON
00538 C	005390	03 F181	PICTURE X.		RON
00539 C	005400	03 F182	PICTURE X.		RON
00540 C	005410	03 F183	PICTURE X.		RON
00541 C	005420				RON
00542 C	005430				RON
00543 C	005440	02 DUM4.			RON
00544 C	005450				RON
00545 C	005460	03 FILLER	PICTURE X(23).		RON
00546 C	005470	03 FILLER	PICTURE X(20).		RON
00547 C	005480				RON
00548 C	005490				RON
00549 C	005500	02 ADMIN-DATA.			RON
00550 C	005510				RON
00551 C	005520	03 FILLER	PICTURE XXX.		RON
00552 C	005530	03 F184	PICTURE X(12).		RON
00553 C	005540	03 F185	PICTURE X(6).		RON
00554 C	005550	03 F186	OCCURS 3 TIMES.		RON
00555 C	005560	04 F18601	PICTURE 99.		RON
00556 C	005570	04 F18602	PICTURE XX.		RON
00557 C	005580	04 F18603	PICTURE XX.		RON
00558 C	005590	03 F187	PICTURE 99.		RON
00559 C	005600	03 F188	PICTURE XXX.		RON
00560 C	005610	03 F189	PICTURE X(13).		RON
00561 C	005620				RON
00562 C	005630				RON
00563 C	005640	02 IDN.			RON
00564 C	005650				RON
00565 C	005660	03 F190	PICTURE X(4).		RON
00566 C	005670				RON
00567 C	005680				RON
00568 C	005690	02 DUM5.			RON
00569 C	005700				RON
00570 C	005710	03 FILLER	PICTURE X(20).		RON
00571 C	005720				RON
00572 C	005730				RON
00573 C	005740	02 AERIAL-APP.			RON
00574 C	005750				RON
00575 C	005760	03 F191.			RON
00576 C	005770	04 FILLER	PICTURE XXX.		RON
00577 C	005780	04 F19101	PICTURE X.		RON
00578 C	005790	03 F192	PICTURE X.		RON
00579 C	005800	03 F193	PICTURE X.		RON
00580 C	005810	03 F194	PICTURE X.		RON
00581 C	005820	03 F195	PICTURE X.		RON
00582 C	005830	03 F196	PICTURE X.		RON
00583 C	005840	03 F197	PICTURE X.		RON

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00584	C	005850	03	F198	PICTURE X.	RON
00585	C	005860	03	F199	PICTURE X.	RON
00586	C	005870	03	F200	PICTURE X.	RON
00587	C	005880	03	F201	PICTURE X.	RON
00588	C	005890	03	F202	PICTURE X.	RON
00589	C	005900	03	F203	PICTURE X.	RON
00590	C	005910	03	F204	PICTURE X.	RON
00591	C	005920	03	F205	PICTURE X.	RON
00592	C	005930	03	F206	PICTURE X.	RON
00593	C	005940	03	F207	PICTURE X.	RON
00594	C	005950	03	F208	PICTURE X.	RON
00595	C	005960	03	F209	PICTURE X(5).	RON
00596	C	005970	04	F20901	PICTURE X.	RON
00597	C	005980	04	F20902	PICTURE X.	RON
00598	C	005990	04	F20903	PICTURE X.	RON
00599	C	006000	03	F210	PICTURE X.	RON
00600	C	006010	04	F21001	PICTURE X.	RON
00601	C	006020	04	F21002	PICTURE X.	RON
00602	C	006030	04	F21003	PICTURE X.	RON
00603	C	006040	03	F211	PICTURE X.	RON
00604	C	006050	03	F212	PICTURE X.	RON
00605	C	006060				RON
00606	C	006070				RON
00607	C	006080	02	DUM6.		RON
00608	C	006090				RON
00609	C	006100	03	FILLER	PICTURE X(28).	RON
00610	C	006110	03	FILLER	PICTURE X(20).	RON
00611	C	006120				RON
00612	C	006130				RON
00613	C	006140	02	COL.		RON
00614	C	006150				RON
00615	C	006160	03	F213	PICTURE X.	RON
00616	C	006170	03	F214	PICTURE X.	RON
00617	C	006180	03	F215	PICTURE X.	RON
00618	C	006190	03	F216	PICTURE X.	RON
00619	C	006200	03	F217	PICTURE X.	RON
00620	C	006210	03	F218	PICTURE X.	RON
00621	C	006220	03	F219	PICTURE X.	RON
00622	C	006230	03	F220	PICTURE XXX.	RON
00623	C	006240	03	F221	PICTURE XXX.	RON
00624	C	006250	03	F222		RON
00625	C	006260	04	F22201	PICTURE XXX.	RON
00626	C	006270	04	F22202	PICTURE XXX.	RON
00627	C	006280	03	F223	PICTURE X.	RON
00628	C	006290	03	F224	PICTURE X.	RON
00629	C	006300	03	F225	PICTURE X.	RON
00630	C	006310	03	F226	PICTURE X.	RON
00631	C	006320	03	F227	PICTURE X.	RON
00632	C	006330				RON
00633	C	006340				RON
00634	C	006350	02	DUM7.		RON
00635	C	006360				RON
00636	C	006370	03	FILLER	PICTURE X(37).	RON
00637	C	006380				RON
00638	C	006390				RON
00639	C	006400	02	DITCH-SURVIVAL.		RON
00640	C	006410				RON
00641	C	006420	03	F228	PICTURE X.	RON
00642	C	006430	03	F229	PICTURE XX.	RON
00643	C	006440	03	F230		RON
00644	C	006450	04	F23001	PICTURE XXX.	RON
00645	C	006460	04	F23002	PICTURE XXX.	RON
00646	C	006470	03	F231	PICTURE X.	RON
00647	C	006480	03	F232	PICTURE X.	RON
00648	C	006490	03	FILLER	PICTURE X.	RON
00649	C	006500	03	F233	PICTURE X.	RON
00650	C	006510	03	F234	PICTURE X.	RON
00651	C	006520	03	F235	PICTURE X.	RON
00652	C	006530	03	F236	PICTURE X.	RON
00653	C	006540	03	F237	PICTURE X.	RON
00654	C	006550	03	F238	PICTURE X.	RON
00655	C	006560	03	F239	PICTURE X.	RON
00656	C	006570	02	DUM8.		RON

00657 C 006580 03 FILLER PICTURE X(127).
00658 006590 FD NTSB-TAPE
00659 006600 RECORDING MODE IS F
00660 006610 LABEL RECORDS ARE OMITTED
00661 006620 DATA RECORD IS NTSB-OUT.
00662 006630 01 NTSB-OUT PIC X(1600).
00663 006640 WORKING-STORAGE SECTION.
00664 006650 77 HISAVE PIC 9(3) VALUE 455.
00665 006660 77 HI PIC 9(3).
00666 006670 77 LU PIC 9(3) VALUE ZERO.
00667 006680 77 I PIC 9(3).
00668 006690 77 SEARCH-WORD PIC X(11).
00669 006700 77 FOUND-WORD PIC X VALUE ZERO.
00670 006710 77 REPLY-77 PIC X(4).
00671 006720 01 NTSB-WORK-01.
00672 006730 02 NTSB-WORK PIC X(1600).
00673 006740 01 FIELD-01.
00674 006750 02 FIELD-1 PIC X(3).
00675 006760 02 FIELD-3 PIC XX.
00676 006770 02 FIELD-2 PIC X(6).
00677 006780 01 MK-MOD-01.
00678 006790 02 MK-MOD-02.
00679 006800 03 FILLER PIC X(11) VALUE '00201100'.
00680 006810 03 FILLER PIC X(11) VALUE '00201500'.
00681 006820 03 FILLER PIC X(11) VALUE '00201500-A'.
00682 006830 03 FILLER PIC X(11) VALUE '00201500-B'.
00683 006840 03 FILLER PIC X(11) VALUE '00201500-S'.
00684 006850 03 FILLER PIC X(11) VALUE '00201500B'.
00685 006860 03 FILLER PIC X(11) VALUE '00201500S'.
00686 006870 03 FILLER PIC X(11) VALUE '00201560'.
00687 006880 03 FILLER PIC X(11) VALUE '00201560-A'.
00688 006890 03 FILLER PIC X(11) VALUE '00201560-E'.
00689 006900 03 FILLER PIC X(11) VALUE '00201560A'.
00690 006910 03 FILLER PIC X(11) VALUE '00201560E'.
00691 006920 03 FILLER PIC X(11) VALUE '00202560-F'.
00692 006930 03 FILLER PIC X(11) VALUE '00202560F'.
00693 006940 03 FILLER PIC X(11) VALUE '00202680'.
00694 006950 03 FILLER PIC X(11) VALUE '00202680-E'.
00695 006960 03 FILLER PIC X(11) VALUE '00202680-F'.
00696 006970 03 FILLER PIC X(11) VALUE '00202680-FL'.
00697 006980 03 FILLER PIC X(11) VALUE '00202680-V'.
00698 006990 03 FILLER PIC X(11) VALUE '00202680E'.
00699 007000 03 FILLER PIC X(11) VALUE '00202680F'.
00700 007010 03 FILLER PIC X(11) VALUE '00202680FL'.
00701 007020 03 FILLER PIC X(11) VALUE '00202680FLP'.
00702 007030 03 FILLER PIC X(11) VALUE '00202680FP'.
00703 007040 03 FILLER PIC X(11) VALUE '00202680S'.
00704 007050 03 FILLER PIC X(11) VALUE '00202680T'.
00705 007060 03 FILLER PIC X(11) VALUE '00202680V'.
00706 007070 03 FILLER PIC X(11) VALUE '00202680W'.
00707 007080 03 FILLER PIC X(11) VALUE '00202681'.
00708 007090 03 FILLER PIC X(11) VALUE '00202690'.
00709 007100 03 FILLER PIC X(11) VALUE '00202690A'.
00710 007110 03 FILLER PIC X(11) VALUE '00205112'.
00711 007120 03 FILLER PIC X(11) VALUE '003127ECA'.
00712 007130 03 FILLER PIC X(11) VALUE '003125-7CCM'.
00713 007140 03 FILLER PIC X(11) VALUE '00312578CM'.
00714 007150 03 FILLER PIC X(11) VALUE '0031257EC'.
00715 007160 03 FILLER PIC X(11) VALUE '003127AC'.
00716 007170 03 FILLER PIC X(11) VALUE '003127ACA'.
00717 007180 03 FILLER PIC X(11) VALUE '003127ACM'.
00718 007190 03 FILLER PIC X(11) VALUE '003127BC'.
00719 007200 03 FILLER PIC X(11) VALUE '003127BCM'.
00720 007210 03 FILLER PIC X(11) VALUE '003127CCM'.
00721 007220 03 FILLER PIC X(11) VALUE '003127CGAA'.
00722 007230 03 FILLER PIC X(11) VALUE '003127DC'.
00723 007240 03 FILLER PIC X(11) VALUE '003127EAC'.
00724 007250 03 FILLER PIC X(11) VALUE '003127EC'.
00725 007260 03 FILLER PIC X(11) VALUE '003127ECA'.
00726 007270 03 FILLER PIC X(11) VALUE '003127FC'.
00727 007280 03 FILLER PIC X(11) VALUE '003127GC'.
00728 007290 03 FILLER PIC X(11) VALUE '003127GC-AA'.
00729 007300 03 FILLER PIC X(11) VALUE '003127GCA'.

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00730	009800	03	FILLER	PIC	X(11)	VALUE	003127GCAA
00731	009900	03	FILLER	PIC	X(11)	VALUE	003127GCB
00732	010000	03	FILLER	PIC	X(11)	VALUE	003127GCB
00733	010100	03	FILLER	PIC	X(11)	VALUE	003127GCB
00734	010200	03	FILLER	PIC	X(11)	VALUE	003127HC
00735	010300	03	FILLER	PIC	X(11)	VALUE	003127KC-AB
00736	010400	03	FILLER	PIC	X(11)	VALUE	003127KCAB
00737	010500	03	FILLER	PIC	X(11)	VALUE	003198KCAB
00738	010600	03	FILLER	PIC	X(11)	VALUE	02217C-18S
00739	010700	03	FILLER	PIC	X(11)	VALUE	02217C18S
00740	010800	03	FILLER	PIC	X(11)	VALUE	02217D-18-S
00741	010900	03	FILLER	PIC	X(11)	VALUE	02217D-18S
00742	011000	03	FILLER	PIC	X(11)	VALUE	02217D18
00743	011100	03	FILLER	PIC	X(11)	VALUE	02217D18C
00744	011200	03	FILLER	PIC	X(11)	VALUE	02217D18S
00745	011300	03	FILLER	PIC	X(11)	VALUE	02217D185
00746	011400	03	FILLER	PIC	X(11)	VALUE	02217E18
00747	011500	03	FILLER	PIC	X(11)	VALUE	02217E18E
00748	011600	03	FILLER	PIC	X(11)	VALUE	02217E18S
00749	011700	03	FILLER	PIC	X(11)	VALUE	02217G-18-S
00750	011800	03	FILLER	PIC	X(11)	VALUE	02217G18S
00751	011900	03	FILLER	PIC	X(11)	VALUE	02217H18
00752	012000	03	FILLER	PIC	X(11)	VALUE	02217H18S
00753	012100	03	FILLER	PIC	X(11)	VALUE	02217I18
00754	012200	03	FILLER	PIC	X(11)	VALUE	02220A-36
00755	012300	03	FILLER	PIC	X(11)	VALUE	02220A33
00756	012400	03	FILLER	PIC	X(11)	VALUE	02220A36
00757	012500	03	FILLER	PIC	X(11)	VALUE	02220B33
00758	012600	03	FILLER	PIC	X(11)	VALUE	02220B35
00759	012700	03	FILLER	PIC	X(11)	VALUE	02220C35
00760	012800	03	FILLER	PIC	X(11)	VALUE	02220D35
00761	012900	03	FILLER	PIC	X(11)	VALUE	02220E33
00762	013000	03	FILLER	PIC	X(11)	VALUE	02220E33A
00763	013100	03	FILLER	PIC	X(11)	VALUE	02220F33
00764	013200	03	FILLER	PIC	X(11)	VALUE	02220F33A
00765	013300	03	FILLER	PIC	X(11)	VALUE	02220G33
00766	013400	03	FILLER	PIC	X(11)	VALUE	02220H-35
00767	013500	03	FILLER	PIC	X(11)	VALUE	02220H35
00768	013600	03	FILLER	PIC	X(11)	VALUE	02220J35
00769	013700	03	FILLER	PIC	X(11)	VALUE	02220K35
00770	013800	03	FILLER	PIC	X(11)	VALUE	02220M-35
00771	013900	03	FILLER	PIC	X(11)	VALUE	02220M35
00772	014000	03	FILLER	PIC	X(11)	VALUE	02220M35B
00773	014100	03	FILLER	PIC	X(11)	VALUE	02220N35
00774	014200	03	FILLER	PIC	X(11)	VALUE	02220P-35
00775	014300	03	FILLER	PIC	X(11)	VALUE	02220P35
00776	014400	03	FILLER	PIC	X(11)	VALUE	02220S-35
00777	014500	03	FILLER	PIC	X(11)	VALUE	02220S35
00778	014600	03	FILLER	PIC	X(11)	VALUE	02220V35
00779	014700	03	FILLER	PIC	X(11)	VALUE	02220V35-TC
00780	014800	03	FILLER	PIC	X(11)	VALUE	02220V35A
00781	014900	03	FILLER	PIC	X(11)	VALUE	02220V35ATC
00782	015000	03	FILLER	PIC	X(11)	VALUE	02220V35B
00783	015100	03	FILLER	PIC	X(11)	VALUE	02220V35TC
00784	015200	03	FILLER	PIC	X(11)	VALUE	0222033
00785	015300	03	FILLER	PIC	X(11)	VALUE	0222035
00786	015400	03	FILLER	PIC	X(11)	VALUE	0222035-A33
00787	015500	03	FILLER	PIC	X(11)	VALUE	0222035-B33
00788	015600	03	FILLER	PIC	X(11)	VALUE	0222035-C33
00789	015700	03	FILLER	PIC	X(11)	VALUE	0222035-E33
00790	015800	03	FILLER	PIC	X(11)	VALUE	0222035-G33
00791	015900	03	FILLER	PIC	X(11)	VALUE	0222035-33
00792	016000	03	FILLER	PIC	X(11)	VALUE	0222035B33
00793	016100	03	FILLER	PIC	X(11)	VALUE	0222035C33A
00794	016200	03	FILLER	PIC	X(11)	VALUE	0222035S
00795	016300	03	FILLER	PIC	X(11)	VALUE	0222036
00796	016400	03	FILLER	PIC	X(11)	VALUE	02222A55
00797	016500	03	FILLER	PIC	X(11)	VALUE	02222A65
00798	016600	03	FILLER	PIC	X(11)	VALUE	02223A5-88
00799	016700	03	FILLER	PIC	X(11)	VALUE	02223A90
00800	016800	03	FILLER	PIC	X(11)	VALUE	02223B65
00801	016900	03	FILLER	PIC	X(11)	VALUE	02223B80
00802	017000	03	FILLER	PIC	X(11)	VALUE	02223B90

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00803	017100	03	FILLER	PIC	X(11)	VALUE	02223C90
00804	017200	03	FILLER	PIC	X(11)	VALUE	02223E90
00805	017300	03	FILLER	PIC	X(11)	VALUE	0222365
00806	017400	03	FILLER	PIC	X(11)	VALUE	0222365-A80
00807	017500	03	FILLER	PIC	X(11)	VALUE	0222365-A90
00808	017600	03	FILLER	PIC	X(11)	VALUE	0222365-B80
00809	017700	03	FILLER	PIC	X(11)	VALUE	0222365-80
00810	017800	03	FILLER	PIC	X(11)	VALUE	0222365-88
00811	017900	03	FILLER	PIC	X(11)	VALUE	0222365A90
00812	018000	03	FILLER	PIC	X(11)	VALUE	0222365S
00813	018100	03	FILLER	PIC	X(11)	VALUE	0222370
00814	018200	03	FILLER	PIC	X(11)	VALUE	0222390
00815	018300	03	FILLER	PIC	X(11)	VALUE	02224855
00816	018400	03	FILLER	PIC	X(11)	VALUE	02224855-95
00817	018500	03	FILLER	PIC	X(11)	VALUE	02224C55
00818	018600	03	FILLER	PIC	X(11)	VALUE	02224D55
00819	018700	03	FILLER	PIC	X(11)	VALUE	02224E55
00820	018800	03	FILLER	PIC	X(11)	VALUE	02224E58
00821	018900	03	FILLER	PIC	X(11)	VALUE	0222455
00822	019000	03	FILLER	PIC	X(11)	VALUE	0222456T
00823	019100	03	FILLER	PIC	X(11)	VALUE	0222456TC
00824	019200	03	FILLER	PIC	X(11)	VALUE	0222458
00825	019300	03	FILLER	PIC	X(11)	VALUE	02225A-23
00826	019400	03	FILLER	PIC	X(11)	VALUE	02225A-23A
00827	019500	03	FILLER	PIC	X(11)	VALUE	02225A19
00828	019600	03	FILLER	PIC	X(11)	VALUE	02225A23
00829	019700	03	FILLER	PIC	X(11)	VALUE	02225A23-19
00830	019800	03	FILLER	PIC	X(11)	VALUE	02225A23-24
00831	019900	03	FILLER	PIC	X(11)	VALUE	02225A23A
00832	020000	03	FILLER	PIC	X(11)	VALUE	02225A24R
00833	020100	03	FILLER	PIC	X(11)	VALUE	02225B-23
00834	020200	03	FILLER	PIC	X(11)	VALUE	02225HE-23
00835	020300	03	FILLER	PIC	X(11)	VALUE	02225HE23
00836	020400	03	FILLER	PIC	X(11)	VALUE	02225B19
00837	020500	03	FILLER	PIC	X(11)	VALUE	02225B23
00838	020600	03	FILLER	PIC	X(11)	VALUE	02225B23-19
00839	020700	03	FILLER	PIC	X(11)	VALUE	02225C-23
00840	020800	03	FILLER	PIC	X(11)	VALUE	02225C23
00841	020900	03	FILLER	PIC	X(11)	VALUE	02225M-23
00842	021000	03	FILLER	PIC	X(11)	VALUE	0222519
00843	021100	03	FILLER	PIC	X(11)	VALUE	0222519A
00844	021200	03	FILLER	PIC	X(11)	VALUE	0222523
00845	021300	03	FILLER	PIC	X(11)	VALUE	0222523-19
00846	021400	03	FILLER	PIC	X(11)	VALUE	0222523-19A
00847	021500	03	FILLER	PIC	X(11)	VALUE	02226A60
00848	021600	03	FILLER	PIC	X(11)	VALUE	0222660
00849	021700	03	FILLER	PIC	X(11)	VALUE	02227A99A
00850	021800	03	FILLER	PIC	X(11)	VALUE	02227B99
00851	021900	03	FILLER	PIC	X(11)	VALUE	02227100
00852	022000	03	FILLER	PIC	X(11)	VALUE	0222799
00853	022100	03	FILLER	PIC	X(11)	VALUE	0222799A
00854	022200	03	FILLER	PIC	X(11)	VALUE	03405B-1
00855	022300	03	FILLER	PIC	X(11)	VALUE	03405B-1A
00856	022400	03	FILLER	PIC	X(11)	VALUE	03912150
00857	022500	03	FILLER	PIC	X(11)	VALUE	03912A150
00858	022600	03	FILLER	PIC	X(11)	VALUE	03912A150-K
00859	022700	03	FILLER	PIC	X(11)	VALUE	03912A150K
00860	022800	03	FILLER	PIC	X(11)	VALUE	03912A150K
00861	022900	03	FILLER	PIC	X(11)	VALUE	03912A150L
00862	023000	03	FILLER	PIC	X(11)	VALUE	03912150F
00863	023100	03	FILLER	PIC	X(11)	VALUE	03912150K
00864	023200	03	FILLER	PIC	X(11)	VALUE	03912150
00865	023300	03	FILLER	PIC	X(11)	VALUE	03912150A
00866	023400	03	FILLER	PIC	X(11)	VALUE	03912150B
00867	023500	03	FILLER	PIC	X(11)	VALUE	03912150C
00868	023600	03	FILLER	PIC	X(11)	VALUE	03912150C
00869	023700	03	FILLER	PIC	X(11)	VALUE	03912150E
00870	023800	03	FILLER	PIC	X(11)	VALUE	03912150F
00871	023900	03	FILLER	PIC	X(11)	VALUE	03912150G
00872	024000	03	FILLER	PIC	X(11)	VALUE	03912150H
00873	024100	03	FILLER	PIC	X(11)	VALUE	03912150J
00874	024200	03	FILLER	PIC	X(11)	VALUE	03912150K
00875	024300	03	FILLER	PIC	X(11)	VALUE	03912150L

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00876	024400	03	FILLER	PIC	X(11)	VALUE	03914172
00877	024500	03	FILLER	PIC	X(11)	VALUE	03914172A
00878	024600	03	FILLER	PIC	X(11)	VALUE	03914172B
00879	024700	03	FILLER	PIC	X(11)	VALUE	03914172C
00880	024800	03	FILLER	PIC	X(11)	VALUE	03914172D
00881	024900	03	FILLER	PIC	X(11)	VALUE	03914172E
00882	025000	03	FILLER	PIC	X(11)	VALUE	03914172F
00883	025100	03	FILLER	PIC	X(11)	VALUE	03914172G
00884	025200	03	FILLER	PIC	X(11)	VALUE	03914172H
00885	025300	03	FILLER	PIC	X(11)	VALUE	03914172I
00886	025400	03	FILLER	PIC	X(11)	VALUE	03914172K
00887	025500	03	FILLER	PIC	X(11)	VALUE	03914172L
00888	025600	03	FILLER	PIC	X(11)	VALUE	03914172M
00889	025700	03	FILLER	PIC	X(11)	VALUE	03914172S
00890	025800	03	FILLER	PIC	X(11)	VALUE	03914177
00891	025900	03	FILLER	PIC	X(11)	VALUE	03916150
00892	026000	03	FILLER	PIC	X(11)	VALUE	03916150
00893	026100	03	FILLER	PIC	X(11)	VALUE	03916180A
00894	026200	03	FILLER	PIC	X(11)	VALUE	03916180B
00895	026300	03	FILLER	PIC	X(11)	VALUE	03916180C
00896	026400	03	FILLER	PIC	X(11)	VALUE	03916180D
00897	026500	03	FILLER	PIC	X(11)	VALUE	03916180E
00898	026600	03	FILLER	PIC	X(11)	VALUE	03916180F
00899	026700	03	FILLER	PIC	X(11)	VALUE	03916180G
00900	026800	03	FILLER	PIC	X(11)	VALUE	03916180H
00901	026900	03	FILLER	PIC	X(11)	VALUE	03916180J
00902	027000	03	FILLER	PIC	X(11)	VALUE	03916182
00903	027100	03	FILLER	PIC	X(11)	VALUE	03916182L
00904	027200	03	FILLER	PIC	X(11)	VALUE	03917180
00905	027300	03	FILLER	PIC	X(11)	VALUE	03917182
00906	027400	03	FILLER	PIC	X(11)	VALUE	03917182-E
00907	027500	03	FILLER	PIC	X(11)	VALUE	03917182A
00908	027600	03	FILLER	PIC	X(11)	VALUE	03917182B
00909	027700	03	FILLER	PIC	X(11)	VALUE	03917182C
00910	027800	03	FILLER	PIC	X(11)	VALUE	03917182D
00911	027900	03	FILLER	PIC	X(11)	VALUE	03917182E
00912	028000	03	FILLER	PIC	X(11)	VALUE	03917182F
00913	028100	03	FILLER	PIC	X(11)	VALUE	03917182G
00914	028200	03	FILLER	PIC	X(11)	VALUE	03917182H
00915	028300	03	FILLER	PIC	X(11)	VALUE	03917182J
00916	028400	03	FILLER	PIC	X(11)	VALUE	03917182K
00917	028500	03	FILLER	PIC	X(11)	VALUE	03917182L
00918	028600	03	FILLER	PIC	X(11)	VALUE	03917182M
00919	028700	03	FILLER	PIC	X(11)	VALUE	03917182N
00920	028800	03	FILLER	PIC	X(11)	VALUE	03917182P
00921	028900	03	FILLER	PIC	X(11)	VALUE	03917182R
00922	029000	03	FILLER	PIC	X(11)	VALUE	03917182S
00923	029100	03	FILLER	PIC	X(11)	VALUE	03917185
00924	029200	03	FILLER	PIC	X(11)	VALUE	03919T-210
00925	029300	03	FILLER	PIC	X(11)	VALUE	03919T210
00926	029400	03	FILLER	PIC	X(11)	VALUE	03919T210-H
00927	029500	03	FILLER	PIC	X(11)	VALUE	03919T210F
00928	029600	03	FILLER	PIC	X(11)	VALUE	03919T210G
00929	029700	03	FILLER	PIC	X(11)	VALUE	03919T210H
00930	029800	03	FILLER	PIC	X(11)	VALUE	03919T210J
00931	029900	03	FILLER	PIC	X(11)	VALUE	03919T210K
00932	030000	03	FILLER	PIC	X(11)	VALUE	03919T210L
00933	030100	03	FILLER	PIC	X(11)	VALUE	03919210
00934	030200	03	FILLER	PIC	X(11)	VALUE	03919210-5
00935	030300	03	FILLER	PIC	X(11)	VALUE	03919210A
00936	030400	03	FILLER	PIC	X(11)	VALUE	03919210B
00937	030500	03	FILLER	PIC	X(11)	VALUE	03919210C
00938	030600	03	FILLER	PIC	X(11)	VALUE	03919210D
00939	030700	03	FILLER	PIC	X(11)	VALUE	03919210E
00940	030800	03	FILLER	PIC	X(11)	VALUE	03919210F
00941	030900	03	FILLER	PIC	X(11)	VALUE	03919210G
00942	031000	03	FILLER	PIC	X(11)	VALUE	03919210H
00943	031100	03	FILLER	PIC	X(11)	VALUE	03919210J
00944	031200	03	FILLER	PIC	X(11)	VALUE	03919210K
00945	031300	03	FILLER	PIC	X(11)	VALUE	03919210L
00946	031400	03	FILLER	PIC	X(11)	VALUE	03919210T
00947	031500	03	FILLER	PIC	X(11)	VALUE	03922T310P
00948	031600	03	FILLER	PIC	X(11)	VALUE	03922T310Q

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00949	031700	03	FILLER	PIC	X(11)	VALUE	*03922310P
00950	031800	03	FILLER	PIC	X(11)	VALUE	*03922310
00951	031900	03	FILLER	PIC	X(11)	VALUE	*03922310A
00952	032000	03	FILLER	PIC	X(11)	VALUE	*03922310B
00953	032100	03	FILLER	PIC	X(11)	VALUE	*03922310C
00954	032200	03	FILLER	PIC	X(11)	VALUE	*03922310D
00955	032300	03	FILLER	PIC	X(11)	VALUE	*03922310E
00956	032400	03	FILLER	PIC	X(11)	VALUE	*03922310G
00957	032500	03	FILLER	PIC	X(11)	VALUE	*03922310H
00958	032600	03	FILLER	PIC	X(11)	VALUE	*03922310I
00959	032700	03	FILLER	PIC	X(11)	VALUE	*03922310J
00960	032800	03	FILLER	PIC	X(11)	VALUE	*03922310K
00961	032900	03	FILLER	PIC	X(11)	VALUE	*03922310L
00962	033000	03	FILLER	PIC	X(11)	VALUE	*03922310N
00963	033100	03	FILLER	PIC	X(11)	VALUE	*03922310P
00964	033200	03	FILLER	PIC	X(11)	VALUE	*03922310Q
00965	033300	03	FILLER	PIC	X(11)	VALUE	*039226A185E
00966	033400	03	FILLER	PIC	X(11)	VALUE	*039226A185F
00967	033500	03	FILLER	PIC	X(11)	VALUE	*039226185
00968	033600	03	FILLER	PIC	X(11)	VALUE	*039226185A
00969	033700	03	FILLER	PIC	X(11)	VALUE	*039226185B
00970	033800	03	FILLER	PIC	X(11)	VALUE	*039226185C
00971	033900	03	FILLER	PIC	X(11)	VALUE	*039226185D
00972	034000	03	FILLER	PIC	X(11)	VALUE	*039226185E
00973	034100	03	FILLER	PIC	X(11)	VALUE	*039226185F
00974	034200	03	FILLER	PIC	X(11)	VALUE	*03927340
00975	034300	03	FILLER	PIC	X(11)	VALUE	*039299P206
00976	034400	03	FILLER	PIC	X(11)	VALUE	*039299P206A
00977	034500	03	FILLER	PIC	X(11)	VALUE	*039299P206B
00978	034600	03	FILLER	PIC	X(11)	VALUE	*039299P206C
00979	034700	03	FILLER	PIC	X(11)	VALUE	*039299TP206
00980	034800	03	FILLER	PIC	X(11)	VALUE	*039299TP206B
00981	034900	03	FILLER	PIC	X(11)	VALUE	*039299TP206C
00982	035000	03	FILLER	PIC	X(11)	VALUE	*039299TP206D
00983	035100	03	FILLER	PIC	X(11)	VALUE	*039299TP206E
00984	035200	03	FILLER	PIC	X(11)	VALUE	*039299TP206A
00985	035300	03	FILLER	PIC	X(11)	VALUE	*039299TP206B
00986	035400	03	FILLER	PIC	X(11)	VALUE	*039299TP206C
00987	035500	03	FILLER	PIC	X(11)	VALUE	*039299TP206D
00988	035600	03	FILLER	PIC	X(11)	VALUE	*039299TP206E
00989	035700	03	FILLER	PIC	X(11)	VALUE	*039299TP206F
00990	035800	03	FILLER	PIC	X(11)	VALUE	*039299TP206G
00991	035900	03	FILLER	PIC	X(11)	VALUE	*039299U206
00992	036000	03	FILLER	PIC	X(11)	VALUE	*039299U206A
00993	036100	03	FILLER	PIC	X(11)	VALUE	*039299U206B
00994	036200	03	FILLER	PIC	X(11)	VALUE	*039299U206C
00995	036300	03	FILLER	PIC	X(11)	VALUE	*039299U206D
00996	036400	03	FILLER	PIC	X(11)	VALUE	*039299U206E
00997	036500	03	FILLER	PIC	X(11)	VALUE	*039299U206F
00998	036600	03	FILLER	PIC	X(11)	VALUE	*039299U206
00999	036700	03	FILLER	PIC	X(11)	VALUE	*039299U206A
01000	036800	03	FILLER	PIC	X(11)	VALUE	*039299U206B
01001	036900	03	FILLER	PIC	X(11)	VALUE	*039299U206C
01002	037000	03	FILLER	PIC	X(11)	VALUE	*039299U206D
01003	037100	03	FILLER	PIC	X(11)	VALUE	*039301-337
01004	037200	03	FILLER	PIC	X(11)	VALUE	*039301-337C
01005	037300	03	FILLER	PIC	X(11)	VALUE	*039301337
01006	037400	03	FILLER	PIC	X(11)	VALUE	*039301337C
01007	037500	03	FILLER	PIC	X(11)	VALUE	*039301337D
01008	037600	03	FILLER	PIC	X(11)	VALUE	*039301337E
01009	037700	03	FILLER	PIC	X(11)	VALUE	*039301337F
01010	037800	03	FILLER	PIC	X(11)	VALUE	*03930337
01011	037900	03	FILLER	PIC	X(11)	VALUE	*03930337A
01012	038000	03	FILLER	PIC	X(11)	VALUE	*03930337B
01013	038100	03	FILLER	PIC	X(11)	VALUE	*03930337C
01014	038200	03	FILLER	PIC	X(11)	VALUE	*03930337D
01015	038300	03	FILLER	PIC	X(11)	VALUE	*03930337E
01016	038400	03	FILLER	PIC	X(11)	VALUE	*03930337F
01017	038500	03	FILLER	PIC	X(11)	VALUE	*03930337G
01018	038600	03	FILLER	PIC	X(11)	VALUE	*03931401
01019	038700	03	FILLER	PIC	X(11)	VALUE	*03931401A
01020	038800	03	FILLER	PIC	X(11)	VALUE	*03931401B
01021	038900	03	FILLER	PIC	X(11)	VALUE	*03931402

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01022	039000	03	FILLER	PIC	X(11)	VALUE	*03931402B
01023	039100	03	FILLER	PIC	X(11)	VALUE	*03931411
01024	039200	03	FILLER	PIC	X(11)	VALUE	*03931411A
01025	039300	03	FILLER	PIC	X(11)	VALUE	*03931414
01026	039400	03	FILLER	PIC	X(11)	VALUE	*03932A-188
01027	039500	03	FILLER	PIC	X(11)	VALUE	*03932AG188
01028	039600	03	FILLER	PIC	X(11)	VALUE	*03932A188
01029	039700	03	FILLER	PIC	X(11)	VALUE	*03932A188A
01030	039800	03	FILLER	PIC	X(11)	VALUE	*03932A188B
01031	039900	03	FILLER	PIC	X(11)	VALUE	*03932188
01032	040000	03	FILLER	PIC	X(11)	VALUE	*03932188A
01033	040100	03	FILLER	PIC	X(11)	VALUE	*03932188B
01034	040200	03	FILLER	PIC	X(11)	VALUE	*03932188C
01035	040300	03	FILLER	PIC	X(11)	VALUE	*03933C177
01036	040400	03	FILLER	PIC	X(11)	VALUE	*03933177
01037	040500	03	FILLER	PIC	X(11)	VALUE	*03933177A
01038	040600	03	FILLER	PIC	X(11)	VALUE	*03933177B
01039	040700	03	FILLER	PIC	X(11)	VALUE	*03934+21
01040	040800	03	FILLER	PIC	X(11)	VALUE	*03934+21A
01041	040900	03	FILLER	PIC	X(11)	VALUE	*03934421B
01042	041000	03	FILLER	PIC	X(11)	VALUE	*03935T207
01043	041100	03	FILLER	PIC	X(11)	VALUE	*03935207
01044	041200	03	FILLER	PIC	X(11)	VALUE	*03936177 RG
01045	041300	03	FILLER	PIC	X(11)	VALUE	*03936177RG
01046	041400	03	FILLER	PIC	X(11)	VALUE	*0560114-19
01047	041500	03	FILLER	PIC	X(11)	VALUE	*0560114-192
01048	041600	03	FILLER	PIC	X(11)	VALUE	*0560114-193
01049	041700	03	FILLER	PIC	X(11)	VALUE	*056011419-2
01050	041800	03	FILLER	PIC	X(11)	VALUE	*0560114193A
01051	041900	03	FILLER	PIC	X(11)	VALUE	*05603A-1
01052	042000	03	FILLER	PIC	X(11)	VALUE	*05603AA-1
01053	042100	03	FILLER	PIC	X(11)	VALUE	*05603AA-1A
01054	042200	03	FILLER	PIC	X(11)	VALUE	*05603AA-1B
01055	042300	03	FILLER	PIC	X(11)	VALUE	*05603AA1
01056	042400	03	FILLER	PIC	X(11)	VALUE	*05603AA1-A
01057	042500	03	FILLER	PIC	X(11)	VALUE	*05603AA1-B
01058	042600	03	FILLER	PIC	X(11)	VALUE	*05603AA1-1A
01059	042700	03	FILLER	PIC	X(11)	VALUE	*05603AA1A
01060	042800	03	FILLER	PIC	X(11)	VALUE	*05603AA1B
01061	042900	03	FILLER	PIC	X(11)	VALUE	*05605AA-5
01062	043000	03	FILLER	PIC	X(11)	VALUE	*05605AA5
01063	043100	03	FILLER	PIC	X(11)	VALUE	*07113G-164
01064	043200	03	FILLER	PIC	X(11)	VALUE	*07113G-164A
01065	043300	03	FILLER	PIC	X(11)	VALUE	*07113G164
01066	043400	03	FILLER	PIC	X(11)	VALUE	*07113G164A
01067	043500	03	FILLER	PIC	X(11)	VALUE	*07113G64A
01068	043600	03	FILLER	PIC	X(11)	VALUE	*07113164
01069	043700	03	FILLER	PIC	X(11)	VALUE	*07113164A
01070	043800	03	FILLER	PIC	X(11)	VALUE	*10103M-20
01071	043900	03	FILLER	PIC	X(11)	VALUE	*10103M-20C
01072	044000	03	FILLER	PIC	X(11)	VALUE	*10103M-20C
01073	044100	03	FILLER	PIC	X(11)	VALUE	*10103M-20F
01074	044200	03	FILLER	PIC	X(11)	VALUE	*10103M-20G
01075	044300	03	FILLER	PIC	X(11)	VALUE	*10103MK-20E
01076	044400	03	FILLER	PIC	X(11)	VALUE	*10103M20-C
01077	044500	03	FILLER	PIC	X(11)	VALUE	*10103M20-F
01078	044600	03	FILLER	PIC	X(11)	VALUE	*10103M20B
01079	044700	03	FILLER	PIC	X(11)	VALUE	*10103M20C
01080	044800	03	FILLER	PIC	X(11)	VALUE	*10103M20D
01081	044900	03	FILLER	PIC	X(11)	VALUE	*10103M20E
01082	045000	03	FILLER	PIC	X(11)	VALUE	*10103M20F
01083	045100	03	FILLER	PIC	X(11)	VALUE	*10103M20G
01084	045200	03	FILLER	PIC	X(11)	VALUE	*10103M20H
01085	045300	03	FILLER	PIC	X(11)	VALUE	*10103M21
01086	045400	03	FILLER	PIC	X(11)	VALUE	*10103M21F
01087	045500	03	FILLER	PIC	X(11)	VALUE	*1010320F
01088	045600	03	FILLER	PIC	X(11)	VALUE	*10103201
01089	045700	03	FILLER	PIC	X(11)	VALUE	*10104M-22
01090	045800	03	FILLER	PIC	X(11)	VALUE	*10104M20F
01091	045900	03	FILLER	PIC	X(11)	VALUE	*10104M22
01092	046000	03	FILLER	PIC	X(11)	VALUE	*12420PA-18
01093	046100	03	FILLER	PIC	X(11)	VALUE	*12420PA-18A
01094	046200	03	FILLER	PIC	X(11)	VALUE	*12420PA-18C


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01095 046300 03 FILLER PIC X(11) VALUE *12420PA-18S*
01096 046400 03 FILLER PIC X(11) VALUE *12420PA18
01097 046500 03 FILLER PIC X(11) VALUE *12424PA-23
01098 046600 03 FILLER PIC X(11) VALUE *12424PA23
01099 046700 03 FILLER PIC X(11) VALUE *12425PA-23
01100 046800 03 FILLER PIC X(11) VALUE *12425PA-24
01101 046900 03 FILLER PIC X(11) VALUE *12425PA24
01102 047000 03 FILLER PIC X(11) VALUE *12426PA-25
01103 047100 03 FILLER PIC X(11) VALUE *12426PA25
01104 047200 03 FILLER PIC X(11) VALUE *12428PA-24
01105 047300 03 FILLER PIC X(11) VALUE *12428PA-28
01106 047400 03 FILLER PIC X(11) VALUE *12428PA-28R
01107 047500 03 FILLER PIC X(11) VALUE *12428PA-28S
01108 047600 03 FILLER PIC X(11) VALUE *12428PA28
01109 047700 03 FILLER PIC X(11) VALUE *12428PA28-R
01110 047800 03 FILLER PIC X(11) VALUE *12429PA-30
01111 047900 03 FILLER PIC X(11) VALUE *12429PA-30B
01112 048000 03 FILLER PIC X(11) VALUE *12429PA-32
01113 048100 03 FILLER PIC X(11) VALUE *12429PA-39
01114 048200 03 FILLER PIC X(11) VALUE *12429PA30
01115 048300 03 FILLER PIC X(11) VALUE *12430PA-32
01116 048400 03 FILLER PIC X(11) VALUE *12430PA32
01117 048500 03 FILLER PIC X(11) VALUE *12431PA-31
01118 048600 03 FILLER PIC X(11) VALUE *12431PA-31A
01119 048700 03 FILLER PIC X(11) VALUE *12431PA-31P
01120 048800 03 FILLER PIC X(11) VALUE *12432PA-34
01121 048900 03 FILLER PIC X(11) VALUE *14803S-2D
01122 049000 03 FILLER PIC X(11) VALUE *14803S-2R
01123 049100 03 FILLER PIC X(11) VALUE *14803S2R
01124 049200 03 FILLER PIC X(11) VALUE *14803THRUSH
01125 049300 03 FILLER PIC X(11) VALUE *14803600S2D
01126 049400 03 FILLER PIC X(11) VALUE *14803600S2R
01127 049500 03 FILLER PIC X(11) VALUE *14803600S24
01128 049600 03 FILLER PIC X(11) VALUE *14803600S2R
01129 049700 03 FILLER PIC X(11) VALUE *21601MU-2
01130 049800 03 FILLER PIC X(11) VALUE *21601MU-2B
01131 049900 03 FILLER PIC X(11) VALUE *21601MU-2F
01132 050000 03 FILLER PIC X(11) VALUE *21601MU-2G
01133 050100 03 FILLER PIC X(11) VALUE *21601MU2B20*
01134 050200 02 MK-MOD REDEFINES MK-MOD-02 OCCURS 550 TIMES PIC X(11).
01135 050300 PROCEDURE DIVISION.
01136 050400 OPEN INPUT NTSB OUTPUT NTSB-TAPE.
01137 050500 READ-NTSB.
01138 050600 READ NTSB INTO NTSB-WORK-01 AT END GO TO END-OF-TAPE.
01139 050700 MOVE F012 TO FIELD-1.
01140 050800 MOVE F007 TO FIELD-2.
01141 050900 MOVE F013 TO FIELD-3.
01142 051000 MOVE FIELD-01 TO SEARCH-WORD.
01143 051100 MOVE ZERO TO FOUND-WORD.
01144 051200 PERFORM MAKE-MODEL THRU END-B1.
01145 051300 IF FOUND-WORD = ZERO GO TO READ-NTSB.
01146 051400 WRITE NTSB-DUT FROM NTSB-REC.
01147 051500 GO TO READ-NTSB.
01148 051600 END-OF-TAPE.
01149 051700 CLOSE NTSB.
01150 051800 DISPLAY 'IF THIS IS THE LAST FILE ENTER LAST'
01151 051900 UPON CONSOLE
01152 052000 DISPLAY 'IF NOT THEN MOUNT NEXT TAPE AND ENTER NEXT'
01153 052100 UPON CONSOLE
01154 052200 ACCEPT REPLY-77 FROM CONSOLE.
01155 052300 REPLY-TEST.
01156 052400 IF REPLY-77 = SPACES OR 'NEXT' OR 'LAST' NEXT SENTENCE ELSE
01157 052500 DISPLAY 'YOU GUDDED' UPON CONSOLE
01158 052600 DISPLAY 'REENTER YOUR RESPONSE' UPON CONSOLE
01159 052700 ACCEPT REPLY-77 FROM CONSOLE
01160 052800 GO TO REPLY-TEST.
01161 052900 IF REPLY-77 = 'NEXT'
01162 053000 OPEN INPUT NTSB
01163 053100 GO TO READ-NTSB.
01164 053200 IF REPLY-77 = 'LAST'
01165 053300 CLOSE NTSB-TAPE WITH LOCK.
01166 053400 STOP RUN.
01167 053500 MAKE-MODEL.

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01168 053600 MOVE ZERO TO LO.
01169 053700 MOVE HISAVE TO HI.
01170 053800 AA. COMPUTE I = (HI + LO) / 2.
01171 053900 IF SEARCH-WORD LESS THAN MK-MOD (I)
01172 054000 MOVE I TO HI
01173 054100 GO TO BB.
01174 054200 IF SEARCH-WORD GREATER THAN MK-MOD (I)
01175 054300 MOVE I TO LO
01176 054400 GO TO BB.
01177 054500 MOVE '1' TO FOUND-WORD.
01178 054600 GO TO END-BI.
01179 054700 BB. IF I LESS THAN (HI - LO) GO TO AA.
01180 054800 END-BI.
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[illegible]

00073 C 000590	03 F010	PICTURE X.	RON
00074 C 000600	03 F011	PICTURE XX.	RON
00075 C 000610	03 F012	PICTURE XXX.	RON
00076 C 000620	03 F013	PICTURE XX.	RON
00077 C 000630	03 F014	PICTURE XX.	RON
00078 C 000640	03 F015	PICTURE XX.	RON
00079 C 000650	03 F016	PICTURE X.	RON
00080 C 000660	03 F017	PICTURE X.	RON
00081 C 000670	03 F018	PICTURE X.	RON
00082 C 000680	03 F019	PICTURE X.	RON
00083 C 000690	03 F020	PICTURE X.	RON
00084 C 000700	03 F021	PICTURE X.	RON
00085 C 000710	03 F022	PICTURE X.	RON
00086 C 000720	03 F023.		RON
00087 C 000730	04 F02301	PICTURE X.	RON
00088 C 000740	04 F02302	PICTURE X.	RON
00089 C 000750	03 F024	PICTURE X.	RON
00090 C 000760	03 F025.		RON
00091 C 000770	04 F02501	PICTURE X.	RON
00092 C 000780	04 F02502	PICTURE X.	RON
00093 C 000790	03 F026	PICTURE XX.	RON
00094 C 000800	03 F027	PICTURE X.	RON
00095 C 000810	03 F028.		RON
00096 C 000820	04 F02801	PICTURE X.	RON
00097 C 000830	04 F02802	PICTURE X.	RON
00098 C 000840	03 F029.		RON
00099 C 000850	04 F02901	PICTURE X.	RON
00100 C 000860	04 F02902	PICTURE X.	RON
00101 C 000870	03 F030.		RON
00102 C 000880	04 F03001	PICTURE X.	RON
00103 C 000890	04 F03002	PICTURE X.	RON
00104 C 000900	03 F031.		RON
00105 C 000910	04 F03101	PICTURE X.	RON
00106 C 000920	04 F03102	PICTURE X.	RON
00107 C 000930	03 F032.		RON
00108 C 000940	04 FILLER	PICTURE X(4).	RON
00109 C 000950	04 F03201	PICTURE X.	RON
00110 C 000960	03 F033.		RON
00111 C 000970	04 FILLER	PICTURE X(4).	RON
00112 C 000980	04 F03301	PICTURE X.	RON
00113 C 000990	03 F034.		RON
00114 C 001000	04 FILLER	PICTURE XX.	RON
00115 C 001010	04 F03401	PICTURE X.	RON
00116 C 001020	03 F035.		RON
00117 C 001030	04 FILLER	PICTURE X(13).	RON
00118 C 001040	04 F03501	PICTURE X.	RON
00119 C 001050			RON
00120 C 001060			RON
00121 C 001070	02 EMGCY-COND.		RON
00122 C 001080			RON
00123 C 001090	03 F036	PICTURE X.	RON
00124 C 001100	03 F037.		RON
00125 C 001110	04 F03701	PICTURE X.	RON
00126 C 001120	04 F03702	PICTURE X.	RON
00127 C 001130	03 F038	PICTURE X.	RON
00128 C 001140	03 F039	PICTURE X.	RON
00129 C 001150	03 F040.		RON
00130 C 001160	04 F04001	PICTURE X.	RON
00131 C 001170	04 F04002	PICTURE X.	RON
00132 C 001180			RON
00133 C 001190			RON
00134 C 001200	02 WEATHER.		RON
00135 C 001210			RON
00136 C 001220	03 F041	PICTURE X.	RON
00137 C 001230	03 F042	PICTURE X.	RON
00138 C 001240	03 F043	PICTURE X.	RON
00139 C 001250	03 F044	PICTURE X.	RON
00140 C 001260	03 F045	PICTURE X.	RON
00141 C 001270	03 F046	PICTURE X.	RON
00142 C 001280	03 F047	PICTURE X.	RON
00143 C 001290			RON
00144 C 001300			RON
00145 C 001310	02 AIRPORT.		RON

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001320	03 F048	PICTURE X.	RON
001330	03 F049	PICTURE X.	RON
001340	03 F050	PICTURE X(5).	RON
001350	03 F051	PICTURE X.	RON
001360	03 F052	PICTURE X(17).	RON
001370	03 F053	PICTURE X(5).	RON
001380	03 F054	PICTURE X.	RON
001390	03 F055	PICTURE X.	RON
001400	03 F056.		RON
001410	04 F05601	PICTURE X.	RON
001420	04 F05602	PICTURE X.	RON
001430	03 F057	PICTURE X.	RON
001440	03 F058	PICTURE X.	RON
001450	03 F059	PICTURE X.	RON
001460	03 F060	PICTURE X(5).	RON
001470			RON
001480			RON
001490			RON
001500	02 ITINERARY.		RON
001510	03 F061.		RON
001520	04 F06101	PICTURE X.	RON
001530	04 FILLER	PICTURE X(20).	RON
001540	03 F062.		RON
001550	04 F06201	PICTURE X.	RON
001560	04 FILLER	PICTURE X(20).	RON
001570	03 F063.		RON
001580	04 F06301	PICTURE X.	RON
001590	04 FILLER	PICTURE X(20).	RON
001600			RON
001610			RON
001620	02 ACC-SITE.		RON
001630	03 F064.		RON
001640	04 FILLER	PICTURE X(4).	RON
001650	04 F06401	PICTURE X.	RON
001660	03 F065	PICTURE X.	RON
001670			RON
001680	02 MISC.		RON
001690	03 F066	PICTURE X.	RON
001700	03 F067	PICTURE X.	RON
001710	03 FILLER	PICTURE X.	RON
001720			RON
001730	02 PILOT-DATA.		RON
001740	03 F068.		RON
001750	04 F06801	PICTURE X.	RON
001760	04 F06802	PICTURE X.	RON
001770	03 F069.		RON
001780	04 F06901.		RON
001790	05 F0690101.		RON
001800	06 FILLER	PICTURE X(4).	RON
001810	06 F069010101	PICTURE X.	RON
001820	05 FILLER	PICTURE X.	RON
001830	04 F06902.		RON
001840	05 F0690201.		RON
001850	06 FILLER	PICTURE X(4).	RON
001860	06 F069020101	PICTURE X.	RON
001870	05 FILLER	PICTURE X.	RON
001880	03 F070.		RON
001890	04 F07001.		RON
001900	05 F0700101.		RON
001910	06 FILLER	PICTURE X(4).	RON
001920	06 F070010101	PICTURE X.	RON
001930	05 FILLER	PICTURE X.	RON
001940	04 F07002.		RON
001950	05 F0700201.		RON
001960	06 FILLER	PICTURE X(4).	RON
001970	06 F070020101	PICTURE X.	RON
001980	05 FILLER	PICTURE X.	RON
001990	04 F07003.		RON
002000	05 F0700301.		RON
002010	06 FILLER	PICTURE X(4).	RON
002020	06 F070030101	PICTURE X.	RON
002030	05 FILLER	PICTURE X.	RON
002040	04 F07004.		RON
002050	05 F0700401.		RON
002060	06 FILLER	PICTURE X(4).	RON
002070	06 F070040101	PICTURE X.	RON
002080	05 FILLER	PICTURE X.	RON
002090	04 F07005.		RON
002100	05 F0700501.		RON
002110	06 FILLER	PICTURE X(4).	RON
002120	06 F070050101	PICTURE X.	RON
002130	05 FILLER	PICTURE X.	RON
002140	04 F07006.		RON
002150	05 F0700601.		RON
002160	06 FILLER	PICTURE X(4).	RON
002170	06 F070060101	PICTURE X.	RON
002180	05 FILLER	PICTURE X.	RON

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F/G 1/2

A METHOD OF ANALYSIS FOR GENERAL AVIATION AIRPLANE STRUCTURAL C--ETC(U)

SEP 76 G WITTLIN, M A GAMON

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FAA-RD-76-123

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00219 C	002050	03 F071.				RON
00220 C	002060	04 F07101.				RON
00221 C	002070	05 F0710101.				RON
00222 C	002080	06 FILLER	PICTURE X.			RON
00223 C	002090	06 F071010101	PICTURE X.			RON
00224 C	002100	05 FILLER	PICTURE X.			RON
00225 C	002110	04 F07102.				RON
00226 C	002120	05 F0710201.				RON
00227 C	002130	06 FILLER	PICTURE X.			RON
00228 C	002140	06 F071020101	PICTURE X.			RON
00229 C	002150	05 FILLER	PICTURE X.			RON
00230 C	002160	03 F072.				RON
00231 C	002170	04 F07201.				RON
00232 C	002180	05 F0720101	PICTURE X.			RON
00233 C	002190	05 FILLER	PICTURE X.			RON
00234 C	002200	04 F07202.				RON
00235 C	002210	05 F0720201	PICTURE X.			RON
00236 C	002220	05 FILLER	PICTURE X.			RON
00237 C	002230	03 F073.				RON
00238 C	002240	04 F07301.				RON
00239 C	002250	05 F0730101	PICTURE X.			RON
00240 C	002260	05 FILLER	PICTURE X.			RON
00241 C	002270	04 F07302.				RON
00242 C	002280	05 F0730201	PICTURE X.			RON
00243 C	002290	05 FILLER	PICTURE X.			RON
00244 C	002300	03 F074.				RON
00245 C	002310	04 F07401.				RON
00246 C	002320	05 F0740101	PICTURE X.			RON
00247 C	002330	05 FILLER	PICTURE X.			RON
00248 C	002340	04 F07402.				RON
00249 C	002350	05 F0740201	PICTURE X.			RON
00250 C	002360	05 FILLER	PICTURE X.			RON
00251 C	002370	03 F075.				RON
00252 C	002380	04 F07501.				RON
00253 C	002390	05 F0750101	PICTURE X.			RON
00254 C	002400	05 FILLER	PICTURE X.			RON
00255 C	002410	04 F07502.				RON
00256 C	002420	05 F0750201	PICTURE X.			RON
00257 C	002430	05 FILLER	PICTURE X.			RON
00258 C	002440	03 F076.				RON
00259 C	002450	04 F07601.				RON
00260 C	002460	05 F0760101	PICTURE X.			RON
00261 C	002470	05 FILLER	PICTURE X.			RON
00262 C	002480	04 F07602.				RON
00263 C	002490	05 F0760201	PICTURE X.			RON
00264 C	002500	05 FILLER	PICTURE X.			RON
00265 C	002510	03 F077	PICTURE X.			RON
00266 C	002520					RON
00267 C	002530					RON
00268 C	002540	02 DUM1.				RON
00269 C	002550					RON
00270 C	002560	03 FILLER	PICTURE X(20).			RON
00271 C	002570					RON
00272 C	002580					RON
00273 C	002590	02 CAUSE-FACTOR.				RON
00274 C	002600					RON
00275 C	002610					RON
00276 C	002620	03 F078 OCCURS 17 TIMES.				RON
00277 C	002630	04 F07801	PICTURE XX.			RON
00278 C	002640	04 F07802	PICTURE X.			RON
00279 C	002650	04 F07803.				RON
00280 C	002660	05 F0780301	PICTURE X.			RON
00281 C	002670	05 F0780302	PICTURE X.			RON
00282 C	002680					RON
00283 C	002690	02 INJRY.				RON
00284 C	002700					RON
00285 C	002710					RON
00286 C	002720	03 F079	PICTURE X.			RON
00287 C	002730	03 F080A.				RON
00288 C	002740	04 F08001A OCCURS 3 TIMES.				RON
00289 C	002750	05 F0800101A OCCURS 6 TIMES	PICTURE XXX.			RON
00290 C	002760	04 FILLER	PICTURE X(7).			RON
00291 C	002770	03 F080B OCCURS 4 TIMES.				RON
		04 F08001B OCCURS 3 TIMES.				RON

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002780	05 F0800101B	OCCURS 6 TIMES	PICTURE XXX.	RON
002790	04 FILLER	PICTURE X(8).		RON
002800	03 F081.			RON
002810	04 F08101	OCCURS 6 TIMES	PICTURE XXX.	RON
002820	04 FILLER	PICTURE X(8).		RON
002830				RON
002840				RON
002850	02 RMRKS.			RON
002860				RON
002870	03 F082.			RON
002880	04 F08201	PICTURE X.		RON
002890	04 F08202	PICTURE X(49).		RON
002900	03 FILLER	PICTURE X(11).		RON
002910				RON
002920				RON
002930	02 CAUSE.			RON
002940				RON
002950	03 F083.			RON
002960	04 F08301	OCCURS 50 TIMES	PICTURE X.	RON
002970	03 FILLER	PICTURE X(11).		RON
002980				RON
002990	02 DUM2.			RON
003000				RON
003010	03 FILLER	PICTURE X(20).		RON
003020				RON
003030				RON
003040	02 E-P-DATA.			RON
003050				RON
003060	03 F084	PICTURE X.		RON
003070	03 F085	PICTURE X.		RON
003080	03 F086	PICTURE X.		RON
003090	03 F087	PICTURE X.		RON
003100	03 F088	PICTURE X.		RON
003110	03 F089	PICTURE X.		RON
003120				RON
003130				RON
003140	02 OVERHAUL.			RON
003150				RON
003160	03 F090.			RON
003170	04 FILLER	PICTURE X(4).		RON
003180	04 F09001	PICTURE X.		RON
003190	03 F091.			RON
003200	04 F09101	OCCURS 4 TIMES.		RON
003210	05 FILLER	PICTURE XXX.		RON
003220	05 F0910101	PICTURE X.		RON
003230	03 F092.			RON
003240	04 F09201	OCCURS 4 TIMES.		RON
003250	05 FILLER	PICTURE XXX.		RON
003260	05 F0920101	PICTURE X.		RON
003270	03 F093.			RON
003280	04 FILLER	PICTURE X(5).		RON
003290	04 F09301	PICTURE X.		RON
003300	03 F094.			RON
003310	04 F09401	PICTURE X.		RON
003320	04 FILLER	PICTURE X(11).		RON
003330	03 FILLER	PICTURE X.		RON
003340				RON
003350	02 WEATHER-SITE.			RON
003360				RON
003370	03 F095	PICTURE X.		RON
003380	03 F096.			RON
003390	04 FILLER	PICTURE X(4).		RON
003400	04 F09601	PICTURE X.		RON
003410	03 F097	PICTURE X.		RON
003420	03 F098.			RON
003430	04 F09801	PICTURE X.		RON
003440	04 F09802	PICTURE X.		RON
003450	03 F099	PICTURE X.		RON
003460	03 F100	PICTURE X.		RON
003470	03 F101	PICTURE XX.		RON
003480	03 F102	PICTURE X(4).		RON
003490				RON
003500				RON

00365 C	003510	03 F103.			RON
00366 C	003520	04 F10301	PICTURE X.		RON
00367 C	003530	04 F10302	PICTURE X.		RON
00368 C	003540	04 F10303	PICTURE X.		RON
00369 C	003550	03 F104	PICTURE XXX.		RON
00370 C	003560	03 F105	PICTURE XXX.		RON
00371 C	003570	03 F106.			RON
00372 C	003580	04 FILLER	PICTURE XX.		RON
00373 C	003590	04 F10601	PICTURE X.		RON
00374 C	003600				RON
00375 C	003610				RON
00376 C	003620	02 AAA.			RON
00377 C	003630				RON
00378 C	003640	03 F107	PICTURE X.		RON
00379 C	003650	03 F108	PICTURE X.		RON
00380 C	003660	03 F109	PICTURE X.		RON
00381 C	003670	03 F110	PICTURE X.		RON
00382 C	003680	03 F111	PICTURE X.		RON
00383 C	003690	03 F112	PICTURE X.		RON
00384 C	003700	03 F113	PICTURE X.		RON
00385 C	003710	03 F114	PICTURE X.		RON
00386 C	003720	03 F115	PICTURE X.		RON
00387 C	003730	03 F116	PICTURE X.		RON
00388 C	003740	03 F117	PICTURE X.		RON
00389 C	003750	03 F118	PICTURE X.		RON
00390 C	003760	03 F119	PICTURE X.		RON
00391 C	003770				RON
00392 C	003780				RON
00393 C	003790	02 DUM3.			RON
00394 C	003800				RON
00395 C	003810	03 FILLER	PICTURE X(20).		RON
00396 C	003820				RON
00397 C	003830				RON
00398 C	003840	02 FLIGHT-DATA.			RON
00399 C	003850				RON
00400 C	003860	03 F120.			RON
00401 C	003870	04 FILLER	PICTURE XXX.		RON
00402 C	003880	04 F12001	PICTURE X.		RON
00403 C	003890	03 F121.			RON
00404 C	003900	04 FILLER	PICTURE XXX.		RON
00405 C	003910	04 F12101	PICTURE X.		RON
00406 C	003920	03 F122	PICTURE XXX.		RON
00407 C	003930	03 F123	PICTURE XX.		RON
00408 C	003940	03 F124.			RON
00409 C	003950	04 FILLER	PICTURE XXX.		RON
00410 C	003960	04 F12401	PICTURE X.		RON
00411 C	003970	03 F125.			RON
00412 C	003980	04 F12501.			RON
00413 C	003990	05 FILLER	PICTURE X.		RON
00414 C	004000	05 F1250101	PICTURE X.		RON
00415 C	004010	04 F12502.			RON
00416 C	004020	05 FILLER	PICTURE XX.		RON
00417 C	004030	05 F1250201	PICTURE X.		RON
00418 C	004040	04 F12503.			RON
00419 C	004050	05 FILLER	PICTURE XX.		RON
00420 C	004060	05 F1250301	PICTURE X.		RON
00421 C	004070				RON
00422 C	004080	03 F126.			RON
00423 C	004090	04 FILLER	PICTURE X.		RON
00424 C	004100	04 F12601	PICTURE X.		RON
00425 C	004110	03 F127.			RON
00426 C	004120	04 FILLER	PICTURE X.		RON
00427 C	004130	04 F12701	PICTURE XX.		RON
00428 C	004140	03 F128			RON
00429 C	004150	03 F129.			RON
00430 C	004160	04 FILLER	PICTURE X(16).		RON
00431 C	004170	04 F12901	PICTURE X.		RON
00432 C	004180	03 F130.			RON
00433 C	004190	04 FILLER	PICTURE X(9).		RON
00434 C	004200	04 F13001	PICTURE X.		RON
00435 C	004210	03 FILLER	PICTURE X(4).		RON
00436 C	004220				RON
00437 C	004230	02 HUMAN-FACTORS.			RON

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00438 C 004240	03 F131.		RON
00439 C 004250	04 F13101	PICTURE X.	RON
00440 C 004260	04 F13102	PICTURE X.	RON
00441 C 004270	04 F13103	PICTURE X.	RON
00442 C 004280	04 F13104	PICTURE X.	RON
00443 C 004290	03 F132	PICTURE XX.	RON
00444 C 004300	03 F133.		RON
00445 C 004310	04 F13301	PICTURE X.	RON
00446 C 004320	04 F13302.		RON
00447 C 004330	05 FILLER	PICTURE X.	RON
00448 C 004340	05 F1330201	PICTURE X.	RON
00449 C 004350	03 F134	PICTURE X.	RON
00450 C 004360	03 F135	PICTURE X.	RON
00451 C 004370	03 F136.		RON
00452 C 004380	04 FILLER	PICTURE XXX.	RON
00453 C 004390	04 F13601	PICTURE X.	RON
00454 C 004400	03 F137.		RON
00455 C 004410	04 F13701	PICTURE X.	RON
00456 C 004420	04 F13702	PICTURE X.	RON
00457 C 004430	04 F13703	PICTURE X.	RON
00458 C 004440	04 F13704	PICTURE X.	RON
00459 C 004450	04 F13705	PICTURE X.	RON
00460 C 004460	03 F138		RON
00461 C 004470	03 F139.		RON
00462 C 004480	04 FILLER	PICTURE XX.	RON
00463 C 004490	04 F13901	PICTURE X.	RON
00464 C 004500	03 F140.		RON
00465 C 004510	04 FILLER	PICTURE XX.	RON
00466 C 004520	04 F14001	PICTURE X.	RON
00467 C 004530	03 F141.		RON
00468 C 004540	04 FILLER	PICTURE XX.	RON
00469 C 004550	04 F14101	PICTURE X.	RON
00470 C 004560	03 F142	PICTURE X.	RON
00471 C 004570	03 F143	PICTURE X.	RON
00472 C 004580	03 F144	PICTURE X.	RON
00473 C 004590	03 F145	PICTURE X.	RON
00474 C 004600	03 F146	PICTURE X.	RON
00475 C 004610	03 F147	PICTURE X.	RON
00476 C 004620	03 F148.		RON
00477 C 004630	04 F14801	PICTURE X.	RON
00478 C 004640	04 F14802	PICTURE X.	RON
00479 C 004650	04 F14803	PICTURE X.	RON
00480 C 004660	04 F14804	PICTURE X.	RON
00481 C 004670	03 F149.		RON
00482 C 004680	04 F14901.		RON
00483 C 004690	05 FILLER	PICTURE XX.	RON
00484 C 004700	05 F1490101	PICTURE X.	RON
00485 C 004710	04 F14902.		RON
00486 C 004720	05 FILLER	PICTURE XX.	RON
00487 C 004730	05 F1490201	PICTURE X.	RON
00488 C 004740	03 F150		RON
00489 C 004750	03 F151.		RON
00490 C 004760	04 F15101	PICTURE X.	RON
00491 C 004770	04 F15102	PICTURE X.	RON
00492 C 004780	04 F15103	PICTURE X.	RON
00493 C 004790	03 F152.		RON
00494 C 004800	04 FILLER	PICTURE XX.	RON
00495 C 004810	04 F15201	PICTURE X.	RON
00496 C 004820	03 F153	PICTURE X.	RON
00497 C 004830	03 FILLER	PICTURE X(7).	RON
00498 C 004840			RON
00499 C 004850			RON
00500 C 004860			RON
00501 C 004870	02 FIRE-INFO.		RON
00502 C 004880			RON
00503 C 004890	03 F154	PICTURE X.	RON
00504 C 004900	03 F155	PICTURE X.	RON
00505 C 004910	03 F156	PICTURE X.	RON
00506 C 004920	03 F157	PICTURE X.	RON
00507 C 004930	03 F158.		RON
00508 C 004940	04 F15801	PICTURE X.	RON
00509 C 004950	04 F15802.		RON
00510 C 004960	05 F1580201	PICTURE X.	RON

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00511 C	004970	05 F1580202	PICTURE X.	RON
00512 C	004980	04 F15803.		RON
00513 C	004990	05 F1580301	PICTURE X.	RON
00514 C	005000	05 F1580302	PICTURE X.	RON
00515 C	005010	03 F159	PICTURE X.	RON
00516 C	005020	03 F160	PICTURE X.	RON
00517 C	005030	03 F161.		RON
00518 C	005040	04 F16101	PICTURE X.	RON
00519 C	005050	04 F16102	PICTURE X.	RON
00520 C	005060			RON
00521 C	005070			RON
00522 C	005080	02 EQUIP.		RON
00523 C	005090			RON
00524 C	005100	03 F162	PICTURE X.	RON
00525 C	005110	03 F163	PICTURE X.	RON
00526 C	005120	03 F164.		RON
00527 C	005130	04 F16401	PICTURE X.	RON
00528 C	005140	04 F16402	PICTURE X.	RON
00529 C	005150	03 F165	PICTURE X.	RON
00530 C	005160	03 F166	PICTURE X.	RON
00531 C	005170			RON
00532 C	005180			RON
00533 C	005190	02 W-B-DAMAGE.		RON
00534 C	005200			RON
00535 C	005210	03 F167	PICTURE X.	RON
00536 C	005220	03 F168	PICTURE X.	RON
00537 C	005230	03 F169	PICTURE X.	RON
00538 C	005240	03 F170	PICTURE X.	RON
00539 C	005250	03 F171	PICTURE X.	RON
00540 C	005260	03 F172	PICTURE X.	RON
00541 C	005270	03 F173	PICTURE X.	RON
00542 C	005280	03 F174.		RON
00543 C	005290	04 F17401	PICTURE X.	RON
00544 C	005300	04 F17402	PICTURE X.	RON
00545 C	005310	03 F175	PICTURE X.	RON
00546 C	005320	03 F176	PICTURE X.	RON
00547 C	005330	03 F177.		RON
00548 C	005340	04 F17701	PICTURE X.	RON
00549 C	005350	04 F17702	PICTURE X.	RON
00550 C	005360	03 F178	PICTURE X.	RON
00551 C	005370	03 F179	PICTURE X.	RON
00552 C	005380	03 F180	PICTURE X.	RON
00553 C	005390	03 F181	PICTURE X.	RON
00554 C	005400	03 F182	PICTURE X.	RON
00555 C	005410	03 F183	PICTURE X.	RON
00556 C	005420			RON
00557 C	005430			RON
00558 C	005440	02 DUM4.		RON
00559 C	005450			RON
00560 C	005460	03 FILLER	PICTURE X(23).	RON
00561 C	005470	03 FILLER	PICTURE X(20).	RON
00562 C	005480			RON
00563 C	005490			RON
00564 C	005500	02 ADMIN-DATA.		RON
00565 C	005510			RON
00566 C	005520	03 FILLER	PICTURE XXX.	RON
00567 C	005530	03 F184	PICTURE X(12).	RON
00568 C	005540	03 F185	PICTURE X(6).	RON
00569 C	005550	03 F186 OCCURS 3 TIMES.		RON
00570 C	005560	04 F18601	PICTURE 99.	RON
00571 C	005570	04 F18602	PICTURE XX.	RON
00572 C	005580	04 F18603	PICTURE XX.	RON
00573 C	005590	03 F187	PICTURE 99.	RON
00574 C	005600	03 F188	PICTURE XXX.	RON
00575 C	005610	03 F189	PICTURE X(13).	RON
00576 C	005620			RON
00577 C	005630			RON
00578 C	005640	02 IDN.		RON
00579 C	005650			RON
00580 C	005660	03 F190	PICTURE X(4).	RON
00581 C	005670			RON
00582 C	005680			RON
00583 C	005690	02 DUM5.		RON

00584 C	005700	03 FILLER	PICTURE X(20).	RON
00585 C	005710			RON
00586 C	005720			RON
00587 C	005730			RON
00588 C	005740	02 AERIAL-APP.		RON
00589 C	005750			RON
00590 C	005760	03 F191.		RON
00591 C	005770	04 FILLER	PICTURE XXX.	RON
00592 C	005780	04 F19101	PICTURE X.	RON
00593 C	005790	03 F192	PICTURE X.	RON
00594 C	005800	03 F193	PICTURE X.	RON
00595 C	005810	03 F194	PICTURE X.	RON
00596 C	005820	03 F195	PICTURE X.	RON
00597 C	005830	03 F196	PICTURE X.	RON
00598 C	005840	03 F197	PICTURE X.	RON
00599 C	005850	03 F198	PICTURE X.	RON
00600 C	005860	03 F199	PICTURE X.	RON
00601 C	005870	03 F200	PICTURE X.	RON
00602 C	005880	03 F201	PICTURE X.	RON
00603 C	005890	03 F202	PICTURE X.	RON
00604 C	005900	03 F203	PICTURE X.	RON
00605 C	005910	03 F204	PICTURE X.	RON
00606 C	005920	03 F205	PICTURE X.	RON
00607 C	005930	03 F206	PICTURE X.	RON
00608 C	005940	03 F207	PICTURE X.	RON
00609 C	005950	03 F208	PICTURE X(5).	RON
00610 C	005960	03 F209.		RON
00611 C	005970	04 F20901	PICTURE X.	RON
00612 C	005980	04 F20902	PICTURE X.	RON
00613 C	005990	04 F20903	PICTURE X.	RON
00614 C	006000	03 F210.		RON
00615 C	006010	04 F21001	PICTURE X.	RON
00616 C	006020	04 F21002	PICTURE X.	RON
00617 C	006030	04 F21003	PICTURE X.	RON
00618 C	006040	03 F211	PICTURE X.	RON
00619 C	006050	03 F212	PICTURE X.	RON
00620 C	006060			RON
00621 C	006070			RON
00622 C	006080	02 DUM6.		RON
00623 C	006090			RON
00624 C	006100	03 FILLER	PICTURE X(28).	RON
00625 C	006110	03 FILLER	PICTURE X(20).	RON
00626 C	006120			RON
00627 C	006130			RON
00628 C	006140	02 COL.		RON
00629 C	006150			RON
00630 C	006160	03 F213	PICTURE X.	RON
00631 C	006170	03 F214	PICTURE X.	RON
00632 C	006180	03 F215	PICTURE X.	RON
00633 C	006190	03 F216	PICTURE X.	RON
00634 C	006200	03 F217	PICTURE X.	RON
00635 C	006210	03 F218	PICTURE X.	RON
00636 C	006220	03 F219	PICTURE X.	RON
00637 C	006230	03 F220	PICTURE XXX.	RON
00638 C	006240	03 F221	PICTURE XXX.	RON
00639 C	006250	03 F222.		RON
00640 C	006260	04 F22201	PICTURE XXX.	RON
00641 C	006270	04 F22202	PICTURE XXX.	RON
00642 C	006280	03 F223	PICTURE X.	RON
00643 C	006290	03 F224	PICTURE X.	RON
00644 C	006300	03 F225	PICTURE X.	RON
00645 C	006310	03 F226	PICTURE X.	RON
00646 C	006320	03 F227	PICTURE X.	RON
00647 C	006330			RON
00648 C	006340			RON
00649 C	006350	02 DUM7.		RON
00650 C	006360			RON
00651 C	006370	03 FILLER	PICTURE X(37).	RON
00652 C	006380			RON
00653 C	006390			RON
00654 C	006400	02 DITCH-SURVIVAL.		RON
00655 C	006410			RON
00656 C	006420	03 F228	PICTURE X.	RON

00657	C	006430	03 F229	PICTURE XX.	RON
00658	C	006440	03 F230		RON
00659	C	006450	04 F23001	PICTURE XX.	RON
00660	C	006460	04 F23002	PICTURE XXX.	RON
00661	C	006470	03 F231	PICTURE X.	RON
00662	C	006480	03 F232	PICTURE X.	RON
00663	C	006490	03 FILLER	PICTURE X.	RON
00664	C	006500	03 F233	PICTURE X.	RON
00665	C	006510	03 F234	PICTURE X.	RON
00666	C	006520	03 F235	PICTURE X.	RUN
00667	C	006530	03 F236	PICTURE X.	RUN
00668	C	006540	03 F237	PICTURE X.	RUN
00669	C	006550	03 F238	PICTURE X.	RUN
00670	C	006560	03 F239	PICTURE X.	RUN
00671	C	006570	02 DUMB		RUN
00672	C	006580	03 FILLER	PICTURE X(127).	RUN
00673	C	004100	WORKING-STORAGE SECTION.		
00674	C	004200	ADD-TOT-AC	PIC X.	
00675	C	004300	ANGLE-SUM	PIC 9(7) VALUE ZERO.	
00676	C	004400	ANGLE-15	PIC 9(5) VALUE ZERO.	
00677	C	004500	ANGLE-30	PIC 9(5) VALUE ZERO.	
00678	C	004600	ANGLE-45	PIC 9(5) VALUE ZERO.	
00679	C	004700	ANGLE-60	PIC 9(5) VALUE ZERO.	
00680	C	004800	ANGLE-75	PIC 9(5) VALUE ZERO.	
00681	C	004900	ANGLE-90	PIC 9(5) VALUE ZERO.	
00682	C	005000	ANGLE-90-PLUS	PIC 9(5) VALUE ZERO.	
00683	C	005100	AV-OCC	PIC 9(5) VALUE ZERO.	
00684	C	005200	AVG-ANGLE	PIC 9999 VALUE ZERO.	
00685	C	005300	AVG-DIST	PIC 9999 VALUE ZERO.	
00686	C	005400	AVG-VEL	PIC 9999 VALUE ZERO.	
00687	C	005500	BEEN-THERE	PIC X.	
00688	C	005600	C-HI	PIC 9(3).	
00689	C	005700	C-INITIAL	PIC 9(3).	
00690	C	005800	C-SAVE	PIC 9(3) VALUE ZERO.	
00691	C	005900	C-SV	PIC 9 VALUE 1.	
00692	C	006000	C-SV-LIMIT	PIC 9.	
00693	C	006100	C-TEST	PIC 9 VALUE 1.	
00694	C	006200	CAUSE-FACTOR-77	PIC 9(4).	
00695	C	006300	CAUSE-77	PIC 9(5) VALUE ZERO.	
00696	C	006400	CFF	PIC 99.	
00697	C	006500	D	PIC 99 VALUE 01.	
00698	C	006600	DIST-SUM	PIC 9(6) VALUE ZERO.	
00699	C	006700	DIST-10	PIC 9(5) VALUE ZERO.	
00700	C	006800	DIST-20	PIC 9(5) VALUE ZERO.	
00701	C	006900	DIST-30	PIC 9(5) VALUE ZERO.	
00702	C	007000	DIST-40	PIC 9(5) VALUE ZERO.	
00703	C	007100	DIST-50	PIC 9(5) VALUE ZERO.	
00704	C	007200	DIST-60	PIC 9(5) VALUE ZERO.	
00705	C	007300	DIST-60-PLUS	PIC 9(5) VALUE ZERO.	
00706	C	007400	DIVIDE-HOLD	PIC 9(4) USAGE COMP SYNC VALUE 0.	
00707	C	007500	DIVIDEND-HOLD	PIC 9(5) USAGE COMP SYNC VALUE 0.	
00708	C	007600	DUMBO	PIC X.	
00709	C	007700	ERR	PIC X(20):	
00710	C	007800	ERR-RT	PIC X(20):	
00711	C	007900	F	PIC 9(3) VALUE ZERO.	
00712	C	008000	FACTOR-SAVE	PIC XX.	
00713	C	008100	FACTOR-77	PIC XX.	
00714	C	008200	FAT-INFLT	PIC 9(5) VALUE ZERO.	
00715	C	008300	FAT-LDG	PIC 9(5) VALUE ZERO.	
00716	C	008400	FAT-NR	PIC 9(5) VALUE ZERO.	
00717	C	008500	FAT-TO	PIC 9(5) VALUE ZERO.	
00718	C	008600	FAT-TS	PIC 9(5) VALUE ZERO.	
00719	C	008700	FDATA	PIC X(68).	
00720	C	008800	FOUND-WORD	PIC X VALUE 0.	
00721	C	008900	G-ANG-SUM	PIC 9(6) VALUE ZERO.	
00722	C	009000	G-ANG-15	PIC 9(5) VALUE ZERO.	
00723	C	009100	G-ANG-30	PIC 9(5) VALUE ZERO.	
00724	C	009200	G-ANG-45	PIC 9(5) VALUE ZERO.	
00725	C	009300	G-ANG-60	PIC 9(5) VALUE ZERO.	
00726	C	009400	G-ANG-75	PIC 9(5) VALUE ZERO.	
00727	C	009500	G-ANG-90	PIC 9(5) VALUE ZERO.	
00728	C	009600	G-ANG-90-PLUS	PIC 9(5) VALUE ZERO.	
00729	C	009700	G-AVG-ANGLE	PIC 9999 VALUE ZERO.	

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00730	007300	77	G-AVG-DIST	PIC 9999 VALUE ZERO.
00731	007300	77	G-AVG-VEL	PIC 9999 VALUE ZERO.
00732	010000	77	G-DIST-SUM	PIC 9(6) VALUE ZERO.
00733	010100	77	G-DIST-10	PIC 9(5) VALUE ZERO.
00734	010200	77	G-DIST-20	PIC 9(5) VALUE ZERO.
00735	010300	77	G-DIST-30	PIC 9(5) VALUE ZERO.
00736	010400	77	G-DIST-40	PIC 9(5) VALUE ZERO.
00737	010500	77	G-DIST-50	PIC 9(5) VALUE ZERO.
00738	010600	77	G-DIST-60	PIC 9(5) VALUE ZERO.
00739	010700	77	G-DIST-60-PLUS	PIC 9(5) VALUE ZERO.
00740	010800	77	G-VEL-SUM	PIC 9(6) VALUE ZERO.
00741	010900	77	G-VEL-120	PIC 9(5) VALUE ZERO.
00742	011000	77	G-VEL-120-PLUS	PIC 9(5) VALUE ZERO.
00743	011100	77	G-VEL-30	PIC 9(5) VALUE ZERO.
00744	011200	77	G-VEL-60	PIC 9(5) VALUE ZERO.
00745	011300	77	G-VEL-90	PIC 9(5) VALUE ZERO.
00746	011400	77	GAVG-DCC	PIC 9(5) VALUE ZERO.
00747	011500	77	GFAT-INFLT	PIC 9(5) VALUE ZERO.
00748	011600	77	GFAT-LDG	PIC 9(5) VALUE ZERO.
00749	011700	77	GFAT-NR	PIC 9(5) VALUE ZERO.
00750	011800	77	GFAT-TQ	PIC 9(5) VALUE ZERO.
00751	011900	77	GFAT-TS	PIC 9(5) VALUE ZERO.
00752	012000	77	GHEL-UNUSED	PIC 9(5) VALUE ZERO.
00753	012100	77	GHEL-USED	PIC 9(5) VALUE ZERO.
00754	012200	77	GS-H-FAILED	PIC 9(5) VALUE ZERO.
00755	012300	77	GS-H-INST	PIC 9(5) VALUE ZERO.
00756	012400	77	GS-H-USED	PIC 9(5) VALUE ZERO.
00757	012500	77	GTOT-AC	PIC 9(5) VALUE ZERO.
00758	012600	77	GTOT-AC-TYPE	PIC 9(5) VALUE ZERO.
00759	012700	77	GTOT-ACC-ANG	PIC 9(5) VALUE ZERO.
00760	012800	77	GTOT-ACC-DIST	PIC 9(5) VALUE ZERO.
00761	012900	77	GTOT-ACC-VEL	PIC 9(5) VALUE ZERO.
00762	013000	77	GTOT-FAT	PIC 9(5) VALUE ZERO.
00763	013100	77	GTOT-FLY	PIC 9(5) VALUE ZERO.
00764	013200	77	GTOT-LDG	PIC 9(5) VALUE ZERO.
00765	013300	77	GTOT-MNR	PIC 9(5) VALUE ZERO.
00766	013400	77	GTOT-NON	PIC 9(5) VALUE ZERO.
00767	013500	77	GTOT-NR	PIC 9(5) VALUE ZERO.
00768	013600	77	GTOT-OCC	PIC 9(5) VALUE ZERO.
00769	013700	77	GTOT-SER	PIC 9(5) VALUE ZERO.
00770	013800	77	GTOT-ST-ACC	PIC 9(5) VALUE ZERO.
00771	013900	77	GTOT-ST-FAIL	PIC 9(5) VALUE ZERO.
00772	014000	77	GTOT-STBLT-ACC	PIC 9(5) VALUE ZERO.
00773	014100	77	GTOT-STBLT-FAIL	PIC 9(5) VALUE ZERO.
00774	014200	77	GTOT-T-U	PIC 9(5) VALUE ZERO.
00775	014300	77	GTOT-TS	PIC 9(5) VALUE ZERO.
00776	014400	77	HD	PIC X(20).
00777	014500	77	HEAD-COUNT	PIC 9(5) VALUE 0.
00778	014600	77	HELMET-UNUSED	PIC 9(5) VALUE ZERO.
00779	014700	77	HELMET-USED	PIC 9(5) VALUE ZERO.
00780	014800	77	HI	PIC 999 VALUE ZERO.
00781	014900	77	HISAVE	PIC 999.
00782	015000	77	HOLD-MAKE	PIC X(3) VALUE LOW-VALUE.
00783	015100	77	HOLD-MAKE-NAME	PIC X(11).
00784	015200	77	HOLD-MODEL	PIC XX VALUE LOW-VALUE.
00785	015300	77	HOLD-YEAR	PIC XX VALUE LOW-VALUE.
00786	015400	77	I	PIC 999 VALUE ZERO.
00787	015500	77	INDEX-HOLD	PIC 9(5) VALUE ZERO.
00788	015600	77	INJ1	PIC 99 VALUE 1.
00789	015700	77	INJ2	PIC 99.
00790	015800	77	ITER-4	PIC 9(5) VALUE ZERO.
00791	015900	77	J	PIC 99 VALUE ZERO.
00792	016000	77	LO	PIC 999 VALUE ZERO.
00793	016100	77	NTSBXY1	PIC 9(3).
00794	016200	77	NTSBXY2	PIC 9(3).
00795	016300	77	NTSBXY3	PIC 9(3).
00796	016400	77	NTSBXY4	PIC 9(3).
00797	016500	77	NTSB9	PIC 9.
00798	016600	77	OP	PIC 99 VALUE ZERO.
00799	016700	77	OP-PH-HOLD	PIC 9(5).
00800	016800	77	PCNTT	PIC 99999.
00801	016900	77	PCT-HOLD	PIC X(5).
00802	017000	77	PERCENT	PIC X(8) VALUE ' % '.

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00803 017100 77 PRINT-ID PIC X.
00804 017200 77 READER-SWITCH PIC X.
00805 017300 77 REC-TOT-OCC PIC 9(3) VALUE ZERO.
00806 017400 77 REPLY-77 PIC X(4) VALUE SPACES.
00807 017500 77 S-H-FAILED PIC 9(5) VALUE ZERO.
00808 017600 77 S-H-INSTALLED PIC 9(5) VALUE ZERO.
00809 017700 77 S-H-USED PIC 9(5) VALUE ZERO.
00810 017800 77 S-SUB PIC 9 VALUE ZERO.
00811 017900 77 SAV-CARD PIC X(9) VALUE SPACES.
00812 018000 77 SEARCH-CODE PIC XX.
00813 018100 77 SEARCH-TYPE PIC X.
00814 018200 77 SEARCH-WORD PIC X(5).
00815 018300 77 SER-IND PIC 99.
00816 018400 77 SER-SUB PIC 9 VALUE 1.
00817 018500 77 SEV-IND PIC 99.
00818 018600 77 SEVERITY-77 PIC X(5) VALUE 'ABCDE'.
00819 018700 77 SPACE-LINE PIC X(132) VALUE SPACES.
00820 018800 77 SS PIC 99.
00821 018900 77 SSS PIC 99.
00822 019000 77 SUM-A PIC 9(18) USAGE COMP SYNC VALUE 0.
00823 019100 77 SUMMARY-COUNTER PIC 9(6) VALUE ZERO.
00824 019200 77 SUMMARY-HEAD-1 PIC X(89) VALUE '***** ACCIDENT SUMMARY *****'.
00825 019300 77 SUMMARY-HEAD-2 PIC X(69) VALUE 'FOR'.
00826 019400 77 TER-IND PIC 99.
00827 019500 77 TERRAIN-77 PIC X(13) VALUE 'ABCDEFGHIJKYZ'.
00828 019600 77 TOT-AC PIC 9(5) VALUE ZERO.
00829 019700 77 TOT-AC-TYPE PIC 9(5) VALUE ZERO.
00830 019800 77 TOT-ACC-ANG PIC 9(5) VALUE ZERO.
00831 019900 77 TOT-ACC-VEL PIC 9(5) VALUE ZERO.
00832 020000 77 TOT-ACC-DIST PIC 9(5) VALUE ZERO.
00833 020100 77 TOT-FAT PIC 9(5) VALUE ZERO.
00834 020200 77 TOT-FLY PIC 9(5) VALUE ZERO.
00835 020300 77 TOT-LDG PIC 9(5) VALUE ZERO.
00836 020400 77 TOT-MNR PIC 9(5) VALUE ZERO.
00837 020500 77 TOT-NON PIC 9(5) VALUE ZERO.
00838 020600 77 TOT-NR PIC 9(5) VALUE ZERO.
00839 020700 77 TOT-OCC PIC 9(5) VALUE ZERO.
00840 020800 77 TOT-SER PIC 9(5) VALUE ZERO.
00841 020900 77 TOT-ST-ACC PIC 9(5) VALUE ZERO.
00842 021000 77 TOT-ST-FAIL PIC 9(5) VALUE ZERO.
00843 021100 77 TOT-STBLT-ACC PIC 9(5) VALUE ZERO.
00844 021200 77 TOT-STBLT-FAIL PIC 9(5) VALUE ZERO.
00845 021300 77 TOT-T-U PIC 9(5) VALUE ZERO.
00846 021400 77 TOT-TS PIC 9(5) VALUE ZERO.
00847 021500 77 TYP-HOLD PIC 9(5) VALUE ZERO.
00848 021600 77 TYPES-77 PIC X(12) VALUE 'DEFLPRO12457'.
00849 021700 77 VEL-SUM PIC 9(6) VALUE ZERO.
00850 021800 77 VEL-120 PIC 9(5) VALUE ZERO.
00851 021900 77 VEL-120-PLUS PIC 9(5) VALUE ZERO.
00852 022000 77 VEL-30 PIC 9(5) VALUE ZERO.
00853 022100 77 VEL-60 PIC 9(5) VALUE ZERO.
00854 022200 77 VEL-90 PIC 9(5) VALUE ZERO.
00855 022300 77 PCNT-OCC PIC 999V99.
00856 022400 77 HOLD-KEY. PIC XX.
00857 022500 01 HOLD-KEY-1 PIC XX.
00858 022600 01 HOLD-KEY-2 PIC XX.
00859 022700 01 P-WORK.
00860 022800 02 P-WORK-02A.
00861 022900 03 FILLER PIC X(10) VALUE SPACES.
00862 023000 03 DESCRIPTION PIC X(48).
00863 023100 03 FILLER PIC X(3) VALUE SPACES.
00864 023200 03 DATA PIC X(68).
00865 023300 03 FILLER PIC X(6) VALUE SPACES.
00866 023400 02 P-WORK-02C REDEFINES P-WORK-02A.
00867 023500 03 FILLER PIC X.
00868 023600 03 P-WORK-02B PIC X(131).
00869 023700 01 TERRAIN-001.
00870 023800 02 TERRAIN-COUNT OCCURS 13 TIMES PIC 9(4).
00871 023900 01 HD-KEY-ACT.
00872 024000 02 HD-KEY.
00873 024100
00874 024200
00875 024300

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00874 024400 03 CCC.
00877 024500 04 CC PIC X(4).
00878 024600 04 C PIC XX.
00879 024700 03 FILL PIC XX.
00880 024800 03 CODE4.
00881 024900 04 CHAR4 PIC X.
00882 025000 04 CODE3.
00883 025100 05 CHAR3 PIC X.
00884 025200 05 CODE2.
00885 025300 06 CHAR2 PIC X.
00886 025400 06 CHAR1 PIC X.
00887 025500 02 HD-KEY-TWO REDEFINES HD-KEY.
00888 025600 10 KYA PIC 9(10) USAGE COMP.
00889 025700 10 KYB PIC 9(6) USAGE COMP.
00890 025800 01 DATE-HOLD-01A.
00891 025900 02 MO PIC XX.
00892 026000 02 DA PIC XX.
00893 026100 02 YR PIC XX.
00894 026200 01 DATE-HOLD-01B.
00895 026300 02 MO-B PIC XX.
00896 026400 02 FILLER PIC X VALUE '/'.
00897 026500 02 DA-B PIC XX.
00898 026600 02 FILLER PIC X VALUE '/'.
00899 026700 02 YR-B PIC XX.
00900 026800 01 TYPES-01.
00901 026900 02 TYPES-02 PIC X(12).
00902 027000 02 TYYP REDEFINES TYPES-02 OCCURS 12 TIMES PIC X.
00903 027100 01 SERIOUSNESS.
00904 027200 02 SER OCCURS 5 TIMES INDEXED BY S-INDEX.
00905 027300 03 S OCCURS 4 TIMES INDEXED BY SERIOUS-INDEX PIC 9(5).
00906 027400 01 ATT-WORK.
00907 027500 02 ATT-02 PIC X(20).
00908 027600 02 FILLER PIC X(48).
00909 027700 01 ATTITUDE.
00910 027800 02 ATTITUDE-1 PIC X(20).
00911 027900 02 FILLER PIC XX VALUE ', '.
00912 028000 02 ATTITUDE-2 PIC X(20).
00913 028100 02 FILLER PIC XX VALUE ', '.
00914 028200 02 ATTITUDE-3 PIC X(20).
00915 028300 01 DESCRIPTION-01.
00916 028400 02 DESCRIPTION-02.
00917 028500 03 FILLER PIC X(48) VALUE
00918 028600 03 'DATE' PIC X(48) VALUE . . . . .
00919 028700 03 'AIRCRAFT MAKE' PIC X(48) VALUE . . . . .
00920 028800 03 FILLER PIC X(48) VALUE . . . . .
00921 028900 03 'AIRCRAFT MODEL' PIC X(48) VALUE . . . . .
00922 029000 03 FILLER PIC X(48) VALUE . . . . .
00923 029100 03 'AIRCRAFT DAMAGE' PIC X(48) VALUE . . . . .
00924 029200 03 FILLER PIC X(48) VALUE . . . . .
00925 029300 03 'FIRE AFTER IMPACT' PIC X(48) VALUE . . . . .
00926 029400 03 FILLER PIC X(48) VALUE . . . . .
00927 029500 03 'KIND OF FLYING (GENERAL AVIATION)' PIC X(48) VALUE . . . . .
00928 029600 03 FILLER PIC X(48) VALUE . . . . .
00929 029700 03 'TYPE OF ACCIDENT, FIRST' PIC X(48) VALUE . . . . .
00930 029800 03 FILLER PIC X(48) VALUE . . . . .
00931 029900 03 'PHASE OF OPERATION, FIRST' PIC X(48) VALUE . . . . .
00932 030000 03 FILLER PIC X(48) VALUE . . . . .
00933 030100 03 'TYPE OF ACCIDENT, SECOND' PIC X(48) VALUE . . . . .
00934 030200 03 FILLER PIC X(48) VALUE . . . . .
00935 030300 03 'PHASE OF OPERATION, SECOND' PIC X(48) VALUE . . . . .
00936 030400 03 FILLER PIC X(48) VALUE . . . . .
00937 030500 03 'AIRCRAFT SPEED' PIC X(48) VALUE . . . . .
00938 030600 03 FILLER PIC X(48) VALUE . . . . .
00939 030700 03 'AIRPORT PROXIMITY' PIC X(48) VALUE . . . . .
00940 030800 03 FILLER PIC X(48) VALUE . . . . .
00941 030900 03 'RUNWAY COMPOSITION' PIC X(48) VALUE . . . . .
00942 031000 03 FILLER PIC X(48) VALUE . . . . .
00943 031100 03 'RUNWAY SURFACE' PIC X(48) VALUE . . . . .
00944 031200 03 FILLER PIC X(48) VALUE . . . . .
00945 031300 03 'RUNWAY HAZARDS' PIC X(48) VALUE . . . . .
00946 031400 03 FILLER PIC X(48) VALUE . . . . .
00947 031500 03 'RUNWAY LENGTH' PIC X(48) VALUE . . . . .
00948 031600
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00949	031700	03	FILLER PIC X(48)	VALUE	
00950	031800		TERRAIN (TYPE) OF	AIRPORT	..
00951	031900	03	FILLER PIC X(48)	VALUE	
00952	032000		CAUSE / FACTOR		..
00953	032100	03	FILLER PIC X(48)	VALUE	
00954	032200		CAUSE / FACTOR		..
00955	032300	03	FILLER PIC X(48)	VALUE	
00956	032400		CAUSE / FACTOR		..
00957	032500	03	FILLER PIC X(48)	VALUE	
00958	032600		CAUSE / FACTOR		..
00959	032700	03	FILLER PIC X(48)	VALUE	
00960	032800		CAUSE / FACTOR		..
00961	032900	03	FILLER PIC X(48)	VALUE	
00962	033000		CAUSE / FACTOR		..
00963	033100	03	FILLER PIC X(48)	VALUE	
00964	033200		CAUSE / FACTOR		..
00965	033300	03	FILLER PIC X(48)	VALUE	
00966	033400		CAUSE / FACTOR		..
00967	033500	03	FILLER PIC X(48)	VALUE	
00968	033600		CAUSE / FACTOR		..
00969	033700	03	FILLER PIC X(48)	VALUE	
00970	033800		CAUSE / FACTOR		..
00971	033900	03	FILLER PIC X(48)	VALUE	
00972	034000		PILOT		..
00973	034100	03	FILLER PIC X(48)	VALUE	
00974	034200		COPILOT		..
00975	034300	03	FILLER PIC X(48)	VALUE	
00976	034400		DUAL PILOT		..
00977	034500	03	FILLER PIC X(48)	VALUE	
00978	034600		CHECK PILOT		..
00979	034700	03	FILLER PIC X(48)	VALUE	
00980	034800		PASSENGERS		..
00981	034900	03	FILLER PIC X(48)	VALUE	
00982	035000		TOTAL ABOARD		..
00983	035100	03	FILLER PIC X(48)	VALUE	
00984	035200		REMARKS		..
00985	035300	03	FILLER PIC X(48)	VALUE	
00986	035400				..
00987	035500	03	FILLER PIC X(48)	VALUE	
00988	035600		AIRCRAFT SERIAL NUMBER		..
00989	035700	03	FILLER PIC X(48)	VALUE	
00990	035800		IMPACT SEVERITY		..
00991	035900	03	FILLER PIC X(48)	VALUE	
00992	036000		IMPACT ANGLE		..
00993	036100	03	FILLER PIC X(48)	VALUE	
00994	036200		RATE OF DECELERATION		..
00995	036300	03	FILLER PIC X(48)	VALUE	
00996	036400		DIRECTION OF PRINCIPLE DECELERATION		..
00997	036500	03	FILLER PIC X(48)	VALUE	
00998	036600		STOPPING DISTANCE		..
00999	036700	03	FILLER PIC X(48)	VALUE	
01000	036800		DAMAGE SEVERITY - IMPACT (NON-TRANS. AIRCRAFT)		..
01001	036900	03	FILLER PIC X(48)	VALUE	
01002	037000		SEATING CONFIGURATION		..
01003	037100	03	FILLER PIC X(48)	VALUE	
01004	037200		SEAT FAILURES - NUMERICAL SUMMARY		..
01005	037300	03	FILLER PIC X(48)	VALUE	
01006	037400		SEAT BELT FAILURES - NUMERICAL SUMMARY		..
01007	037500	03	FILLER PIC X(48)	VALUE	
01008	037600		DEATH RESULTING FROM FIRE AFTER IMPACT		..
01009	037700	03	FILLER PIC X(48)	VALUE	
01010	037800		ATTITUDE AT IMPACT - ROLL		..
01011	037900	03	FILLER PIC X(48)	VALUE	
01012	038000		ATTITUDE AT IMPACT - PITCH		..
01013	038100	03	FILLER PIC X(48)	VALUE	
01014	038200		ATTITUDE AT IMPACT - YAW		..
01015	038300	03	FILLER PIC X(48)	VALUE	
01016	038400		SPEED AT IMPACT - KNOTS		..
01017	038500	03	FILLER PIC X(48)	VALUE	
01018	038600		KIND OF OPERATION		..
01019	038700	03	FILLER PIC X(48)	VALUE	
01020	038800		SHOULDER HARNESS		..
01021	038900	03	FILLER PIC X(48)	VALUE	

01022 039000 03 'SEAT BELT' FILLER PIC X(48) VALUE
01023 039100 03 'CRASH HELMET' FILLER PIC X(48) VALUE
01024 039200 03 'CRASH BAR' FILLER PIC X(48) VALUE
01025 039300 03 'COCKPIT CRASH PAD' FILLER PIC X(48) VALUE
01026 039400 03 'CRASH BAR' FILLER PIC X(48) VALUE
01027 039500 03 'OBSTRUCTIONS' FILLER PIC X(48) VALUE
01028 039600 03 'TERRAIN TYPE' FILLER PIC X(48) VALUE
01029 039700 02 DESC REDEFINES DESCRIPTION-02 OCCURS 70 TIMES PIC X(48).
01030 039800 01 ACT-KEY.
01031 039900 05 TRACK-ID PIC S9(8) USAGE COMP SYNC VALUE 0.
01032 040000 05 SYMBOLIC-KEY.
01033 040100 10 KYF PIC X(6).
01034 040200 10 FILLER PIC XX VALUE SPACES.
01035 040300 10 KYG PIC X(4).
01036 040400 01 TERRAIN-01.
01037 040500 02 TERRAIN-02 PIC X(13).
01038 040600 02 TERRAIN REDEFINES TERRAIN-02 OCCURS 13 TIMES
01039 040700 02 INDEXED BY TERRAIN-INDEX PIC X.
01040 040800 01 SEVERITY.
01041 040900 02 SEVERITY-02 PIC X(5).
01042 041000 02 SEV REDEFINES SEVERITY-02 OCCURS 5 TIMES
01043 041100 02 INDEXED BY SEVERITY-INDEX PIC X.
01044 041200 01 NTSB-WORK.
01045 041300 02 FILLER PIC X(1600).
01046 041400 01 INJ-01.
01047 041500 02 INJ-02 PIC X(13).
01048 041600 02 INJURY REDEFINES INJ-02 PIC 9(13).
01049 041700 01 DIST-01.
01050 041800 02 DIST-02 PIC 9(4).
01051 041900 01 S-01.
01052 042000 02 SEAT PIC 9(13).
01053 042100 01 MK-MDU.
01054 042200 02 MK PIC XXX.
01055 042300 02 MDU PIC XX.
01056 042400 01 S-B-01.
01057 042500 02 SEAT-BELT PIC 9(13).
01058 042600 01 ANGLE-01.
01059 042700 02 ANGLE-02 PIC 99.
01060 042800 01 VEL-01.
01061 042900 02 VEL-02 PIC 9(13).
01062 043000 01 TYP-OP-01.
01063 043100 02 TYP-OP-02 PIC X(22) VALUE 'ABCGHIJKMNQSTUV
01064 043200 02 TYP-OP REDEFINES 'WXYZ367'.
01065 043300 02 TYP-OP-02 OCCURS 22 TIMES PIC X.
01066 043400 01 TYP-TOT-01.
01067 043500 03 TYP-TOT-03 OCCURS 23 TIMES.
01068 043600 04 TYP-TOT OCCURS 5 TIMES PIC 9(5).
01069 043700 01 OP-PH-TOT.
01070 043800 03 OP-PH-03 OCCURS 43 TIMES.
01071 043900 04 OP-PH-04 OCCURS 5 TIMES PIC 9(5).
01072 044000 01 CAUSE-01.
01073 044100 02 CAUSE-492 OCCURS 487 TIMES PIC 9(5).
01074 044200 01 CAUSE-FATAL-01.
01075 044300 02 CAUSE-FATAL OCCURS 487 TIMES PIC 9(5).
01076 044400 01 CAUSE-NONFAT-01.
01077 044500 02 CAUSE-NON-FAT OCCURS 487 TIMES PIC 9(5).
01078 044600 01 PAGE-1-01.
01079 044700 02 PAGE-1-02.
01080 044800 03 PAGE-1-03A.
01081 044900 04 FILLER PIC X(32) VALUE
01082 045000 'AIRCRAFT MANUFACTURER / MODEL - '.
01083 045100 04 PAGE-1-MAKE PIC X(11).
01084 045200 04 FILLER PIC X(3) VALUE ' / '.
01085 045300 04 PAGE-1-MOD PIC X(16).
01086 045400 04 FILLER PIC X(16) VALUE SPACES.
01087 045500 03 PAGE-1-03C.
01088 045600 04 FILLER PIC X(34) VALUE 'MAXIMUM TO WEIGHT -
01089 045700 'POUNDS'.
01090 045800 04 FILLER PIC X(34) VALUE SPACES
01091 045900
01092 046000
01093 046100
01094 046200

01095	046300	03	FILLER PIC X(68) VALUE 'WING CONFIGURATION
01096	046400-		
01097	046500	03	FILLER PIC X(68) VALUE 'NUMBER OF ENGINES / LOCATION
01098	046600-		
01099	046700	03	FILLER PIC X(68) VALUE 'GENERAL INFORMATION
01100	046800-		
01101	046900	03	PAGE-1-03D.
01102	047000	04	FILLER PIC X(63) VALUE ' TOTAL NUMBER OF ACCID
01103	047100-	04	'ENTS SURVEYED - - - - -
01104	047200	04	PG-1-TOTA PIC Z(5).
01105	047300	03	PAGE-1-03DB.
01106	047400	04	FILLER PIC X(63) VALUE ' TOTAL APPLICABLE ACCI
01107	047500-	04	'ENTS SURVEYED - - - - -
01108	047600	04	PG-1-TOTAB PIC Z(5).
01109	047700	03	PAGE-1-03E.
01110	047800	04	FILLER PIC X(63) VALUE ' TOTAL NUMBER OF OCCUPA
01111	047900-	04	'ENTS - - - - -
01112	048000	04	PG-1-TOTB PIC Z(5).
01113	048100	03	PAGE-1-03F.
01114	048200	04	FILLER PIC X(63) VALUE ' AVERAGE NUMBER OF OCCU
01115	048300-	04	'PANTS PER ACCIDENT - - - - -
01116	048400	04	PG-1-TOTC PIC Z(5).
01117	048500	03	PAGE-1-03G.
01118	048600	04	FILLER PIC X(63) VALUE ' NUMBER OF ACCIDENTS WI
01119	048700-	04	'TH AT LEAST ONE (1) FATAL INJURY - - -
01120	048800	04	PG-1-TOTD PIC Z(5).
01121	048900	03	PAGE-1-03H.
01122	049000	04	FILLER PIC X(63) VALUE ' NUMBER OF ACCIDENTS WI
01123	049100-	04	'TH AT LEAST ONE (1) SERIOUS INJURY - - -
01124	049200	04	PG-1-TOTE PIC Z(5).
01125	049300	03	FILLER PIC X(68) VALUE ' AND NONE MORE SERIOUS
01126	049400-		
01127	049500	03	PAGE-1-03J.
01128	049600	04	FILLER PIC X(63) VALUE ' NUMBER OF ACCIDENTS WI
01129	049700-	04	'TH AT LEAST ONE (1) MINOR INJURY - - -
01130	049800	04	PG-1-TOTF PIC Z(5).
01131	049900	03	FILLER PIC X(68) VALUE ' AND NONE MORE SERIOUS
01132	050000-		
01133	050100	03	PAGE-1-03L.
01134	050200	04	FILLER PIC X(63) VALUE ' NUMBER OF ACCIDENTS WI
01135	050300-	04	'TH NO INJURY - - - - -
01136	050400	04	PG-1-TOTH PIC Z(5).
01137	050500	03	FILLER PIC X(68) VALUE ' AND NONE MORE SERIOUS
01138	050600-		
01139	050700	03	FILLER PIC X(68) VALUE ' ***** TOTALS OF SER
01140	050800-		'IOUSNESS OF INJURIES *****
01141	050900	03	FILLER PIC X(68) VALUE ' FATAL SE
01142	051000-		'RIOUS MINOR NONE
01143	051100	03	PAGE-1-03M.
01144	051200	04	FILLER PIC X(19) VALUE ' PILOT
01145	051300	04	PG-1-TOTI PIC Z(5).
01146	051400	04	FILLER PIC X(4) VALUE SPACES.
01147	051500	04	PG-1-TOTJ PIC Z(5).
01148	051600	04	FILLER PIC X(4) VALUE SPACES.
01149	051700	04	PG-1-TOTK PIC Z(5).
01150	051800	04	FILLER PIC X(4) VALUE SPACES.
01151	051900	04	PG-1-TOTL PIC Z(5).
01152	052000	04	FILLER PIC X(17) VALUE SPACES.
01153	052100	03	PAGE-1-03N.
01154	052200	04	FILLER PIC X(19) VALUE ' COPILOT
01155	052300	04	PG-1-TOTM PIC Z(5).
01156	052400	04	FILLER PIC X(4) VALUE SPACES.
01157	052500	04	PG-1-TOTN PIC Z(5).
01158	052600	04	FILLER PIC X(4) VALUE SPACES.
01159	052700	04	PG-1-TOTP PIC Z(5).
01160	052800	04	FILLER PIC X(4) VALUE SPACES.
01161	052900	04	PG-1-TOTQ PIC Z(5).
01162	053000	04	FILLER PIC X(17) VALUE SPACES.
01163	053100	03	PAGE-1-03P.
01164	053200	04	FILLER PIC X(19) VALUE ' PASSENGERS
01165	053300	04	PG-1-TOTR PIC Z(5).
01166	053400	04	FILLER PIC X(4) VALUE SPACES.
01167	053500	04	PG-1-TOTS PIC Z(5).

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01169 053600 04 FILLER PIC X(4) VALUE SPACES.
01170 053700 04 PG-1-TOTT PIC Z(5).
01171 053800 04 FILLER PIC X(4) VALUE SPACES.
01172 053900 04 PG-1-TOTU PIC Z(5).
01173 054000 04 FILLER PIC X(17) VALUE SPACES.
01174 054100 03 PAGE-1-030.
01175 054200 04 FILLER PIC X(19) VALUE ' * OTHER '
01176 054300 04 PG-1-TOTV PIC Z(5).
01177 054400 04 FILLER PIC X(4) VALUE SPACES.
01178 054500 04 PG-1-TOTW PIC Z(5).
01179 054600 04 FILLER PIC X(4) VALUE SPACES.
01180 054700 04 PG-1-TOTX PIC Z(5).
01181 054800 04 FILLER PIC X(4) VALUE SPACES.
01182 054900 04 PG-1-TOTY PIC Z(5).
01183 055000 04 FILLER PIC X(17) VALUE SPACES.
01184 055100 03 FILLER PIC X(68) VALUE ' * OTHER INCLUDES D
01185 055200- 'UAL STUDENT & CHECK PILOT
01186 055300 02 PAGE-1 REDEFINES PAGE-1-02 OCCURS 23 TIMES PIC X(68).
01187 055400 01 PAGE-2-01.
01188 055500 02 PAGE-2-02.
01189 055600 03 FILLER PIC X(120) VALUE 'FLIGHT CONDITIONS -
01190 055700-
01191 055800-
01192 055900-
01193 056000-
01194 056100-
01195 056200-
01196 056300-
01197 056400-
01198 056500-
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01200 056700-
01201 056800-
01202 056900-
01203 057000-
01204 057100-
01205 057200-
01206 057300-
01207 057400-
01208 057500-
01209 057600-
01210 057700-
01211 057800-
01212 057900-
01213 058000-
01214 058100-
01215 058200-
01216 058300-
01217 058400-
01218 058500-
01219 058600-
01220 058700-
01221 058800-
01222 058900-
01223 059000-
01224 059100-
01225 059200-
01226 059300-
01227 059400-
01228 059500-
01229 059600-
01230 059700-
01231 059800-
01232 059900-
01233 060000-
01234 060100-
01235 060200-
01236 060300-
01237 060400-
01238 060500-
01239 060600-
01240 060700-
060800

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04 PG-1-TOTT PIC Z(5).
04 FILLER PIC X(4) VALUE SPACES.
04 PG-1-TOTU PIC Z(5).
04 FILLER PIC X(17) VALUE SPACES.
03 PAGE-1-030.
04 FILLER PIC X(19) VALUE ' * OTHER '
04 PG-1-TOTV PIC Z(5).
04 FILLER PIC X(4) VALUE SPACES.
04 PG-1-TOTW PIC Z(5).
04 FILLER PIC X(4) VALUE SPACES.
04 PG-1-TOTX PIC Z(5).
04 FILLER PIC X(4) VALUE SPACES.
04 PG-1-TOTY PIC Z(5).
04 FILLER PIC X(17) VALUE SPACES.
03 FILLER PIC X(68) VALUE ' * OTHER INCLUDES D
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02 PAGE-2-01.
02 PAGE-2-02.
03 FILLER PIC X(120) VALUE 'FLIGHT CONDITIONS -
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03 FILLER PIC X(120) VALUE ' TOTAL NUMBER OF ACCIDENTS WHICH OCCURRED DURING THE FOLLOWING FIVE MAJOR PHASES OF OPERATION /
03 FILLER PIC X(120) VALUE ' NUMBER OF ACCIDENTS WITH AT LEAST ONE FATALITY WHICH OCCURRED DURING THE MAJOR PHASE
03 PAGE-2-03A.
04 FILLER PIC X(128) VALUE '
' TAKEOFF - - '
04 PG-2-TO PIC Z(5).
04 FILLER PIC X(3) VALUE ' / '.
04 PG-2-TOFAT PIC Z(5).
04 FILLER PIC X(79) VALUE SPACES.
03 PAGE-2-03B.
04 FILLER PIC X(128) VALUE '
' IN FLIGHT - '
04 PG-2-IF PIC Z(5).
04 FILLER PIC X(3) VALUE ' / '.
04 PG-2-IFFAT PIC Z(5).
04 FILLER PIC X(79) VALUE SPACES.
03 PAGE-2-03C.
04 FILLER PIC X(128) VALUE '
' LANDING - - '
04 PG-2-LDG PIC Z(5).
04 FILLER PIC X(3) VALUE ' / '.
04 PG-2-LDG FAT PIC Z(5).
04 FILLER PIC X(79) VALUE SPACES.
03 PAGE-2-03CB.
04 FILLER PIC X(128) VALUE '
' OTHER - - - '
04 PG-2-OTHER PIC Z(5).
04 FILLER PIC X(3) VALUE ' / '.
04 PG-2-OTHER FAT PIC Z(5).
04 FILLER PIC X(79) VALUE SPACES.
03 PAGE-2-03CC.
04 FILLER PIC X(128) VALUE '
' NOT REPORTED '
04 PG-2-NR PIC Z(5).
04 FILLER PIC X(3) VALUE ' / '.
04 PG-2-NR FAT PIC Z(5).
04 FILLER PIC X(79) VALUE SPACES.
03 FILLER PIC X(120) VALUE ' NINE (9) MOST FREQUENT MINOR PHASES OF OPERATION WITHIN THE FIRST THREE MAJOR PHASES ABOVE
03 FILLER PIC X(120) VALUE ' LISTED IN DESCENDING ORDER OF FREQUENCY
03 FILLER PIC X(120) VALUE ' MINOR PHASE OF OPERATION
' TAL NO. ***** INJURIES ***** '
03 FILLER PIC X(120) VALUE ' TO
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01241 060900-
01242 061000-
01243 061100-
01244 061200-
01245 061300-
01246 061400-
01247 061500-
01248 061600-
01249 061700-
01250 061800-
01251 061900-
01252 062000-
01253 062100-
01254 062200-
01255 062300-
01256 062400-
01257 062500-
01258 062600-
01259 062700-
01260 062800-
01261 062900-
01262 063000-
01263 063100-
01264 063200-
01265 063300-
01266 063400-
01267 063500-
01268 063600-
01269 063700-
01270 063800-
01271 063900-
01272 064000-
01273 064100-
01274 064200-
01275 064300-
01276 064400-
01277 064500-
01278 064600-
01279 064700-
01280 064800-
01281 064900-
01282 065000-
01283 065100-
01284 065200-
01285 065300-
01286 065400-
01287 065500-
01288 065600-
01289 065700-
01290 065800-
01291 065900-
01292 066000-
01293 066100-
01294 066200-
01295 066300-
01296 066400-
01297 066500-
01298 066600-
01299 066700-
01300 066800-
01301 066900-
01302 067000-
01303 067100-
01304 067200-
01305 067300-
01306 067400-
01307 067500-
01308 067600-
01309 067700-
01310 067800-
01311 067900-
01312 068000-
01313 068100-

03 ACCIDENTS FATAL SERIOUS MINOR NONE . OF
PAGE-2-03D OCCURS 9 TIMES.
04 FILLER PIC X(7).
04 MP-NO PIC Z9.
04 PERIOD-04 PIC XX.
04 MINOR PI PIC X(68).
04 FILLER PIC XX.
04 TOT-ACC-MP PIC Z(5).
04 FILLER PIC X(5).
04 FAT-INJ-MP PIC Z(5).
04 FILLER PIC X(3).
04 SER-INJ-MP PIC Z(5).
04 FILLER PIC X(3).
04 MIN-INJ-MP PIC Z(5).
04 FILLER PIC X(3).
04 NON-INJ-MP PIC Z(5).
03 FILLER PIC X(120) VALUE . EIGHT (8) MOST FREQUENT
TYPES OF ACCIDENTS WITHIN THE FIRST THREE MAJOR PHA
SES ABOVE
03 FILLER PIC X(120) VALUE . LISTED IN DESCEND
ING ORDER OF FREQUENCY
03 FILLER PIC X(120) VALUE .
TYPE OF ACCIDENT TO
TAL NO. ***** INJURIES *****
03 FILLER PIC X(120) VALUE . OF
ACCIDENTS FATAL SERIOUS MINOR NONE .
03 PAGE-2-03DA OCCURS 8 TIMES.
04 FILLER PIC X(7).
04 TYP-NO PIC Z9.
04 PERIODT-04 PIC XX.
04 TYP-DESC PIC X(68).
04 FILLER PIC XX.
04 TOT-ACC-TYP PIC Z(5).
04 FILLER PIC X(5).
04 FAT-INJ-TYP PIC Z(5).
04 FILLER PIC XXX.
04 SER-INJ-TYP PIC Z(5).
04 FILLER PIC XXX.
04 MIN-INJ-TYP PIC Z(5).
04 FILLER PIC XXX.
04 NON-INJ-TYP PIC Z(5).
03 FILLER PIC X(120) VALUE . NOTE -- OTHER IS SUM OF ALL
ACCEPTABLE PHASES AND TYPES EXCEPT THOSE LISTED
02 PAGE-2 REDEFINES PAGE-2-02 OCCURS 34 TIMES PIC X(120).
01 PAGE-3-01.
02 PAGE-3-02.
03 FILLER PIC X(120) VALUE . IMPACT CONDITIONS
03 PAGE-3-03E.
04 FILLER PIC X(60) VALUE . TOTAL NUMBER OF ACCI
DENTS WHICH RECORD IMPACT ANGLES - .
04 TOT-IMPACT PIC Z(5).
04 FILLER PIC X(55) VALUE SPACES.
03 FILLER PIC X(120) VALUE . IMPACT ANGLE NUMERICAL
SUMMARY -
03 FILLER PIC X(120) VALUE . AVERAGE ANGLE
IMPACT ANGLE CATEGORIES - DEGREES
03 FILLER PIC X(120) VALUE . DEGREES
03 FILLER PIC X(120) VALUE .
0 -15 16-30 31-45 46-60 61-75 7
6-90 90+
03 PAGE-3-03F.
04 FILLER PIC X(13) VALUE SPACES.
04 AVG-ANGLE-3 PIC Z(5).

01315 068000 04 FILLER PIC X(11) VALUE SPACES.
01316 068100 04 F0-15 PIC Z(5).
01317 068200 04 FILLER PIC X(5) VALUE SPACES.
01318 068300 04 F16-30 PIC Z(5).
01319 068400 04 FILLER PIC X(5) VALUE SPACES.
01320 068500 04 F31-45 PIC Z(5).
01321 068600 04 FILLER PIC X(5) VALUE SPACES.
01322 068700 04 F46-60 PIC Z(5).
01323 068800 04 FILLER PIC X(5) VALUE SPACES.
01324 068900 04 F61-75 PIC Z(5).
01325 069000 04 FILLER PIC X(5) VALUE SPACES.
01326 069100 04 F76-90 PIC Z(5).
01327 069200 04 FILLER PIC X(5) VALUE SPACES.
01328 069300 04 F90 PIC Z(5).
01329 069400 04 FILLER PIC X(26) VALUE SPACES.
01330 069500 03 PAGE-3-03G.
01331 069600- 04 FILLER PIC X(73) VALUE ' TOTAL NUMBER OF ACCI
01332 069700 04 'DENTS WHICH RECORD IMPACT VELOCITY - '.
01333 069800 04 VEL-IMP PIC Z(5).
01334 069900 03 FILLER PIC X(120) VALUE ' IMPACT VELOCITY NUMERIC
01335 070000- 'AL SUMMARY -
01336 070100-
01337 070200 03 FILLER PIC X(120) VALUE ' AVERAGE VELOCITY
01338 070300- IMPACT VELOCITY CATEGORIES - KNOTS
01339 070400-
01340 070500 03 FILLER PIC X(120) VALUE ' KNOTS
01341 070600-
01342 070700-
01343 070800 03 FILLER PIC X(120) VALUE '
01344 070900- ' 1-30 31-60 61-90 91-120 120+
01345 071000-
01346 071100 03 PAGE-3-03H.
01347 071200 04 FILLER PIC X(65) VALUE ' TOTAL NUMBER OF ACCI
01348 071300- 'DENTS WHICH RECORD STOPPING DISTANCES - '.
01349 071400 04 STOP-DIST PIC Z(5).
01350 071500 04 FILLER PIC X(50) VALUE SPACES.
01351 071600 03 FILLER PIC X(120) VALUE ' STOPPING DISTANCE NUMER
01352 071700- 'ICAL SUMMARY -
01353 071800-
01354 071900 03 FILLER PIC X(120) VALUE ' AVERAGE STOPPING
01355 072000- STOPPING DISTANCE CATEGORIES - FEET
01356 072100-
01357 072200 03 FILLER PIC X(120) VALUE ' DISTANCE - FEET
01358 072300-
01359 072400-
01360 072500 03 FILLER PIC X(120) VALUE '
01361 072600- ' 1-59 60-119 120-179 180-239 240-299 300
01362 072700- '-359 360+
01363 072800 03 FILLER PIC X(120) VALUE ' OCCUPANT INJURY NUMERIC
01364 072900- 'AL SUMMARY AT RESPECTIVE AIRCRAFT DAMAGE SEVERITY IN
01365 073000- 'DICES -
01366 073100 03 FILLER PIC X(120) VALUE ' DAMAGE SEVERITY
01367 073200- ' * * * * OCCUPANT INJURY * * * *
01368 073300-
01369 073400 03 FILLER PIC X(120) VALUE '
01370 073500- ' FATAL SERIOUS MINOR NONE
01371 073600-
01372 073700 03 PAGE-3-03I OCCURS 5 TIMES.
01373 073800 04 FILLER PIC X(12).
01374 073900 04 SEV-NAME PIC X(8).
01375 074000 04 FILLER PIC X(16).
01376 074100 04 SEV-FAT PIC Z(5).
01377 074200 04 FILLER PIC X(5).
01378 074300 04 SEV-SER PIC Z(5).
01379 074400 04 FILLER PIC X(5).
01380 074500 04 SEV-MIN PIC Z(5).
01381 074600 04 FILLER PIC X(5).
01382 074700 04 SEV-NON PIC Z(5).
01383 074800 04 FILLER PIC X(49).
01384 074900 02 PAGE-3 REDEFINES PAGE-3-02 OCCURS 25 TIMES PIC X(120).
01385 075000 02 PAGE-4-02.
01386 075100 03 FILLER PIC X(91) VALUE 'AIRCRAFT CABIN ACCOMMODATION

01387	075200-	IS -
01388	075300-	
01389	075400-	
01390	075500-	03 PAGE-4-03A. FILLER PIC X(63) VALUE ' NUMBER OF ACCIDENTS
01391	075600-	IN WHICH SEAT FAILURE OCCURRED - - -
01392	075700-	04 SEAT-FAIL-ACC PIC Z(5).
01393	075800-	04 FILLER PIC X(23) VALUE SPACES.
01394	075900-	03 PAGE-4-03B. FILLER PIC X(63) VALUE ' TOTAL NUMBER OF SEAT
01395	076000-	FAILURES - - - - -
01396	076100-	04 SEAT-FAIL PIC Z(5).
01397	076200-	04 FILLER PIC X(23) VALUE SPACES.
01398	076300-	03 PAGE-4-03C. FILLER PIC X(63) VALUE ' NUMBER OF ACCIDENTS
01399	076400-	IN WHICH SEAT BELT FAILURE OCCURRED -
01400	076500-	04 SEAT-BELT-ACC PIC Z(5).
01401	076600-	04 FILLER PIC X(23) VALUE SPACES.
01402	076700-	03 PAGE-4-03D. FILLER PIC X(63) VALUE ' TOTAL NUMBER OF SEAT
01403	076800-	BELT FAILURES - - - - -
01404	076900-	04 SEAT-BELT-FAIL PIC Z(5).
01405	077000-	04 FILLER PIC X(23) VALUE SPACES.
01406	077100-	03 PAGE-4-03E. FILLER PIC X(63) VALUE ' * NUMBER OF SHOULDER H
01407	077200-	ARNESSES USED - - - - -
01408	077300-	04 SH-HARN-USED PIC Z(5).
01409	077400-	04 FILLER PIC X(23) VALUE SPACES.
01410	077500-	03 PAGE-4-03F. FILLER PIC X(63) VALUE ' * NUMBER OF SHOULDER H
01411	077600-	ARNESSES FAILURES - - - - -
01412	077700-	04 SH-HARN-FAIL PIC Z(5).
01413	077800-	04 FILLER PIC X(23) VALUE SPACES.
01414	077900-	03 PAGE-4-03G. FILLER PIC X(63) VALUE ' * NUMBER OF CRASH HELM
01415	078000-	ETS USED / NOT USED - - - - -
01416	078100-	04 CRASH-HELM-USED PIC Z(5).
01417	078200-	04 FILLER PIC X(3) VALUE ' / '.
01418	078300-	04 CRASH-HELM-UNUSED PIC Z(5).
01419	078400-	04 FILLER PIC X(15) VALUE SPACES.
01420	078500-	03 FILLER PIC X(91) VALUE ' * APPLICABLE TO AGRIC
01421	078600-	CULTURAL AIRCRAFT ONLY
01422	078700-	03 FILLER PIC X(91) VALUE ' IMPACT AREA
01423	078800-	
01424	078900-	03 FILLER PIC X(91) VALUE ' PERCENT OF ACCIDENTS WHI
01425	079000-	CH OCCURRED IN PARTICULAR TERRAIN TYPE
01426	079100-	03 FILLER PIC X(91) VALUE ' TERRAIN TYPE
01427	079200-	
01428	079300-	03 FILLER PIC X(91) VALUE ' PERCENT
01429	079400-	
01430	079500-	03 FILLER PIC X(91) VALUE ' ACC
01431	079600-	
01432	079700-	
01433	079800-	
01434	079900-	
01435	080000-	
01436	080100-	
01437	080200-	
01438	080300-	
01439	080400-	
01440	080500-	
01441	080600-	
01442	080700-	
01443	080800-	
01444	080900-	
01445	081000-	
01446	081100-	
01447	081200-	
01448	081300-	
01449	081400-	
01450	081500-	
01451	081600-	
01452	081700-	
01453	081800-	
01454	081900-	
01455	082000-	
01456	082100-	
01457	082200-	
01458	082300-	
01459	082400-	

02 PAGE-4 REDEFINES PAGE-4-02 OCCURS 29 TIMES PIC X(91).

02 PAGE-5-02.

03 FILLER PIC X(110) VALUE 'CAUSE / FACTOR SUMMARY

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01460 082600-
01462 082700-
01463 082800-
01464 082900-
01465 083000-
01466 083100-
01467 083200-
01468 083300-
01469 083400-
01470 083500-
01471 083600-
01472 083700-
01473 083800-
01474 083900-
01475 084000-
01476 084100-
01477 084200-
01478 084300-
01479 084400-
01480 084500-
01481 084600-
01482 084700-
01483 084800-
01484 084900-
01485 085000-
01486 085100-
01487 085200-
01488 085300-
01489 085400-
01490 085500-
01491 085600-
01492 085700-
01493 085800-
01494 085900-
01495 086000-
01496 086100-
01497 086200-
01498 086300-
01499 086400-
01500 086500-
01501 086600-
01502 086700-
01503 086800-
01504 086900-
01505 087000-
01506 087100-
01507 087200-
01508 087300-
01509 087400-
01510 087500-
01511 087600-
01512 087700-
01513 087800-
01514 087900-
01515 088000-
01516 088100-
01517 088200-
01518 088300-
01519 088400-
01520 088500-
01521 088600-
01522 088700-
01523 088800-
01524 088900-
01525 089000-
01526 089100-
01527 089200-
01528 089300-
01529 089400-
01530 089500-
01531 089600-
01532 089700-

03 FILLER PIC X(110) VALUE '
      CAUSE
      FATAL NONFATAL
03 FILLER PIC X(110) VALUE '
      ACCIDENTS ACCIDENTS
03 PAGE-5-02A.
04 FILLER PIC X(5) VALUE SPACES.
04 CF-NO PIC X.
04 FILLER PIC XX VALUE ' '.
04 CAUSE-FACTOR-5 PIC X(68).
04 FILLER PIC X(7) VALUE SPACES.
04 FILLER PIC X(3) VALUE SPACES.
04 CF-FATALS PIC Z(5).
04 FILLER PIC X(10) VALUE SPACES.
04 CF-NONFAT PIC Z(5).
04 FILLER PIC X(12) VALUE SPACES.
03 FILLER PIC X(110) VALUE ' * * PILOT * *
      '
03 FILLER PIC X(110) VALUE ' * * COPILOT * *
      '
03 FILLER PIC X(110) VALUE ' * * DUAL STUDENT * *
      '
03 FILLER PIC X(110) VALUE ' * * CHECK PILOT * *
      '
03 FILLER PIC X(110) VALUE ' * * AIRFRAME * *
      '
03 FILLER PIC X(110) VALUE ' * * MISCELLANEOUS ACTS, COND
      ITIONS * *
02 PAGE-5 REDEFINES PAGE-5-02 OCCURS 10 TIMES PIC X(110).
P-IND-REC-01.
02 P-IND-02.
03 P-IND-DESC PIC X(48).
03 P-IND-ENG PIC X(68).
01 GTOT-OP-01.
02 GTOT-OP-02.
03 GTOT-OP-03 OCCURS 43 TIMES.
04 GTOT-OP OCCURS 5 TIMES PIC 9(5).
01 GTOT-TYP-01.
02 GTOT-TYP-02.
03 GTOT-TYP-03 OCCURS 23 TIMES.
04 GTOT-TYP OCCURS 5 TIMES PIC 9(5).
01 G-CAUSE-01.
02 G-CAUSE OCCURS 487 TIMES PIC 9(5).
01 G-CAUSE-FAT-01.
02 G-CAUSE-FAT OCCURS 487 TIMES PIC 9(5).
01 G-CAUSE-NONFAT-01.
02 G-CAUSE-NONFAT OCCURS 487 TIMES PIC 9(5).
01 OP-PH-01.
02 OP-PH-CODE.
03 FILLER PIC X(22) VALUE 'COCIC2C3C4C5C6DADBDDDE'.
03 FILLER PIC X(22) VALUE 'DFDGDHDIJDJDKDLDMDNDND1'.
03 FILLER PIC X(22) VALUE 'D2D3D4D5D6D7D8D9EAEBECE'.
03 FILLER PIC X(22) VALUE 'EDEEEFEGEHEIEJEKZ'.
02 OP-PH REDEFINES OP-PH-CODE OCCURS 42 TIMES PIC XX.
01 CAUSE-FACTOR-01.
02 CAUSE-FACTOR-02.
03 FILLER PIC X(28) VALUE '6401640264036404640564066407'.
03 FILLER PIC X(28) VALUE '6408640964106411641264136414'.
03 FILLER PIC X(28) VALUE '6415641664176418641964206421'.
03 FILLER PIC X(28) VALUE '6422642364246425642664276428'.
03 FILLER PIC X(28) VALUE '6429643064316432643364346435'.
03 FILLER PIC X(28) VALUE '6436643764386439644064416442'.
03 FILLER PIC X(28) VALUE '6443644464456446644764486449'.
03 FILLER PIC X(28) VALUE '6451645264536454645564566457'.
03 FILLER PIC X(28) VALUE '646464656466646764686469'.
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01533 089800 03 FILLER PIC X(28) VALUE '6480648164826501650265036504'
01534 089900 03 FILLER PIC X(28) VALUE '6505650665076508650965106511'
01535 090000 03 FILLER PIC X(28) VALUE '6512651365146515651665176518'
01536 090100 03 FILLER PIC X(28) VALUE '6519652065216522652365246525'
01537 090200 03 FILLER PIC X(28) VALUE '6526652765286529653065316532'
01538 090300 03 FILLER PIC X(28) VALUE '6533653465356536653765386539'
01539 090400 03 FILLER PIC X(28) VALUE '6540654265436544654565466547'
01540 090500 03 FILLER PIC X(28) VALUE '6548654965506551655265536554'
01541 090600 03 FILLER PIC X(28) VALUE '6555655665576558655965606561'
01542 090700 03 FILLER PIC X(28) VALUE '6571657465757658657965806581'
01543 090800 03 FILLER PIC X(28) VALUE '6602660366046605660666076608'
01544 090900 03 FILLER PIC X(28) VALUE '6609661066116612661366146615'
01545 091000 03 FILLER PIC X(28) VALUE '6616661766186619662066216622'
01546 091100 03 FILLER PIC X(28) VALUE '6623662466256626662766286629'
01547 091200 03 FILLER PIC X(28) VALUE '6630663166326633663466356636'
01548 091300 03 FILLER PIC X(28) VALUE '6637663866396640664166426643'
01549 091400 03 FILLER PIC X(28) VALUE '6645664666476648664966506651'
01550 091500 03 FILLER PIC X(28) VALUE '6652665366546655665666576658'
01551 091600 03 FILLER PIC X(28) VALUE '6665666666676668666966706671'
01552 091700 03 FILLER PIC X(28) VALUE '6681668266836684668566866687'
01553 091800 03 FILLER PIC X(28) VALUE '6706670767086709671067116712'
01554 091900 03 FILLER PIC X(28) VALUE '6713671467156716671767186719'
01555 092000 03 FILLER PIC X(28) VALUE '6720672167226723672467256726'
01556 092100 03 FILLER PIC X(28) VALUE '6727672867296730673167326733'
01557 092200 03 FILLER PIC X(28) VALUE '6734673567366737673867396740'
01558 092300 03 FILLER PIC X(28) VALUE '6742674367446745674667476748'
01559 092400 03 FILLER PIC X(28) VALUE '6749675067516752675367546755'
01560 092500 03 FILLER PIC X(28) VALUE '6756676267636764676567666767'
01561 092600 03 FILLER PIC X(28) VALUE '6774677967806781678270AA70AB'
01562 092700 03 FILLER PIC X(28) VALUE '70AC70AD70AE70AF70AG70AH70AJ'
01563 092800 03 FILLER PIC X(28) VALUE '70AY70BA70BB70BC70BD70BE70BF'
01564 092900 03 FILLER PIC X(28) VALUE '70BG70BH70BI70BJ70BK70CA70CB'
01565 093000 03 FILLER PIC X(28) VALUE '70CC70CD70CE70CF70CG70CH70CI'
01566 093100 03 FILLER PIC X(28) VALUE '70CJ70CK70CL70CM70CN70CP70CQ'
01567 093200 03 FILLER PIC X(28) VALUE '70D070D170D270D370D470D570D6'
01568 093300 03 FILLER PIC X(28) VALUE '70D988A888AC88AD88AE88AF88B0'
01569 093400 03 FILLER PIC X(28) VALUE '88AF88AG88AH88AI88AJ88AK88AL'
01570 093500 03 FILLER PIC X(28) VALUE '88AM88AN88AP88AQ88AR88AS88AT'
01571 093600 03 FILLER PIC X(28) VALUE '88AU88AV88AW88AX88AY88BA88BB'
01572 093700 03 FILLER PIC X(28) VALUE '88BC88BD88BE88BF88BG88BH88BI'
01573 093800 03 FILLER PIC X(28) VALUE '88BJ88BK88BL88BM88BN88BO88BP'
01574 093900 03 FILLER PIC X(28) VALUE '88BQ88BR88BS88BT88BU88BV88BW'
01575 094000 03 FILLER PIC X(28) VALUE '88BX88BY88BZ88CB88CD88CE88CF'
01576 094100 03 FILLER PIC X(28) VALUE '88CG88CH88CI88CJ88CK88CL88CM'
01577 094200 03 FILLER PIC X(28) VALUE '88CN88CO88CP88CQ88CR88CS88CT'
01578 094300 03 FILLER PIC X(28) VALUE '88CU88CV88CW88CX88CY88CZ88DA'
01579 094400 03 FILLER PIC X(28) VALUE '88DB88DC88DD88DE88DF88D088D1'
01580 094500 03 FILLER PIC X(28) VALUE '88D288D388D488D588D688D788D8'
01581 094600 03 FILLER PIC X(28) VALUE '88D988D1088D1188D1288D1388D14'
01582 094700 03 FILLER PIC X(28) VALUE '88D1688D1788D1888D1988D2088D21'
01583 094800 03 FILLER PIC X(28) VALUE '88D2388D2488D2588D2688D2788D28'
01584 094900 03 FILLER PIC X(28) VALUE '88D3088D3188D3288D3388D3488D35'
01585 095000 03 FILLER PIC X(28) VALUE '88D3788D3888D3988D4088D4188D42'
01586 095100 03 FILLER PIC X(28) VALUE '88D4488D4588D4688D4788D4888D49'
01587 095200 03 FILLER PIC X(28) VALUE '88D5188D5288D5388D5488D5588D56'
01588 095300 03 FILLER PIC X(28) VALUE '88D5888D5988D6088D6188D6288D63'
01589 095400 03 FILLER PIC X(28) VALUE '88D6588D6688D6788D6888D6988D70'
01590 095500 03 FILLER PIC X(28) VALUE '88D7588D7688D7788D7888D7988D80'
01591 095600 03 FILLER PIC X(28) VALUE '88D8288D8388D8488D8588D8688D87'
01592 095700 03 FILLER PIC X(28) VALUE '88D8988D9088D9188D9288D9388D94'
01593 095800 03 FILLER PIC X(28) VALUE '88D9688D9788D9888D99'
01594 095900 02 CAUSE-FACTOR-02R REDEFINES CAUSE-FACTOR-02
01595 096000 OCCURS 500 TIMES PIC X(14).
01596 096100 01 SAVE-SUB-01.
01597 096200 02 SAVE-SUB OCCURS 16 TIMES PIC 99.
01598 096300 01 G-PG-1-01.
01599 096400 02 G-PG-1-02 OCCURS 4 TIMES.
01600 096500 03 G-PG-1 OCCURS 4 TIMES PIC 9(5).
01601 096600 01 PG-1-SERIOUS-01.
01602 096700 02 PG-1-SER-02 OCCURS 4 TIMES.
01603 096800 03 PG-1-SER OCCURS 4 TIMES PIC 9(5).
01604 096900 01 HOLD-ARRAY-01.
01605 097000 02 HOLD-ARRAY OCCURS 6 TIMES PIC X(3).
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01606 097100 01 C-SAVE-01.
01607 097200 02 C-SAVE-02 OCCURS 4 TIMES PIC 9(3).
01608 097300 01 CAUSE-FACTOR-HOLD.
01609 097400 02 FACTOR-02 PIC XX.
01610 097500 02 CAUSE-02 PIC XX.
01611 097600 01 GTERRAIN-01.
01612 097700 02 GTERRAIN-COUNT OCCURS 13 TIMES PIC 9(4).
01613 097800 01 G-SERIOUS.
01614 097900 02 GSER OCCURS 5 TIMES INDEXED BY GS-INDEX.
01615 098000 03 GS OCCURS 4 TIMES INDEXED BY GSERIOUS-INDEX
01616 098100 PIC 9(5).
01617 098200 01 F080R-01.
01618 098300 02 F080B-A PIC X(12).
01619 098400 02 FILLER PIC X(6).
01620 098500 01 PAGE-4-WORK.
01621 098600 02 PAGE-4-W02 OCCURS 13 TIMES PIC X(91).
01622 098700 PROCEDURE DIVISION.
01623 098800 OPEN INPUT NTSB, HEAD
01624 098900 OUTPUT PRT, HEAD
01625 099000 MOVE SPACES TO FILL-ER.
01626 099100 MOVE SEVERITY-77 TO SEVERITY.
01627 099200 MOVE TERRAIN-77 TO TERRAIN-01.
01628 099300 MOVE TYPES-77 TO TYPES-01.
01629 099400 MOVE ZERO TO G-PG-1-01.
01630 099500 MOVE ZERO TO GTERRAIN-01.
01631 099600 MOVE ZERO TO GTOT-UP-01 G-SERIOUS G-CAUSE-FAT-01.
01632 099700 MOVE ZERO TO G-CAUSE-01 GTOT-TYP-01 G-SERIOUS G-PG-1-01.
01633 099800 MOVE ZERO TO G-CAUSE-NONFAT-01.
01634 099900 MOVE SPACES TO P-WORK.
01635 099910*
01636 099920***** PLACE PERCENT SYMBOL IN ITS FIELD
01637 099930*
01638 100000 MOVE-PCT.
01639 100100 ADD 1 TO I.
01640 100200 IF I GREATER THAN 13 MOVE ZERO TO I
01641 100300 GO TO READ-NTSB ELSE
01642 100400 MOVE PERCENT TO FILLER-4-03H (1)
01643 100500 GO TO MOVE-PCT.
01644 100600 READ-NTSB.
01645 100700 READ NTSB INTO NTSB-WORK AT END
01646 100800 CLOSE NTSB WITH LOCK
01647 100900 PERFORM PRINT-SUMMARY THRU END-PAGE-5
01648 101000 PERFORM INITIALIZE-COUNTERS THRU END-INITIALIZE
01649 101100 GO TO EUJ.
01650 101200*
01651 101300***** INITIALIZE COUNTERS AND FLAGS
01652 101400*
01653 101500 CHECK-HOLD.
01654 101600 IF NOT (F012 = HOLD-MAKE AND F013 = HOLD-MODEL)
01655 101700 ADD 1 TO SUMMARY-COUNTER
01656 101800 IF SUMMARY-COUNTER GREATER THAN 1
01657 101900 PERFORM PRINT-SUMMARY THRU END-PAGE-5.
01658 102000 IF NOT(F012 = HOLD-MAKE AND F013 = HOLD-MODEL)
01659 102100 PERFORM INITIALIZE-COUNTERS THRU END-INITIALIZE
01660 102200 MOVE F006 TO HOLD-MAKE-NAME
01661 102300 MOVE F012 TO HOLD-MAKE
01662 102400 MOVE F013 TO HOLD-MODEL.
01663 102500 MOVE 1 TO O.
01664 102600 ADD 1 TO GTOT-AC.
01665 102700 ADD 1 TO TOT-AC.
01666 102800*
01667 103100***** SEARCH TYPE OF ACCIDENT IN MAJOR FIELD BUT REJECT THOSE
01668 103200***** FOR WHICH A MATCH IS FOUND.
01669 103300*
01670 103400 SEARCH-TYPES.
01671 103500 ADD 1 TO J.
01672 103600 IF J GREATER THAN 12
01673 103700 MOVE ZERO TO J
01674 103800 MOVE '0' TO ADD-TOT-AC
01675 103900 GO TO TOTAL-AC.
01676 104000 IF TYYP (J) = F02801
01677 104100 MOVE ZERO TO J
01678 104200 MOVE '1' TO ADD-TOT-AC
01679 104300

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01679 104400 GO TO READ-NTSB.
01680 104500 GO TO SEARCH-TYPES.
01681 104600 TOTAL-AC.
01682 104700*
01683 104800***** ACCUMULATE TOTAL FATALITIES, SERIOUS, MINOR & NONE
01684 104900*
01685 105000* SKIP ALL Z CODES IN TOTAL ON BOARD AREA
01686 105100*
01687 105200 IF F02901 = 'C'
01688 105300 ADD 1 TO GTOT-T-0
01689 105400 ADD 1 TO TOT-T-0
01690 105500 IF F079 = 'F' ADD 1 TO FAT-TU
01691 105600 ADD 1 TO GFAT-TU.
01692 105700 IF F02901 = 'D'
01693 105800 ADD 1 TO GTOT-FLY
01694 105900 ADD 1 TO TOT-FLY
01695 106000 IF F079 = 'F' ADD 1 TO FAT-INFLT
01696 106100 ADD 1 TO GFAT-INFLT.
01697 106200 IF F02901 = 'E'
01698 106300 ADD 1 TO GTOT-LDG
01699 106400 ADD 1 TO TOT-LDG
01700 106500 IF F079 = 'F' ADD 1 TO FAT-LDG
01701 106600 ADD 1 TO GFAT-LDG.
01702 106700 IF F02901 = 'A' OR 'B'
01703 106800 ADD 1 TO GTOT-TS
01704 106900 ADD 1 TO TOT-TS
01705 107000 IF F079 = 'F' ADD 1 TO FAT-TS
01706 107100 ADD 1 TO GFAT-TS.
01707 107200 IF F02901 = 'Z' OR ' '
01708 107300 ADD 1 TO GTOT-NR
01709 107400 ADD 1 TO TOT-NR
01710 107500 IF F079 = 'F' ADD 1 TO FAT-NR
01711 107600 ADD 1 TO GFAT-NR.
01712 107610*
01713 107620***** CHECK OPERATIONAL PHASES - TAKE-OFF, IN FLIGHT & LANDING
01714 107630*
01715 107700 IF NOT (F02901 = 'C' OR 'D' OR 'E')
01716 107800 GO TO READ-NTSB.
01717 107900 ADD 1 TO TOT-AC-TYPE.
01718 108000 ADD 1 TO GTOT-AC-TYPE.
01719 108100 TRANSFORM F080B (3) FROM SPACES TO ZEROS.
01720 108200 MOVE F0800101B (3,1,6) TO REC-TOT-OCC.
01721 108300 ADD REC-TOT-OCC TO TOT-OCC.
01722 108400 ADD REC-TOT-OCC TO GTOT-OCC.
01723 108500 IF TOT-AC-TYPE NOT = ZERO
01724 108600 DIVIDE TOT-OCC BY TOT-AC-TYPE GIVING AV-OCC ROUNDED.
01725 108700 IF GTOT-AC-TYPE NOT = ZERO
01726 108800 DIVIDE GTOT-OCC BY GTOT-AC-TYPE GIVING GAVG-OCC ROUNDED.
01727 108900*
01728 109000**** TALLY THE HIGHEST SEVERITY LEVEL RECORDED FOR THE ACCIDENT.
01729 109100**** FOR PAGE 1 SUMMARY USING TOTAL ON BOARD FIELD
01730 109200*
01731 109300 MOVE F0800101B (3,1,1) TO NTSBXY1.
01732 109400 MOVE F0800101B (3,1,2) TO NTSBXY2.
01733 109500 MOVE F0800101B (3,1,3) TO NTSBXY3.
01734 109600 MOVE F0800101B (3,1,4) TO NTSBXY4.
01735 109700 IF F079 = 'F'
01736 109800 ADD 1 TO GTOT-FAT
01737 109900 ADD 1 TO TOT-FAT.
01738 110000 IF NTSBXY1 IS = ZEROS AND
01739 110100 NTSBXY2 IS NOT = ZEROS
01740 110200 ADD 1 TO GTOT-SER
01741 110300 ADD 1 TO TOT-SER.
01742 110400 IF NTSBXY1 IS = ZEROS AND
01743 110500 NTSBXY2 IS = ZEROS AND
01744 110600 NTSBXY3 IS NOT = ZEROS
01745 110700 ADD 1 TO GTOT-MNR
01746 110800 ADD 1 TO TOT-MNR.
01747 110900 IF NTSBXY1 IS = ZEROS AND
01748 111000 NTSBXY2 = ZERO AND
01749 111100 NTSBXY3 = ZERO AND
01750 111200 NTSBXY4 IS NOT = ZEROS
01751 111300 ADD 1 TO GTOT-NON

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01752 111400 ADD 1 TO TOT-NON.
01753 111500*
01754 111600***** ACCUMULATE INJURIES INTO PILOT, COPILOT, PASSENGERS AND
01755 111700***** OTHERS. OTHERS TO INCLUDE DUAL STUDENT AND CHECK PILOT.
01756 111800*
01757 111900 MOVE 1 TO SER-SUB.
01758 112000 ACCUMULATE-PG-1.
01759 112100 IF SER-SUB = 5 MOVE 4 TO S-SUB
01760 112200 ELSE MOVE SER-SUB TO S-SUB.
01761 112300 IF SER-SUB = 1 MOVE F08001A (1) TO HOLD-ARRAY-01.
01762 112400 IF SER-SUB = 2 MOVE F08001A (2) TO HOLD-ARRAY-01.
01763 112500 IF SER-SUB = 3 MOVE F08001B (2,3) TO HOLD-ARRAY-01.
01764 112600 IF SER-SUB = 4 MOVE F08001A (3) TO HOLD-ARRAY-01.
01765 112700 IF SER-SUB = 5 MOVE F08001B (1,1) TO HOLD-ARRAY-01.
01766 112800 MOVE HOLD-ARRAY (1) TO NTSBXY1.
01767 112900 MOVE HOLD-ARRAY (2) TO NTSBXY2.
01768 113000 MOVE HOLD-ARRAY (3) TO NTSBXY3.
01769 113100 MOVE HOLD-ARRAY (4) TO NTSBXY4.
01770 113200 ADD NTSBXY1 TO PG-1-SER (S-SUB, 1).
01771 113300 ADD NTSBXY2 TO PG-1-SER (S-SUB, 2).
01772 113400 ADD NTSBXY3 TO PG-1-SER (S-SUB, 3).
01773 113500 ADD NTSBXY4 TO PG-1-SER (S-SUB, 4).
01774 113600 ADD NTSBXY1 TO G-PG-1 (S-SUB, 1).
01775 113700 ADD NTSBXY2 TO G-PG-1 (S-SUB, 2).
01776 113800 ADD NTSBXY3 TO G-PG-1 (S-SUB, 3).
01777 113900 ADD NTSBXY4 TO G-PG-1 (S-SUB, 4).
01778 114000 ADD 1 TO SER-SUB.
01779 114100 IF SER-SUB GREATER THAN 5 NEXT SENTENCE
01780 114200 ELSE GO TO ACCUMULATE-PG-1.
01781 114300*
01782 114400***** CHECK FOR PRESENCE OF IMPACT ANGLE, IMPACT VELOCITY,
01783 114500***** STOPPING DISTANCE, SEAT FAILURE, SEAT BELT FAILURE OR ATT
01784 114600***** AT IMPACT.
01785 114700*
01786 114800 PRINT-CRITERIA.
01787 114900 IF F13302 = SPACES NEXT SENTENCE ELSE
01788 115000 EXAMINE F13302 TALLYING ALL 'Z'.
01789 115100 IF TALLY = ZERO GO TO FORM-RECORD.
01790 115200 MOVE ZERO TO TALLY.
01791 115300 IF F136 = SPACES NEXT SENTENCE ELSE
01792 115400 EXAMINE F136 TALLYING ALL 'Z'.
01793 115500 IF TALLY = ZERO GO TO FORM-RECORD.
01794 115600 MOVE ZERO TO TALLY.
01795 115700 IF F152 = SPACES NEXT SENTENCE ELSE
01796 115800 EXAMINE F152 TALLYING ALL 'Z'.
01797 115900 IF TALLY = ZERO GO TO FORM-RECORD.
01798 116000 MOVE ZERO TO TALLY.
01799 116100 IF F139 = SPACES NEXT SENTENCE ELSE
01800 116200 EXAMINE F139 TALLYING ALL 'Z'.
01801 116300 IF TALLY = ZERO GO TO FORM-RECORD.
01802 116400 MOVE ZERO TO TALLY.
01803 116500 IF F140 = SPACES NEXT SENTENCE ELSE
01804 116600 EXAMINE F140 TALLYING ALL 'Z'.
01805 116700 IF TALLY = ZERO GO TO FORM-RECORD.
01806 116800 MOVE ZERO TO TALLY.
01807 116900 IF F151 = SPACES NEXT SENTENCE ELSE
01808 117000 EXAMINE F151 TALLYING ALL 'Z'.
01809 117100 IF TALLY NOT = 3 MOVE ZERO TO TALLY
01810 117200 GO TO FORM-RECORD.
01811 117300 MOVE ZERO TO TALLY.
01812 117400 GO TO CABIN-INJURY.
01813 117500 FORM-RECORD.
01814 117600 MOVE '0' TO READER-SWITCH.
01815 117700 IF ADD-TOT-AC = '1'
01816 117800 MOVE '0' TO ADD-TOT-AC
01817 117900 ADD 1 TO GTOT-AC
01818 118000 ADD 1 TO TOT-AC.
01819 118100 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 0.
01820 118200 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 3.
01821 118300*
01822 118400***** CHECK DATE OF ACCIDENT
01823 118500 MOVE SPACES TO P-WORK.
01824 118600*

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01825 118700 IF F004 = SPACES OR F00401 = 'Z' NEXT SENTENCE ELSE
01826 118800 MOVE F004 TO DATE-HOLD-01A
01827 118900 MOVE DA TO DA-8
01828 119000 MOVE MO TO MO-8
01829 119100 MOVE YR TO YR-8
01830 119200 MOVE DATE-HOLD-01B TO FDATA
01831 119300 PERFORM MOVE-DIRECT.
01832 119400 ADD 1 TO D.
01833 119500*
01834 119600***** CHECK AIRCRAFT MAKE
01835 119700*
01836 119800 IF F006 = SPACES NEXT SENTENCE ELSE
01837 119900 MOVE F006 TO FDATA
01838 120000 PERFORM MOVE-DIRECT.
01839 120100 ADD 1 TO D.
01840 120200*
01841 120300***** CHECK AIRCRAFT MODEL
01842 120400*
01843 120500 IF F007 = SPACES NEXT SENTENCE ELSE
01844 120600 MOVE F007 TO FDATA
01845 120700 PERFORM MOVE-DIRECT.
01846 120800 ADD 1 TO D.
01847 120900 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
01848 121000*
01849 121100***** CHECK AIRCRAFT DAMAGE
01850 121200*
01851 121300 IF F021 = SPACES OR 'Z' NEXT SENTENCE ELSE
01852 121400 MOVE SPACES TO HD-KEY
01853 121500 MOVE 013434 TO CCC
01854 121600 MOVE F021 TO CHAR1
01855 121700 PERFORM READER THRU REXIT.
01856 121800 ADD 1 TO D.
01857 121900*
01858 122000***** FIRE AFTER IMPACT
01859 122100*
01860 122200 IF F022 = SPACES OR 'Z' NEXT SENTENCE ELSE
01861 122300 MOVE SPACES TO HD-KEY
01862 122400 MOVE 013535 TO CCC
01863 122500 MOVE F022 TO CHAR1
01864 122600 PERFORM READER THRU REXIT.
01865 122700 ADD 1 TO D.
01866 122800*
01867 122900***** KIND OF FLYING
01868 123000*
01869 123100 IF F025 = SPACES OR 'CZ' OR 'DZ' NEXT SENTENCE ELSE
01870 123200 MOVE SPACES TO HD-KEY
01871 123300 MOVE 013940 TO CCC
01872 123400 MOVE F025 TO CODE2
01873 123500 PERFORM READER THRU REXIT.
01874 123600 ADD 1 TO D.
01875 123700 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
01876 123800*
01877 123900***** FIRST TYPE OF ACCIDENT
01878 124000*
01879 124100 IF F028 = SPACES OR '7' NEXT SENTENCE ELSE
01880 124200 ADD 1 TO HEAD-COUNT
01881 124300 MOVE SPACES TO HD-KEY
01882 124400 MOVE 014447 TO CCC
01883 124500 MOVE F02801 TO CHAR2
01884 124600 PERFORM READER THRU REXIT.
01885 124700 IF F02802 NOT = SPACES
01886 124800 ADD 1 TO HEAD-COUNT
01887 124900 MOVE F02802 TO CHAR1
01888 125000 PERFORM READER THRU REXIT.
01889 125100 ADD 1 TO D.
01890 125200 MOVE ZERO TO HEAD-COUNT.
01891 125300 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
01892 125400*
01893 125500***** FIRST PHASE OF OPERATION
01894 125600*
01895 125700 IF F029 = SPACES OR '2' NEXT SENTENCE ELSE
01896 125800 ADD 1 TO HEAD-COUNT
01897 125900 MOVE SPACES TO HD-KEY

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01898 126000 MOVE 014851 TO CCC
01899 126100 MOVE F02901 TO CHAR2
01900 126200 PERFORM READER THRU REXIT.
01901 126300 IF F02902 NOT = SPACES
01902 126400 ADD 1 TO HEAD-COUNT
01903 126500 MOVE F02902 TO CHAR1
01904 126600 PERFORM READER THRU REXIT.
01905 126700 ADD 1 TO D.
01906 126800 MOVE ZERO TO HEAD-COUNT.
01907 126900*
01908 127000***** SECONDARY TYPE OF ACCIDENT
01909 127100*
01910 127200 IF F030 = SPACES OR '7' NEXT SENTENCE ELSE
01911 127300 ADD 1 TO HEAD-COUNT
01912 127400 MOVE SPACES TO HD-KEY
01913 127500 MOVE 014447 TO CCC
01914 127600 MOVE F03001 TO CHAR2
01915 127700 PERFORM READER THRU REXIT.
01916 127800 IF F03002 NOT = SPACES
01917 127900 ADD 1 TO HEAD-COUNT
01918 128000 MOVE F03002 TO CHAR1
01919 128100 PERFORM READER THRU REXIT.
01920 128200 ADD 1 TO D.
01921 128300 MOVE ZERO TO HEAD-COUNT.
01922 128400*
01923 128500***** SECONDARY PHASE OF OPERATION
01924 128600*
01925 128700 IF F031 = SPACES OR 'Z' NEXT SENTENCE ELSE
01926 128800 ADD 1 TO HEAD-COUNT
01927 128900 MOVE SPACES TO HD-KEY
01928 129000 MOVE 014851 TO CCC
01929 129100 MOVE F03101 TO CHAR2
01930 129200 PERFORM READER THRU REXIT.
01931 129300 IF F03102 NOT = SPACES
01932 129400 ADD 1 TO HEAD-COUNT
01933 129500 MOVE F03102 TO CHAR1
01934 129600 PERFORM READER THRU REXIT.
01935 129700 ADD 1 TO D.
01936 129800 MOVE ZERO TO HEAD-COUNT.
01937 129900*
01938 130000***** AIRCRAFT SPEED
01939 130100*
01940 130200 EXAMINE F034 TALLYING ALL 'Z'.
01941 130300 IF F034 = SPACES OR TALLY GREATER THAN ZERO NEXT SENTENCE
01942 130400 ELSE
01943 130500 EXAMINE F034 REPLACING LEADING ZERO BY SPACES
01944 130600 MOVE F034 TO FDATA
01945 130700 PERFORM MOVE-DIRECT.
01946 130800 ADD 1 TO D.
01947 130900 MOVE ZERO TO TALLY.
01948 131000*
01949 131100***** AIRPORT PROXIMITY
01950 131200*
01951 131300 IF F048 = SPACES OR 'Z' NEXT SENTENCE ELSE
01952 131400 MOVE SPACES TO HD-KEY
01953 131500 MOVE 023131 TO CCC
01954 131600 MOVE F048 TO CHAR1
01955 131700 PERFORM READER THRU REXIT.
01956 131800 ADD 1 TO D.
01957 131900*
01958 132000***** RUNWAY COMPOSITION
01959 132100*
01960 132200 IF F054 = SPACES OR 'Z' NEXT SENTENCE ELSE
01961 132300 MOVE SPACES TO HD-KEY
01962 132400 MOVE 026161 TO CCC
01963 132500 MOVE F054 TO CHAR1
01964 132600 PERFORM READER THRU REXIT.
01965 132700 ADD 1 TO D.
01966 132800*
01967 132900***** RUNWAY SURFACE
01968 133000*
01969 133100 IF F055 = SPACES OR 'Z' NEXT SENTENCE ELSE
01970 133200 MOVE SPACES TO HD-KEY

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01971 133300      MOVE 026262 TO CCC
01972 133400      MOVE F055 TO CHAR1
01973 133500      PERFORM READER THRU REXIT.
01974 133600      ADD 1 TO D.
01975 133700*
01976 133800***** RUNWAY HAZARDS
01977 133900*
01978 134000      IF F057 = SPACES OR 'Z' NEXT SENTENCE ELSE
01979 134100          MOVE SPACES TO HD-KEY
01980 134200          MOVE 026565 TO CCC
01981 134300          MOVE F057 TO CHAR1
01982 134400          PERFORM READER THRU REXIT.
01983 134500      ADD 1 TO D.
01984 134600*
01985 134700***** RUNWAY LENGTH
01986 134800*
01987 134900      EXAMINE F060 TALLYING ALL 'Z'.
01988 135000      IF F060 = SPACES OR TALLY GREATER THAN ZERO NEXT SENTENCE
01989 135100          ELSE
01990 135200          EXAMINE F060 REPLACING LEADING ZERO BY SPACES
01991 135300          MOVE F060 TO FDATA
01992 135400          PERFORM MOVE-DIRECT.
01993 135500      ADD 1 TO D.
01994 135600      MOVE ZERO TO TALLY.
01995 135700*
01996 135800***** TERRAIN TYPE
01997 135900*
01998 136000      IF F065 = SPACES OR 'Z' NEXT SENTENCE ELSE
01999 136100          MOVE SPACES TO HD-KEY
02000 136200          MOVE 042222 TO CCC
02001 136300          MOVE F065 TO CHAR1
02002 136400          PERFORM READER THRU REXIT.
02003 136500      ADD 1 TO D.
02004 136600*
02005 136700***** CAUSE / FACTOR
02006 136800*
02007 136900      MOVE 1 TO CFF.
02008 137000      MOVE SPACES TO P-WORK
02009 137100      WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
02010 137200      MOVE '          CAUSE / FACTOR' TO
02011 137300          DESCRIPTION.
02012 137400      WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
02013 137500      PERFORM C-F-PRINT THRU C-F-EXIT UNTIL CFF GREATER THAN 10.
02014 137600      MOVE ZERO TO HEAD-COUNT.
02015 137700*
02016 137800***** INJURY INDEX
02017 137900*
02018 138000      MOVE SPACES TO P-WORK.
02019 138100      WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
02020 138200      MOVE '          INJURY - INDEX' TO
02021 138300          DESCRIPTION.
02022 138400      WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
02023 138500      MOVE SPACES TO P-WORK.
02024 138600      MOVE ' F S M N Z T ' TO DATA.
02025 138700      WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
02026 138800      MOVE SPACES TO P-WORK.
02027 138900      INJ-PRINT.
02028 139000      IF F080A = SPACES GO TO CHECK-PILOT.
02029 139100      PERFORM UNIQUE THRU END-UNIQUE 3 TIMES.
02030 139200      MOVE 1 TO INJ1.
02031 139300*
02032 139400***** CHECK PILOT INJURIES
02033 139500*
02034 139600      CHECK-PILOT.
02035 139700      IF F08001B (1, 1) = ZERO NEXT SENTENCE ELSE
02036 139800          MOVE F08001B (1, 1) TO F08001A (1)
02037 139900          PERFORM UNIQUE THRU END-UNIQUE.
02038 140000      MOVE 1 TO INJ1.
02039 140100      IF F08001B (1, 1) = ZERO ADD 1 TO D.
02040 140200*
02041 140300***** PASSENGER INJURIES
02042 140400*
02043 140500      IF F08001B (2, 3) = ZERO NEXT SENTENCE ELSE

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02044 140600      MOVE F08001B (2, 3) TO F08001A (1)
02045 140700      PERFORM UNIQUE THRU END-UNIQUE.
02046 140800      MOVE 1 TO INJ1.
02047 140900      IF F08001B (2, 3) = ZERO    ADD 1 TO D.
02048 141000*
02049 141100***** TOTAL ABOARD INJURIES
02050 141200*
02051 141300      IF F08001B (3, 1) = ZERO    NEXT SENTENCE ELSE
02052 141400      MOVE F08001B (3, 1) TO F08001A (1)
02053 141500      PERFORM UNIQUE THRU END-UNIQUE.
02054 141600      MOVE 1 TO INJ1.
02055 141700      AFTER-INJURY.
02056 141800      IF F08001B (3, 1) = ZERO    ADD 1 TO D.
02057 141900      WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
02058 142000*
02059 142100***** REMARKS
02060 142200*
02061 142300      IF F08202 = SPACES NEXT SENTENCE ELSE
02062 142400      MOVE F08202 TO FDATA
02063 142500      PERFORM MOVE-DIRECT.
02064 142600      ADD 1 TO D.
02065 142700*
02066 142800***** SECOND REMARK
02067 142900*
02068 143000      IF F07801 (1) = '84' OR F083 = SPACES NEXT SENTENCE ELSE
02069 143100      MOVE F083 TO FDATA
02070 143200      PERFORM MOVE-DIRECT.
02071 143300      ADD 1 TO D.
02072 143400*
02073 143500***** AIRCRAFT SERIAL NUMBER
02074 143600*
02075 143700      IF F094 = SPACES OR F09401 = 'Z' NEXT SENTENCE ELSE
02076 143800      MOVE F094 TO FDATA
02077 143900      PERFORM MOVE-DIRECT.
02078 144000      ADD 1 TO D.
02079 144100*
02080 144200***** IMPACT SEVERITY
02081 144300*
02082 144400      IF F13101 = SPACES OR 'Z' OR ZERO NEXT SENTENCE ELSE
02083 144500      MOVE SPACES TO HD-KEY
02084 144600      MOVE 202323 TO CCC
02085 144700      MOVE F13301 TO CHAR1
02086 144800      PERFORM READER THRU REXIT.
02087 144900      ADD 1 TO D.
02088 145000*
02089 145100***** ANGLE OF IMPACT
02090 145200*
02091 145300      IF F13302 = SPACES OR 'Z' NEXT SENTENCE ELSE
02092 145400      MOVE F13302 TO FDATA
02093 145500      PERFORM MOVE-DIRECT.
02094 145600      ADD 1 TO D.
02095 145700*
02096 145800***** RATE OF DECELERATION
02097 145900*
02098 146000      IF F134 = SPACES OR 'Z' NEXT SENTENCE ELSE
02099 146100      MOVE SPACES TO HD-KEY
02100 146200      MOVE 202626 TO CCC
02101 146300      MOVE F134 TO CHAR1
02102 146400      PERFORM READER THRU REXIT.
02103 146500      ADD 1 TO D.
02104 146600*
02105 146700***** DIRECTION OF PRINCIPLE DECELERATION
02106 146800*
02107 146900      IF F135 = SPACES OR 'Z' NEXT SENTENCE ELSE
02108 147000      MOVE SPACES TO HD-KEY
02109 147100      MOVE 202727 TO CCC
02110 147200      MOVE F135 TO CHAR1
02111 147300      PERFORM READER THRU REXIT.
02112 147400      ADD 1 TO D.
02113 147500*
02114 147600***** STOPPING DISTANCE
02115 147700*
02116 147800      IF F136 = SPACES OR 'Z' OR ZERO NEXT SENTENCE ELSE

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02117 147900 EXAMINE F136 REPLACING LEADING ZERO BY SPACES
02118 148000 MOVE F136 TO FDATA
02119 148100 PERFORM MOVE-DIRECT.
02120 148200 ADD 1 TO D.
02121 148300*
02122 148400***** DAMAGE SEVERITY - IMPACT
02123 148500*
02124 148600 IF F13705 = SPACES OR 'Z' NEXT SENTENCE ELSE
02125 148700 MOVE SPACES TO HD-KEY
02126 148800 MOVE 203636 TO CCC
02127 148900 MOVE F13705 TO CHAR1
02128 149000 PERFORM READER THRU REXIT.
02129 149100 ADD 1 TO D.
02130 149200*
02131 149300***** SEATING CONFIGURATION
02132 149400*
02133 149500 IF F138 = SPACES OR 'Z' NEXT SENTENCE ELSE
02134 149600 MOVE SPACES TO HD-KEY
02135 149700 MOVE 203737 TO CCC
02136 149800 MOVE F138 TO CHAR1
02137 149900 PERFORM READER THRU REXIT.
02138 150000 ADD 1 TO D.
02139 150100*
02140 150200***** SEAT FAILURES
02141 150300*
02142 150400 IF F139 = SPACES OR 'Z' OR ZERO NEXT SENTENCE ELSE
02143 150500 EXAMINE F139 REPLACING LEADING ZERO BY SPACES
02144 150600 MOVE F139 TO FDATA
02145 150700 PERFORM MOVE-DIRECT.
02146 150800 ADD 1 TO D.
02147 150900*
02148 151000***** SEAT BELT FAILURES
02149 151100*
02150 151200
02151 151300 IF F140 = SPACES OR 'Z' OR ZERO NEXT SENTENCE ELSE
02152 151400 EXAMINE F140 REPLACING LEADING ZERO BY SPACES
02153 151500 MOVE F140 TO FDATA
02154 151600 PERFORM MOVE-DIRECT.
02155 151700 ADD 1 TO D.
02156 151800*
02157 151900***** DEATHS FROM FIRE AFTER IMPACT
02158 152000*
02159 152100 IF F141 = SPACES OR 'Z' OR ZERO NEXT SENTENCE ELSE
02160 152200 EXAMINE F141 REPLACING LEADING ZERO BY SPACES
02161 152300 MOVE F141 TO FDATA
02162 152400 PERFORM MOVE-DIRECT.
02163 152500 ADD 1 TO D.
02164 152600 MOVE '1' TO READER-SWITCH.
02165 152700*
02166 152800***** ATTITUDE AT IMPACT
02167 152900*
02168 153000 IF F151 = 'ZZZ'
02169 153100 ADD 3 TO D
02170 153200 GO TO AFTER-ATTITUDE.
02171 153300 IF F15101 = 'Z' NEXT SENTENCE ELSE
02172 153400 IF F15101 = SPACES MOVE SPACES TO ATTITUDE-1 ELSE
02173 153500 MOVE SPACES TO HD-KEY
02174 153600 MOVE 206464 TO CCC
02175 153700 MOVE F15101 TO CHAR1
02176 153800 PERFORM READER THRU REXIT
02177 153900 MOVE FDATA TO ATT-WORK
02178 154000 MOVE ATT-02 TO ATTITUDE-1.
02179 154100 ADD 1 TO D.
02180 154200 IF F15102 = 'Z' NEXT SENTENCE ELSE
02181 154300 IF F15102 = SPACES MOVE SPACES TO ATTITUDE-2 ELSE
02182 154400 MOVE SPACE TO HD-KEY
02183 154500 MOVE 206565 TO CCC
02184 154600 MOVE F15102 TO CHAR1
02185 154700 PERFORM READER THRU REXIT
02186 154800 MOVE FDATA TO ATT-WORK
02187 154900 MOVE ATT-02 TO ATTITUDE-2.
02188 155000 ADD 1 TO D.
02189 155100 IF F15103 = 'Z' NEXT SENTENCE ELSE
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02190 155200 IF F15103 = SPACES MOVE SPACES TO ATTITUDE-3 ELSE
02191 155300 MOVE SPACES TO HD-KEY
02192 155400 MOVE 206666 TO CCC
02193 155500 MOVE F15103 TO CHAR1
02194 155600 PERFORM READER THRU REXIT
02195 155700 MOVE FDATA TO ATT-WORK
02196 155800 MOVE ATT-02 TO ATTITUDE-3.
02197 155900 ADD 1 TO D.
02198 156000 AFTER-ATTITUDE.
02199 156100 MOVE '0' TO READER-SWITCH.
02200 156200*
02201 156300***** SPEED AT IMPACT
02202 156400*
02203 156500 IF F152 = SPACES OR 'Z' NEXT SENTENCE ELSE
02204 156600 MOVE F152 TO FDATA
02205 156700 PERFORM MOVE-DIRECT.
02206 156800 ADD 1 TO D.
02207 156900*
02208 157000***** TEST FOR AGRICULTURAL AIRCRAFT
02209 157100*
02210 157200 IF F02501 = 'C' AND (F02502 = 'A' OR 'B' OR 'C' OR 'D')
02211 157300 NEXT SENTENCE ELSE ADD 10 TO D GO TO CABIN-INJURY.
02212 157400*
02213 157500***** KIND OF OPERATION
02214 157600*
02215 157700 IF F192 = SPACES OR 'Z' NEXT SENTENCE ELSE
02216 157800 MOVE SPACES TO HD-KEY
02217 157900 MOVE 252121 TO CCC
02218 158000 MOVE F192 TO CHAR1
02219 158100 PERFORM READER THRU REXIT.
02220 158200 ADD 1 TO D.
02221 158300*
02222 158400***** SHOULDER HARNESS USED
02223 158500*
02224 158600 IF F198 = SPACES OR 'Z' NEXT SENTENCE ELSE
02225 158700 MOVE SPACES TO HD-KEY
02226 158800 MOVE 252727 TO CCC
02227 158900 MOVE F198 TO CHAR1
02228 159000 PERFORM READER THRU REXIT.
02229 159100 ADD 1 TO D.
02230 159200*
02231 159300***** SEAT BELT STATUS
02232 159400*
02233 159500 IF F199 = SPACES OR 'Z' NEXT SENTENCE ELSE
02234 159600 MOVE SPACES TO HD-KEY
02235 159700 MOVE 252828 TO CCC
02236 159800 MOVE F199 TO CHAR1
02237 159900 PERFORM READER THRU REXIT.
02238 160000 ADD 1 TO D.
02239 160100*
02240 160200***** CRASH HELMET STATUS
02241 160300*
02242 160400 IF F204 = SPACES OR 'Z' NEXT SENTENCE ELSE
02243 160500 MOVE SPACES TO HD-KEY
02244 160600 MOVE 253333 TO CCC
02245 160700 MOVE F204 TO CHAR1
02246 160800 PERFORM READER THRU REXIT.
02247 160900 ADD 1 TO D.
02248 161000*
02249 161100***** COCKPIT CRASH PAD STATUS
02250 161200*
02251 161300 IF F205 = SPACES OR 'Z' NEXT SENTENCE ELSE
02252 161400 MOVE SPACES TO HD-KEY
02253 161500 MOVE 253434 TO CCC
02254 161600 MOVE F205 TO CHAR1
02255 161700 PERFORM READER THRU REXIT.
02256 161800 ADD 1 TO D.
02257 161900*
02258 162000***** CRASH BAR STATUS
02259 162100*
02260 162200 IF F206 = SPACES OR 'Z' NEXT SENTENCE ELSE
02261 162300 MOVE SPACES TO HD-KEY
02262 162400 MOVE 253535 TO CCC

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02263 162500      MOVE F206 TO CHAR1
02264 162600      PERFORM READER THRU REXIT.
02265 162700      ADD 1 TO D.
02266 162800*
02267 162900***** OBSTRUCTION STATUS
02268 163000*
02269 163100      IF F20901 = SPACES OR 'Z' NEXT SENTENCE ELSE
02270 163200      MOVE SPACES TO HD-KEY
02271 163300      MOVE 255153 TO CCC
02272 163400      MOVE F20901 TO CHAR1
02273 163500      PERFORM READER THRU REXIT.
02274 163600      ADD 1 TO D.
02275 163700      IF F20902 = SPACES OR 'Z' NEXT SENTENCE ELSE
02276 163800      MOVE SPACES TO HD-KEY
02277 163900      MOVE 255153 TO CCC
02278 164000      MOVE F20902 TO CHAR1
02279 164100      PERFORM READER THRU REXIT.
02280 164200      ADD 1 TO D.
02281 164300      IF F20903 = SPACES OR 'Z' NEXT SENTENCE ELSE
02282 164400      MOVE SPACES TO HD-KEY
02283 164500      MOVE 255153 TO CCC
02284 164600      MOVE F20903 TO CHAR1
02285 164700      PERFORM READER THRU REXIT.
02286 164800      ADD 1 TO D.
02287 164900*
02288 165000***** TERRAIN TYPE
02289 165100*
02290 165200      IF F21001 = SPACES NEXT SENTENCE ELSE
02291 165300      MOVE SPACES TO HD-KEY
02292 165400      MOVE 255456 TO CCC
02293 165500      MOVE F21001 TO CHAR1
02294 165600      PERFORM READER THRU REXIT.
02295 165700      ADD 1 TO D.
02296 165800      IF F21002 = SPACES NEXT SENTENCE ELSE
02297 165900      MOVE SPACES TO HD-KEY
02298 166000      MOVE 255456 TO CCC
02299 166100      MOVE F21003 TO CHAR1
02300 166200      PERFORM READER THRU REXIT.
02301 166300*
02302 166400*
02303 166500*
02304 166600*
02305 166700*
02306 166800      INJURY SUMMARIES
02307 166900*
02308 167000      DID INJURY OCCUR IN CABIN
02309 167100*
02310 167200      CABIN-INJURY.
02311 167300*
02312 167400***** COLLECT PAGE 2 INFORMATION *****
02313 167500*
02314 167600      IF ADD-TOT-AC = '1'
02315 167700      ADD 1 TO TOT-AC
02316 167800      ADD 1 TO GTOT-AC.
02317 167900      MOVE F08001B (3,1) TO F0808-01.
02318 168000      DISPLAY 'STATEMENT 168100, F3808-01 = ' F0808-01.
02319 168100      IF F0808-A = ZERO GO TO IMPACT-ANGLE.
02320 168200*
02321 168300***** CHECK AND TALLY MINOR OPERATIONAL PHASES
02322 168400*
02323 168500      MOVE 42 TO HISAVE.
02324 168600      MOVE F029 TO SEARCH-CODE.
02325 168700      PERFORM OP-SEARCH THRU END-OP.
02326 168800      IF FOUND-WORD = '1' MOVE ZERO TO FOUND-WORD
02327 168900      GO TO LOAD-ARRAY.
02328 169000      GO TO CHECK-TYPES.
02329 169100*
02330 169200***** CHECK TOTAL ON BOARD AREA FOR VALUES IN INJURY CATEGORIES
02331 169300*
02332 169400      LOAD-ARRAY.
02333 169500      MOVE '0' TO BEEN-THERE.
02334 169600      IF F0800101B (3,1,1) NOT = ZERO
02335 169700      MOVE 1 TO UP
02336 170000      PERFORM SERIOUS-B THRU END-SERIOUS-B.
02337 170100      IF F0800101B (3,1,2) NOT = ZERO
02338 170200      MOVE 2 TO OP
02339 170300      PERFORM SERIOUS-B THRU END-SERIOUS-B.
02340 170400
02341 170500

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02336 170600 IF F0800101B (3,1,3) NOT = ZERO
02337 170700 MOVE 3 TO OP
02338 170800 PERFORM SERIOUS-B THRU END-SERIOUS-B.
02339 170900 IF F0800101B (3,1,4) NOT = ZERO
02340 171000 MOVE 4 TO OP
02341 171100 PERFORM SERIOUS-B THRU END-SERIOUS-B.
02342 171200
02343 171300*
02344 171400***** CHECK AND TALLY TYPES OF ACCIDENTS
02345 171500*
02346 171600 CHECK-TYPES.
02347 171700 MOVE 22 TO HISAVE.
02348 171800 MOVE F02801 TO SEARCH-TYPE.
02349 171900 PERFORM TYPE-SEARCH THRU END-TYPE.
02350 172000 IF FOUND-WORD = '1' MOVE ZERO TO FOUND-WORD
02351 172100 GO TO COLLECT-TYPES.
02352 172200 GO TO IMPACT-ANGLE.
02353 172300
02354 172400 COLLECT-TYPES.
02355 172500 MOVE '0' TO BEEN-THERE.
02356 172600 IF F0800101B (3,1,1) NOT = ZERO
02357 172700 MOVE 1 TO OP
02358 172800 PERFORM TYPE-COLLECT THRU END-COLLECT.
02359 172900 IF F0800101B (3,1,2) NOT = ZERO
02360 173000 MOVE 2 TO OP
02361 173100 PERFORM TYPE-COLLECT THRU END-COLLECT.
02362 173200 IF F0800101B (3,1,3) NOT = ZERO
02363 173300 MOVE 3 TO OP
02364 173400 PERFORM TYPE-COLLECT THRU END-COLLECT.
02365 173500
02366 173600 IF F0800101B (3,1,4) NOT = ZERO
02367 173700 MOVE 4 TO OP
02368 173800 PERFORM TYPE-COLLECT THRU END-COLLECT.
02369 173900
02370 174000 IMPACT-ANGLE.
02371 174100 IF F13302 = SPACES GO TO IMPACT-VELOCITY.
02372 174200 MOVE ZERO TO TALLY.
02373 174300 EXAMINE F13302 TALLYING ALL '2'.
02374 174400 IF TALLY NOT = ZERO GO TO IMPACT-VELOCITY.
02375 174500 IF F13302 IS GREATER THAN ' ' AND LESS THAN '16'
02376 174600 ADD 1 TO G-ANG-15
02377 174700 ADD 1 TO ANGLE-15.
02378 174800 IF F13302 IS GREATER THAN '15' AND LESS THAN '31'
02379 174900 ADD 1 TO G-ANG-30
02380 175000 ADD 1 TO ANGLE-30.
02381 175100 IF F13302 IS GREATER THAN '30' AND LESS THAN '46'
02382 175200 ADD 1 TO G-ANG-45
02383 175300 ADD 1 TO ANGLE-45.
02384 175400 IF F13302 IS GREATER THAN '45' AND LESS THAN '61'
02385 175500 ADD 1 TO G-ANG-60
02386 175600 ADD 1 TO ANGLE-60.
02387 175700 IF F13302 IS GREATER THAN '60' AND LESS THAN '76'
02388 175800 ADD 1 TO G-ANG-75
02389 175900 ADD 1 TO ANGLE-75.
02390 176000 IF F13302 IS GREATER THAN '75' AND LESS THAN '90'
02391 176100 ADD 1 TO G-ANG-90
02392 176200 ADD 1 TO ANGLE-90.
02393 176300 IF F13302 IS GREATER THAN '89'
02394 176400 ADD 1 TO G-ANG-90-PLUS
02395 176500 ADD 1 TO ANGLE-90-PLUS.
02396 176600
02397 176700 ADD 1 TO GTOT-ACC-ANG.
02398 176800 ADD 1 TO TOT-ACC-ANG.
02399 176900 TRANSFORM F13302 FROM SPACES TO ZERO.
02400 177000 MOVE F13302 TO ANGLE-01.
02401 177100 ADD ANGLE-02 TO ANGLE-SUM.
02402 177200 ADD ANGLE-02 TO G-ANG-SUM.
02403 177300 DIVIDE ANGLE-SUM BY TOT-ACC-ANG GIVING AVG-ANGLE ROUNDED.
02404 177400 DIVIDE G-ANG-SUM BY GTOT-ACC-ANG GIVING G-AVG-ANGLE ROUNDED.
02405 177500
02406 177600 IMPACT-VELOCITY.
02407 177700 EXAMINE F152 REPLACING LEADING ZERO BY SPACES.
02408 177800 IF F152 = SPACES GO TO STOPPING-DISTANCE.
02409 177900 MOVE ZERO TO TALLY.

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02409 178000 EXAMINE F152 TALLYING ALL 'Z'.
02410 178100 IF TALLY NOT = ZERO GO TO STOPPING-DISTANCE.
02411 178200 IF F152 GREATER THAN ' ' AND LESS THAN ' 31'
02412 178300 ADD 1 TO G-VEL-30
02413 178400 ADD 1 TO VEL-30.
02414 178500 IF F152 GREATER THAN ' 30' AND LESS THAN ' 61'
02415 178600 ADD 1 TO G-VEL-60
02416 178700 ADD 1 TO VEL-60.
02417 178800 IF F152 GREATER THAN ' 60' AND LESS THAN ' 91'
02418 178900 ADD 1 TO G-VEL-90
02419 179000 ADD 1 TO VEL-90.
02420 179100 IF F152 GREATER THAN ' 90' AND LESS THAN '120'
02421 179200 ADD 1 TO G-VEL-120
02422 179300 ADD 1 TO VEL-120.
02423 179400 IF F152 GREATER THAN '119'
02424 179500 ADD 1 TO G-VEL-120-PLUS
02425 179600 ADD 1 TO VEL-120-PLUS.
02426 179700 ADD 1 TO TOT-ACC-VEL.
02427 179800 ADD 1 TO GTOT-ACC-VEL.
02428 179900 TRANSFORM F152 FROM SPACES TO ZERO.
02429 180000 MOVE F152 TO VEL-01.
02430 180100 ADD VEL-02 TO VEL-SUM.
02431 180200 ADD VEL-02 TO G-VEL-SUM.
02432 180300 DIVIDE VEL-SUM BY TOT-ACC-VEL GIVING AVG-VEL ROUNDED.
02433 180400 DIVIDE G-VEL-SUM BY GTOT-ACC-VEL GIVING G-AVG-VEL ROUNDED.
02434 180500
02435 180600 STOPPING-DISTANCE.
02436 180700 EXAMINE F136 REPLACING LEADING ZERO BY SPACES.
02437 180800 IF F136 = SPACES GO TO OCCUPANT-INJURY.
02438 180900 MOVE ZERO TO TALLY.
02439 181000 EXAMINE F136 TALLYING ALL 'Z'.
02440 181100 IF TALLY NOT = ZERO GO TO SEAT-BELT-FAILURE.
02441 181200 IF F136 IS GREATER THAN ' ' AND LESS THAN ' 59'
02442 181300 ADD 1 TO G-DIST-10
02443 181400 ADD 1 TO DIST-10.
02444 181500 IF F136 IS GREATER THAN ' 59' AND LESS THAN ' 120'
02445 181600 ADD 1 TO G-DIST-20
02446 181700 ADD 1 TO DIST-20.
02447 181800 IF F136 IS GREATER THAN ' 119' AND LESS THAN ' 180'
02448 181900 ADD 1 TO G-DIST-30
02449 182000 ADD 1 TO DIST-30.
02450 182100 IF F136 IS GREATER THAN ' 179' AND LESS THAN ' 240'
02451 182200 ADD 1 TO G-DIST-40
02452 182300 ADD 1 TO DIST-40.
02453 182400 IF F136 IS GREATER THAN ' 239' AND LESS THAN ' 300'
02454 182500 ADD 1 TO G-DIST-50
02455 182600 ADD 1 TO DIST-50.
02456 182700 IF F136 IS GREATER THAN ' 299' AND LESS THAN ' 360'
02457 182800 ADD 1 TO G-DIST-60
02458 182900 ADD 1 TO DIST-60.
02459 183000 IF F136 IS GREATER THAN ' 359'
02460 183100 ADD 1 TO G-DIST-60-PLUS
02461 183200 ADD 1 TO DIST-60-PLUS.
02462 183300 ADD 1 TO TOT-ACC-DIST.
02463 183400 ADD 1 TO GTOT-ACC-DIST.
02464 183500 TRANSFORM F136 FROM SPACES TO ZEROS.
02465 183600 MOVE F136 TO DIST-01.
02466 183700 ADD DIST-02 TO DIST-SUM.
02467 183800 ADD DIST-02 TO G-DIST-SUM.
02468 183900 DIVIDE DIST-SUM BY TOT-ACC-DIST GIVING AVG-DIST ROUNDED.
02469 184000 DIVIDE G-DIST-SUM BY GTOT-ACC-DIST GIVING G-AVG-DIST ROUNDED.
02470 184100 OCCUPANT-INJURY.
02471 184200*
02472 184300***** NUMERICAL OCCUPANT INJURY SUMMARY
02473 184400*
02474 184500 IF F13705 IS = SPACES OR 'Z' GO TO TERRAIN-CHECK.
02475 184600 PERFORM SEVERITY-TEST THRU END-SEVERITY VARYING
02476 184700 SEVERITY-INDEX FROM 1 BY 1
02477 184800 UNTIL SEVERITY-INDEX GREATER THAN 5.
02478 184900 IF SEVERITY-INDEX IS GREATER THAN 5
02479 185000 GO TO TERRAIN-CHECK.
02480 185100 PERFORM-SERIOUS.
02481 185200 PERFORM SERIOUS-TEST THRU END-SERIOUS VARYING

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02482 185300          SERIOUS-INDEX FROM 1 BY 1
02483 185400          UNTIL SERIOUS-INDEX GREATER THAN 4.
02484 185500*
02485 185600***** SEARCH FOR ACCEPTABLE TERRAIN TYPE. IF FOUND INCREMENT
02486 185700***** THAT TERRAIN COUNT BY 1.
02487 185800*
02488 185900 TERRAIN-CHECK.
02489 186000          IF F065 = SPACES MOVE '2' TO F065.
02490 186100          PERFORM TERRAIN-A THRU END-TERRAIN VARYING TERRAIN-INDEX
02491 186200          FROM 1 BY 1 UNTIL F065 = TERRAIN (TERRAIN-INDEX) OR
02492 186300          TERRAIN-INDEX GREATER THAN 13.
02493 186400          IF TERRAIN-INDEX GREATER THAN 13 GO TO SEAT-BELT-FAILURE.
02494 186500          SET TER-IND TO TERRAIN-INDEX.
02495 186600          ADD 1 TO GTERRAIN-COUNT (TER-IND).
02496 186700          ADD 1 TO TERRAIN-COUNT (TER-IND).
02497 186800 SEAT-BELT-FAILURE.
02498 186900          IF F140 = SPACES OR ZERO GO TO SEAT-FAILURE.
02499 187000          MOVE ZERO TO TALLY.
02500 187100          EXAMINE F140 TALLYING ALL 'Z'.
02501 187200          IF TALLY NOT = ZERO GO TO SEAT-FAILURE.
02502 187300          ADD 1 TO GTOT-STBLT-ACC.
02503 187400          ADD 1 TO TOT-STBLT-ACC.
02504 187500          TRANSFORM F140 FROM SPACES TO ZERO.
02505 187600          MOVE F140 TO S-B-01.
02506 187700          ADD SEAT-BELT TO TOT-STBLT-FAIL.
02507 187800          ADD SEAT-BELT TO GTOT-STBLT-FAIL.
02508 187900 SEAT-FAILURE.
02509 188000          IF F139 = SPACES OR ZERO GO TO AG-PLANE.
02510 188100          MOVE ZERO TO TALLY.
02511 188200          EXAMINE F139 TALLYING ALL 'Z'.
02512 188300          IF TALLY NOT = ZERO GO TO AG-PLANE.
02513 188400          ADD 1 TO GTOT-ST-ACC.
02514 188500          ADD 1 TO TOT-ST-ACC.
02515 188600          TRANSFORM F139 FROM SPACES TO ZERO.
02516 188700          MOVE F139 TO S-01.
02517 188800          ADD SEAT TO TOT-ST-FAIL.
02518 188900          ADD SEAT TO GTOT-ST-FAIL.
02519 189000
02520 189100 AG-PLANE.
02521 189200          MOVE F012 TO MK.
02522 189300          MOVE F013 TO MOD.
02523 189400          IF MK-MOD = '03932' OR '07113' OR
02524 189500          '03405' OR '12426' OR '14803'
02525 189600          NEXT SENTENCE ELSE GO TO CAUSE-FACTOR-P.
02526 189700          IF F198 = 'A' OR 'B' OR 'C' OR 'E'
02527 189800          ADD 1 TO GS-H-INST
02528 189900          ADD 1 TO S-H-INSTALLED.
02529 190000          IF F198 = 'A' OR 'C' OR 'E'
02530 190100          ADD 1 TO GS-H-USED
02531 190200          ADD 1 TO S-H-USED.
02532 190300          IF F198 = 'B'
02533 190400          ADD 1 TO GS-H-FAILED
02534 190500          ADD 1 TO S-H-FAILED.
02535 190600          IF F204 = 'A'
02536 190700          ADD 1 TO GHET-USED
02537 190800          ADD 1 TO HELMET-USED.
02538 190900          IF F204 = 'B'
02539 191000          ADD 1 TO GHET-UNUSED
02540 191100          ADD 1 TO HELMET-UNUSED.
02541 191200*
02542 191300***** CAUSE-FACTOR SUMMARY
02543 191400*
02544 191500 CAUSE-FACTOR-P.
02545 191600          MOVE 487 TO HISAVE.
02546 191700          MOVE 1 TO CFF.
02547 191710*
02548 191720***** THIS PERFORM IS DONE 10 TIMES BECAUSE THERE ARE A POSSIBLE
02549 191730***** 10 CAUSE/FACTORS IN THE CAUSE-FACTOR FIELD
02550 191740*
02551 191800          PERFORM C-F-SEARCH THRU END-CF-SEARCH UNTIL CFF IS
02552 191900          GREATER THAN 10.
02553 192000          GO TO READ-NTSB.
02554 192100*

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02555 192200***** PRINT SUMMARIES
02556 192300*
02557 192400 PRINT-SUMMARY.
02558 192500 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 0.
02559 192600 WRITE P-REC FROM SUMMARY-HEAD-1 AFTER POSITIONING 3.
02560 192700 WRITE P-REC FROM SUMMARY-HEAD-2 AFTER POSITIONING 1.
02561 192800 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 2.
02562 192900 MOVE ZERO TO D.
02563 193000 STOP-SUMMARY.
02564 193100*
02565 193200***** FILL PAGE 1 FIELDS
02566 193300*
02567 193400 MOVE HOLD-MAKE-NAME TO PAGE-1-MAKE.
02568 193500 MOVE HOLD-MODEL TO PAGE-1-MOD.
02569 193600 MOVE TOT-AC TO PG-1-TOTA.
02570 193700 MOVE TOT-AC-TYPE TO PG-1-TOTAB.
02571 193800 MOVE TOT-OCC TO PG-1-TOTB.
02572 193900 MOVE AV-OCC TO PG-1-TOTC.
02573 194000 MOVE TOT-FAT TO PG-1-TOTD.
02574 194100 MOVE TOT-SER TO PG-1-TOTE.
02575 194200 MOVE TOT-MNR TO PG-1-TOTF.
02576 194300 MOVE TOT-NON TO PG-1-TOTH.
02577 194400 MOVE PG-1-SER (1, 1) TO PG-1-TOTI.
02578 194500 MOVE PG-1-SER (1, 2) TO PG-1-TOTJ.
02579 194600 MOVE PG-1-SER (1, 3) TO PG-1-TOTK.
02580 194700 MOVE PG-1-SER (1, 4) TO PG-1-TOTL.
02581 194800 MOVE PG-1-SER (2, 1) TO PG-1-TOTM.
02582 194900 MOVE PG-1-SER (2, 2) TO PG-1-TOTN.
02583 195000 MOVE PG-1-SER (2, 3) TO PG-1-TOTP.
02584 195100 MOVE PG-1-SER (2, 4) TO PG-1-TOTQ.
02585 195200 MOVE PG-1-SER (3, 1) TO PG-1-TOTR.
02586 195300 MOVE PG-1-SER (3, 2) TO PG-1-TOTS.
02587 195400 MOVE PG-1-SER (3, 3) TO PG-1-TOTT.
02588 195500 MOVE PG-1-SER (3, 4) TO PG-1-TOTU.
02589 195600 MOVE PG-1-SER (4, 1) TO PG-1-TOTV.
02590 195700 MOVE PG-1-SER (4, 2) TO PG-1-TOTW.
02591 195800 MOVE PG-1-SER (4, 3) TO PG-1-TOTX.
02592 195900 MOVE PG-1-SER (4, 4) TO PG-1-TOTY.
02593 196000 PERFORM PAGE-1-P THRU END-PG-1 UNTIL D = 23.
02594 196100 PERFORM SKIP-TO-HEAD.
02595 196200*
02596 196300***** FILL PAGE 2 FIELDS
02597 196400*
02598 196500 MOVE TOT-T-O TO PG-2-TO.
02599 196600 MOVE TOT-FLY TO PG-2-IF.
02600 196700 MOVE TOT-LDG TO PG-2-LDG.
02601 196800 MOVE FAT-IS TO PG-2-OTHERFAT.
02602 196900 MOVE TOT-IS TO PG-2-OTHER.
02603 197000 MOVE FAT-TO TO PG-2-TOFAT.
02604 197100 MOVE FAT-INFLI TO PG-2-IFFAT.
02605 197200 MOVE TOT-NR TO PG-2-NR.
02606 197300 MOVE FAT-NR TO PG-2-NRFAT.
02607 197400 MOVE FAT-LDG TO PG-2-LDGFAT.
02608 197500 MOVE ZERO TO SAVE-SUB-01.
02609 197600 MOVE 1 TO SS.
02610 197700 MOVE 1 TO OP.
02611 197800 MOVE ZERO TO SSS.
02612 197900*
02613 198000***** SEARCH OPERATIONAL PHASES TOTAL FIELD FOR 8 HIGHEST
02614 198100***** TOTAL NO. OF ACCIDENTS.
02615 198200*
02616 198300 SEARCH-UP-A.
02617 198400 MOVE OP-PH-04 (1, 5) TO OP-PH-HOLD.
02618 198500 IF SS GREATER THAN 8
02619 198600 DISPLAY 'SAVE-SUB-01 = ' SAVE-SUB-01
02620 198700 MOVE 1 TO SS
02621 198800 GO TO OP-HEADERS.
02622 198900 SEARCH-OP-B.
02623 199000 IF OP GREATER THAN 42
02624 199100 MOVE 1 TO OP
02625 199200 ADD 1 TO SS
02626 199300 GO TO SEARCH-OP-A.
02627 199400*

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02628 199500***** SEE IF SUBSCRIPT HAS ALREADY BEEN USED
02629 199600*
02630 199700 PERFORM BEGIN-SUB-SEARCH THRU END-SUB-SEARCH.
02631 199800 IF FOUND-WORD = '1'
02632 199900 ADD 1 TO OP
02633 200000 GO TO SEARCH-OP-B.
02634 200100 IF OP-PH-04 (OP, 5) IS GREATER THAN OP-PH-HOLD
02635 200200 OR EQUAL TO OP-PH-HOLD
02636 200300 MOVE OP-PH-04 (OP, 5) TO OP-PH-HOLD
02637 200400 IF OP-PH-HOLD = ZERO
02638 200500 MOVE 99 TO SAVE-SUB (SS) ELSE
02639 200600 MOVE OP TO SAVE-SUB (SS).
02640 200700 ADD 1 TO OP.
02641 200800 GO TO SEARCH-OP-B.
02642 200900 OP-HEADERS.
02643 201000 MOVE SPACES TO MINOR-P1 (SS).
02644 201100 MOVE '1' TO READER-SWITCH.
02645 201200 MOVE SPACES TO PAGE-2-03D (SS).
02646 201300 MOVE SAVE-SUB (SS) TO SSS.
02647 201400 IF NOT (SSS = 99 OR ZERO)
02648 201500 MOVE SPACES TO HD-KEY
02649 201600 MOVE 014651 TO CCC
02650 201700 MOVE OP-PH (SSS) TO CODE2
02651 201800 PERFORM READER THRU REXIT
02652 201900 MOVE HDER TO MINOR-P1 (SS).
02653 202000 MOVE SS TO MP-NO (SS).
02654 202100 MOVE ' ' TO PERIOD-04 (SS).
02655 202200 IF SSS = 99 OR ZERO NEXT SENTENCE ELSE
02656 202300 SUBTRACT OP-PH-04 (SSS, 5) FROM OP-PH-04 (43, 5)
02657 202400 SUBTRACT OP-PH-04 (SSS, 1) FROM OP-PH-04 (43, 1)
02658 202500 SUBTRACT OP-PH-04 (SSS, 2) FROM OP-PH-04 (43, 2)
02659 202600 SUBTRACT OP-PH-04 (SSS, 3) FROM OP-PH-04 (43, 3)
02660 202700 SUBTRACT OP-PH-04 (SSS, 4) FROM OP-PH-04 (43, 4)
02661 202800 MOVE OP-PH-04 (SSS, 5) TO TOT-ACC-MP (SS)
02662 202900 MOVE OP-PH-04 (SSS, 1) TO FAT-INJ-MP (SS)
02663 203000 MOVE OP-PH-04 (SSS, 2) TO SER-INJ-MP (SS)
02664 203100 MOVE OP-PH-04 (SSS, 3) TO MIN-INJ-MP (SS)
02665 203200 MOVE OP-PH-04 (SSS, 4) TO NON-INJ-MP (SS).
02666 203300 ADD 1 TO SS.
02667 203400 IF SS GREATER THAN 8 NEXT SENTENCE ELSE
02668 203500 GO TO OP-HEADERS.
02669 203600 MOVE SPACES TO PAGE-2-03D (9).
02670 204300 MOVE 09 TO MP-NO (9).
02671 204400 MOVE ' ' TO PERIOD-04 (9).
02672 204500 MOVE 'OTHERS' TO MINOR-P1 (9).
02673 204600 MOVE OP-PH-04 (43, 5) TO TOT-ACC-MP (9).
02674 204700 MOVE OP-PH-04 (43, 1) TO FAT-INJ-MP (9).
02675 204800 MOVE OP-PH-04 (43, 2) TO SER-INJ-MP (9).
02676 204900 MOVE OP-PH-04 (43, 3) TO MIN-INJ-MP (9).
02677 205000 MOVE OP-PH-04 (43, 4) TO NON-INJ-MP (9).
02678 205900*
02679 206000***** SEARCH TYPE HEADERS FOR 6 HIGHEST
02680 206100*
02681 206200 MOVE ZERO TO SAVE-SUB-01.
02682 206300 MOVE 1 TO SS.
02683 206400 MOVE 1 TO OP.
02684 206500 MOVE ZERO TO SSS.
02685 206600 SEARCH-TYP-A.
02686 206700 MOVE TYP-TOT (1, 5) TO TYP-HOLD.
02687 206800 IF SS GREATER THAN 6
02688 206900 MOVE 1 TO SS
02689 207000 DISPLAY 'SAVE-SUB-01-TYPS ' SAVE-SUB-01
02690 207100 GO TO TYP-HEADERS.
02691 207200 SEARCH-TYP-B.
02692 207300 IF OP GREATER THAN 22
02693 207400 MOVE 1 TO OP
02694 207500 ADD 1 TO SS
02695 207600 GO TO SEARCH-TYP-A.
02696 207700 PERFORM BEGIN-SUB-SEARCH THRU END-SUB-SEARCH.
02697 207800 IF FOUND-WORD = '1'
02698 207900 ADD 1 TO OP
02699 208000 GO TO SEARCH-TYP-B.
02700 208100 IF TYP-TOT (OP, 5) IS GREATER THAN TYP-HOLD OR = TYP-HOLD

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02701 208200      MOVE TYP-TOT (OP, 5) TO TYP-HOLD
02702 208300      IF TYP-HOLD = ZERO
02703 208400          MOVE 99 TO SAVE-SUB (SS) ELSE
02704 208500          MOVE OP TO SAVE-SUB (SS).
02705 208600      ADD 1 TO OP.
02706 208700      GO TO SEARCH-TYP-8.
02707 208800      TYP-HEADERS.
02708 208900          MOVE SPACES TO TYP-DESC (SS).
02709 209000          MOVE SPACES TO PAGE-2-03DA (SS).
02710 209100          MOVE SAVE-SUB (SS) TO SSS.
02711 209200          IF NOT (SSS = 99 OR ZERO)
02712 209300              MOVE SPACES TO HD-KEY
02713 209400              MOVE 014447 TO CCC
02714 209500              MOVE TYP-OP (SSS) TO CHAR2
02715 209600              PERFORM READER THRU REXIT
02716 209700              MOVE HDR TO TYP-DESC (SS).
02717 209800              MOVE SS TO TYP-NO (SS).
02718 209900              MOVE ' ' TO PERIODT-04 (SS).
02719 210000              IF SSS = 99 OR ZERO NEXT SENTENCE ELSE
02720 210100                  SUBTRACT TYP-TOT (SSS, 5) FROM TYP-TOT (23, 5)
02721 210200                  SUBTRACT TYP-TOT (SSS, 1) FROM TYP-TOT (23, 1)
02722 210300                  SUBTRACT TYP-TOT (SSS, 2) FROM TYP-TOT (23, 2)
02723 210400                  SUBTRACT TYP-TOT (SSS, 3) FROM TYP-TOT (23, 3)
02724 210500                  SUBTRACT TYP-TOT (SSS, 4) FROM TYP-TOT (23, 4)
02725 210600                  MOVE TYP-TOT (SSS, 5) TO TOT-ACC-TYP (SS)
02726 210700                  MOVE TYP-TOT (SSS, 1) TO FAT-INJ-TYP (SS)
02727 210800                  MOVE TYP-TOT (SSS, 2) TO SER-INJ-TYP (SS)
02728 210900                  MOVE TYP-TOT (SSS, 3) TO MIN-INJ-TYP (SS)
02729 211000                  MOVE TYP-TOT (SSS, 4) TO NON-INJ-TYP (SS).
02730 211100      ADD 1 TO SS.
02731 211200      IF SS GREATER THAN 6 NEXT SENTENCE ELSE
02732 211300          GO TO TYP-HEADERS.
02733 211400          MOVE SPACES TO PAGE-2-03DA (7).
02734 211500          MOVE SPACES TO PAGE-2-03DA (8).
02735 211600          SUBTRACT TYP-TOT (22, 5) FROM TYP-TOT (23, 5).
02736 211700          SUBTRACT TYP-TOT (22, 1) FROM TYP-TOT (23, 1).
02737 211800          SUBTRACT TYP-TOT (22, 2) FROM TYP-TOT (23, 2).
02738 211900          SUBTRACT TYP-TOT (22, 3) FROM TYP-TOT (23, 3).
02739 212000          SUBTRACT TYP-TOT (22, 4) FROM TYP-TOT (23, 4).
02740 212100          MOVE 07 TO TYP-NO (7).
02741 212200          MOVE ' ' TO PERIODT-04 (7).
02742 212300          MOVE 'OTHERS' TO TYP-DESC (7).
02743 212400          MOVE TYP-TOT (23, 5) TO TOT-ACC-TYP (7).
02744 212500          MOVE TYP-TOT (23, 1) TO FAT-INJ-TYP (7).
02745 212600          MOVE TYP-TOT (23, 2) TO SER-INJ-TYP (7).
02746 212700          MOVE TYP-TOT (23, 3) TO MIN-INJ-TYP (7).
02747 212800          MOVE TYP-TOT (23, 4) TO NON-INJ-TYP (7).
02748 212900          MOVE 8 TO TYP-NO (8).
02749 213000          MOVE ' ' TO PERIODT-04 (8).
02750 213100          MOVE 'NOT REPORTED' TO TYP-DESC (8).
02751 213200          MOVE TYP-TOT (22, 5) TO TOT-ACC-TYP (8).
02752 213300          MOVE TYP-TOT (22, 1) TO FAT-INJ-TYP (8).
02753 213400          MOVE TYP-TOT (22, 2) TO SER-INJ-TYP (8).
02754 213500          MOVE TYP-TOT (22, 3) TO MIN-INJ-TYP (8).
02755 213600          MOVE TYP-TOT (22, 4) TO NON-INJ-TYP (8).
02756 213700          PERFORM PAGE-2-P THRU END-PG-2 UNTIL D = 34.
02757 213800      END-PAGE-2.
02758 213900      PERFORM SKIP-TO-HEAD.
02759 214000*
02760 214100***** LOAD PAGE 3 OCCUPANT INJURY TABLE.
02761 214200*
02762 214300      PERFORM LOAD-PG-3 THRU END-LOAD-3
02763 214400          VARYING S-INDEX FROM 1 BY 1
02764 214500          UNTIL S-INDEX GREATER THAN 5
02765 214600          AFTER SERIOUS-INDEX FROM 1 BY 1
02766 214700          UNTIL SERIOUS-INDEX GREATER THAN 1.
02767 214800          MOVE 'EXTREME' TO SEV-NAME (1).
02768 214900          MOVE 'SEVERE' TO SEV-NAME (2).
02769 215000          MOVE 'MODERATE' TO SEV-NAME (3).
02770 215100          MOVE 'MINOR' TO SEV-NAME (4).
02771 215200          MOVE 'NONE' TO SEV-NAME (5).
02772 215300          MOVE TOT-ACC-ANG TO TOT-IMPACT.
02773 215400          MOVE TOT-ACC-VEL TO VEL-IMP.

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02774 215500 MOVE TOT-ACC-DIST TO STOP-DIST.
02775 215600 PERFORM PAGE-3-P THRU END-PG-3 UNTIL D = 25.
02776 215700 PERFORM SKIP-TO-HEAD.
02777 215800 END-PAGE-3.
02778 215900*
02779 216000***** LOAD PAGE 4
02780 216100*
02781 216200 MOVE TOT-ST-ACC TO SEAT-FAIL-ACC.
02782 216300 MOVE TOT-ST-FAIL TO SEAT-FAIL.
02783 216400 MOVE TOT-STBLT-ACC TO SEAT-BELT-ACC.
02784 216500 MOVE TOT-STBLT-FAIL TO SEAT-BELT-FAIL.
02785 216600 MOVE S-H-USED TO SH-HARN-USED.
02786 216700 MOVE S-H-FAILED TO SH-HARN-FAIL.
02787 216800 MOVE HELMET-USED TO CRASH-HEL-USED.
02788 216900 MOVE HELMET-UNUSED TO CRASH-HEL-UNUSED.
02789 217000*
02790 217100***** LOAD PAGE 4 TERRAIN TYPE TABLE
02791 217200*
02792 217300 LOAD-4.
02793 217400 PERFORM LOAD-PG-4 THRU END-LOAD-4 VARYING TERRAIN-INDEX
02794 217500 FROM 1 BY 1 UNTIL TERRAIN-INDEX GREATER THAN 13.
02795 217600 MOVE SPACES TO PAGE-4-WORK.
02796 217700 MOVE 1 TO ITER-4.
02797 217800 MOVE PCT-TER (1) TO PCT-HOLD.
02798 217900 MOVE ZERO TO TER-IND.
02799 218000 PERFORM SORT-PG-4 THRU END-SORT.
02800 218100 LOAD-4-A.
02801 218200 PERFORM PAGE-4-P THRU END-PG-4 UNTIL D = 29.
02802 218300 PERFORM SKIP-TO-HEAD.
02803 218400 END-PAGE-4. EXIT.
02804 218500*
02805 218600*
02806 218700***** PRINT PAGE 5
02807 218800***** PRINT CAUSE/FACTOR SUMMARIES.
02808 218900*
02809 219000 LOAD-5.
02810 219100 MOVE 1 TO C-INITIAL.
02811 219200 MOVE ZERO TO C-SAVE-01.
02812 219300 MOVE PAGE-5 (1) TO P-WORK-02B.
02813 219400 WRITE P-REC FROM P-WORK AFTER POSITIONING 3.
02814 219500 MOVE PAGE-5 (2) TO P-WORK-02B.
02815 219600 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02816 219700 MOVE PAGE-5 (3) TO P-WORK-02B.
02817 219800 WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
02818 219900 MOVE PAGE-5 (5) TO P-WORK-02B.
02819 220000 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02820 220100 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
02821 220200 MOVE 4 TO C-SV-LIMIT.
02822 220300*
02823 220400***** PRINT PILOT SUMMARY
02824 220500*
02825 220600 MOVE ZERO TO C-SAVE.
02826 220700 PERFORM SEARCH-FACTOR THRU END-FACTOR.
02827 220800*
02828 220900***** PRINT COPILOT SUMMARY
02829 221000*
02830 221100 DISPLAY 'C-HI ' C-HI 'C-INITIAL ' C-INITIAL.
02831 221200 MOVE C-HI TO C-INITIAL.
02832 221300 MOVE PAGE-5 (6) TO P-WORK-02B.
02833 221400 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02834 221500 MOVE ZERO TO C-SAVE-01.
02835 221600 MOVE 2 TO C-SV-LIMIT.
02836 221700 MOVE ZERO TO C-SAVE.
02837 221800 PERFORM SEARCH-FACTOR THRU END-FACTOR.
02838 221900*
02839 222000***** PRINT DUAL STUDENT SUMMARY
02840 222100*
02841 222200 DISPLAY 'C-HI ' C-HI 'C-INITIAL ' C-INITIAL.
02842 222300 MOVE C-HI TO C-INITIAL.
02843 222400 MOVE PAGE-5 (7) TO P-WORK-02B.
02844 222500 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02845 222600 MOVE ZERO TO C-SAVE-01.
02846 222700 MOVE C-HI TO C-INITIAL.

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02847 222800 MOVE ZERO TO C-SAVE.
02848 222900 PERFORM SEARCH-FACTOR THRU END-FACTOR.
02849 223000*
02850 223100***** PRINT CHECK PILOT SUMMARY
02851 223200*
02852 223300 DISPLAY 'C-HI ' C-HI 'C-INITIAL ' C-INITIAL.
02853 223400 MOVE C-HI TO C-INITIAL.
02854 223500 MOVE PAGE-5 (8) TO P-WORK-028.
02855 223600 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02856 223700 MOVE C-HI TO C-INITIAL.
02857 223800 MOVE ZERO TO C-SAVE-01.
02858 223900 MOVE ZERO TO C-SAVE.
02859 224000 PERFORM SEARCH-FACTOR THRU END-FACTOR.
02860 224100*
02861 224200***** PRINT AIRFRAME SUMMARY
02862 224300*
02863 224400 DISPLAY 'C-HI ' C-HI 'C-INITIAL ' C-INITIAL.
02864 224500 MOVE C-HI TO C-INITIAL.
02865 224600 MOVE PAGE-5 (9) TO P-WORK-028.
02866 224700 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02867 224800 MOVE C-HI TO C-INITIAL.
02868 224900 MOVE ZERO TO C-SAVE-01.
02869 225000 MOVE ZERO TO C-SAVE.
02870 225100 PERFORM SEARCH-FACTOR THRU END-FACTOR.
02871 225200*
02872 225300***** PRINT MISC ACTS & CONDITIONS SUMMARY
02873 225400*
02874 225500 DISPLAY 'C-HI ' C-HI 'C-INITIAL ' C-INITIAL.
02875 225600 MOVE C-HI TO C-INITIAL.
02876 225700 MOVE 4 TO C-SV-LIMIT.
02877 225800 MOVE PAGE-5 (10) TO P-WORK-028.
02878 225900 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
02879 226000 MOVE C-HI TO C-INITIAL.
02880 226100 MOVE ZERO TO C-SAVE-01.
02881 226200 MOVE ZERO TO C-SAVE.
02882 226300 PERFORM SEARCH-FACTOR THRU END-FACTOR.
02883 226400 END-PAGE-5. EXIT.
02884 226500 EQJ.
02885 226600*
02886 226700***** PRINT GRAND TOTAL SUMMARIES
02887 226800*
02888 226900*****
02889 227000*
02890 227100*
02891 227200 MOVE *
02892 227300- 'D TOTAL ACCIDENT SUMMARY * * * * * TO SUMMARY-HEAD-1. GRAN
02893 227400 PERFORM PRINT-SUMMARY.
02894 227500 MOVE 'ALL' TO PAGE-1-MAKE.
02895 227600 MOVE 'ALL' TO PAGE-1-MOD.
02896 227700 MOVE GTOT-AC TO PG-1-TOTA.
02897 227710 MOVE GTOT-AC-TYPE TO PG-1-TOTAB.
02898 227800 MOVE GTOT-OCC TO PG-1-TOTB.
02899 227900 MOVE GAVG-OCC TO PG-1-TOTC.
02900 228000 MOVE GTOT-FAT TO PG-1-TOTD.
02901 228100 MOVE GTOT-SER TO PG-1-TOTE.
02902 228200 MOVE GTOT-MNR TO PG-1-TOTF.
02903 228300 MOVE GTOT-NON TO PG-1-TOTH.
02904 228400 MOVE G-PG-1 (1, 1) TO PG-1-TOTI.
02905 228500 MOVE G-PG-1 (1, 2) TO PG-1-TOTJ.
02906 228600 MOVE G-PG-1 (1, 3) TO PG-1-TOTK.
02907 228700 MOVE G-PG-1 (1, 4) TO PG-1-TOTL.
02908 228800 MOVE G-PG-1 (2, 1) TO PG-1-TOTM.
02909 228900 MOVE G-PG-1 (2, 2) TO PG-1-TOTN.
02910 229000 MOVE G-PG-1 (2, 3) TO PG-1-TOTP.
02911 229100 MOVE G-PG-1 (2, 4) TO PG-1-TOTQ.
02912 229200 MOVE G-PG-1 (3, 1) TO PG-1-TOTR.
02913 229300 MOVE G-PG-1 (3, 2) TO PG-1-TOTS.
02914 229400 MOVE G-PG-1 (3, 3) TO PG-1-TOTT.
02915 229500 MOVE G-PG-1 (3, 4) TO PG-1-TOTU.
02916 229600 MOVE G-PG-1 (4, 1) TO PG-1-TOTV.
02917 229700 MOVE G-PG-1 (4, 2) TO PG-1-TOTW.
02918 229800 MOVE G-PG-1 (4, 3) TO PG-1-TOTX.
02919 229900 MOVE G-PG-1 (4, 4) TO PG-1-TOTY.

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02920 230000 PERFORM PAGE-1-P THRU END-PG-1 UNTIL D = 24.
02921 230100*
02922 230200***** FILL AND PRINT PG 2 GRAND TOTAL
02923 230300*
02924 230400 MOVE GTOT-T-O TO PG-2-TO.
02925 230500 MOVE GTOT-FLY TO PG-2-IF.
02926 230600 MOVE GTOT-LOG TO PG-2-LOG.
02927 230700 MOVE GFAT-TU TO PG-2-TOFAT.
02928 230800 MOVE GFAT-INFLT TO PG-2-IFFAT.
02929 230900 MOVE GFAT-LOG TO PG-2-LOGFAT.
02930 231000 MOVE GTOT-TS TO PG-2-OTHER.
02931 231100 MOVE GFAT-TS TO PG-2-OTHERFAT.
02932 231200 MOVE GTOT-NR TO PG-2-NR.
02933 231300 MOVE GFAT-NR TO PG-2-NRAT.
02934 231400 MOVE ZERO TO SAVE-SUB-01.
02935 231500 MOVE 1 TO SS.
02936 231600 MOVE ZERO TO SSS.
02937 231700 MOVE 1 TO OP.
02938 231800 MOVE GTOT-TYP-01 TO TYP-TOT-01.
02939 231900 MOVE GTOT-OP-01 TO OP-PH-TOT.
02940 232000 PERFORM SKIP-TO-HEAD.
02941 232100 PERFORM SEARCH-OP-A THRU TYP-HEADERS.
02942 232200*
02943 232300***** FILL AND PRINT PG 3 GRAND TOTALS
02944 232400*
02945 232500 MOVE G-ANG-15 TO ANGLE-15.
02946 232600 MOVE G-ANG-30 TO ANGLE-30.
02947 232700 MOVE G-ANG-45 TO ANGLE-45.
02948 232800 MOVE G-ANG-60 TO ANGLE-60.
02949 232900 MOVE G-ANG-75 TO ANGLE-75.
02950 233000 MOVE G-ANG-90 TO ANGLE-90.
02951 233100 MOVE G-ANG-90-PLUS TO ANGLE-90-PLUS.
02952 233200 MOVE G-VEL-30 TO VEL-30.
02953 233300 MOVE G-VEL-60 TO VEL-60.
02954 233400 MOVE G-VEL-90 TO VEL-90.
02955 233500 MOVE G-VEL-120 TO VEL-120.
02956 233600 MOVE G-VEL-120-PLUS TO VEL-120-PLUS.
02957 233700 MOVE G-DIST-10 TO DIST-10.
02958 233800 MOVE G-DIST-20 TO DIST-20.
02959 233900 MOVE G-DIST-30 TO DIST-30.
02960 234000 MOVE G-DIST-40 TO DIST-40.
02961 234100 MOVE G-DIST-50 TO DIST-50.
02962 234200 MOVE G-DIST-60 TO DIST-60.
02963 234300 MOVE G-DIST-60-PLUS TO DIST-60-PLUS.
02964 234400 MOVE G-SERIOUS TO SERIOUSNESS.
02965 234500 MOVE GTOT-ACC-ANG TO TOT-ACC-ANG.
02966 234600 MOVE GTOT-ACC-VEL TO TOT-ACC-VEL.
02967 234700 MOVE GTOT-ACC-DIST TO TOT-ACC-DIST.
02968 234800 MOVE G-AVG-ANGLE TO AVG-ANGLE.
02969 234900 MOVE G-AVG-VEL TO AVG-VEL.
02970 235000 MOVE G-AVG-DIST TO AVG-DIST.
02971 235100 PERFORM END-PAGE-2.
02972 235200*
02973 235300***** FILL AND PRINT PG 4 GRAND TOTALS
02974 235400*
02975 235500 MOVE GTOT-ST-ACC TO SEAT-FAIL-ACC.
02976 235600 MOVE GTOT-ST-FAIL TO SEAT-FAIL.
02977 235700 MOVE GTOT-STBLT-ACC TO SEAT-BELT-ACC.
02978 235800 MOVE GTOT-STBLT-FAIL TO SEAT-BELT-FAIL.
02979 235900 MOVE GS-H-USED TO SH-HARN-USED.
02980 236000 MOVE GS-H-FAILED TO SH-HARN-FAIL.
02981 236100 MOVE GHCL-USED TO CRASH-HCL-USED.
02982 236200 MOVE GHCL-UNUSED TO CRASH-HCL-UNUSED.
02983 236300 MOVE GTOT-AC-TYPE TO TOT-AC-TYPE.
02984 236400 MOVE GTERRAIN-01 TO TERRAIN-001.
02985 236500 PERFORM LOAD-4 THRU END-PAGE-4.
02986 236600*
02987 236700***** LOAD AND PRINT PAGE 5 GRAND TOTALS
02988 236800*
02989 236900 MOVE ' CAUSE / FACTOR GRAND SUMM
02990 237000- 'ARY' TO P-REC.
02991 237100 WRITE P-REC AFTER POSITIONING 2.
02992 237200 MOVE G-CAUSE-01 TO CAUSE-01.

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02993 237300 MOVE G-CAUSE-FAT-01 TO CAUSE-FATAL-01.
02994 237400 MOVE G-CAUSE-NONFAT-01 TO CAUSE-NONFAT-01.
02995 237500 MOVE ZERO TO C-SAVE-01.
02996 237600 MOVE ZERO TO CAUSE-77.
02997 237700 PERFORM LOAD-5 THRU END-PAGE-5.
02998 237800 CLOSE HEAD PRT.
02999 237900 STOP RUN.
03000 238000 UNIQUE.
03001 238100 MOVE ZERO TO INJ2.
03002 238200 IF F08001A (INJ1) = SPACES
03003 238300 ADD 1 TO D, INJ1
03004 238400 GO TO END-UNIQUE.
03005 238500 TRANS-INJURY.
03006 238600 ADD 1 TO INJ2.
03007 238700 IF INJ2 GREATER THAN 6 GO TO AFTER-TRANS.
03008 238800 EXAMINE F0800101A (INJ1, INJ2) REPLACING LEADING ZEROS
03009 238900 BY SPACES.
03010 239000 GO TO TRANS-INJURY.
03011 239100 AFTER-TRANS.
03012 239200 MOVE F08001A (INJ1) TO FDATA.
03013 239300 PERFORM MOVE-DIRECT.
03014 239400 ADD 1 TO D, INJ1.
03015 239500 END-UNIQUE. EXIT.
03016 239600 READER.
03017 239700 MULTIPLY KYB BY KYB GIVING SUM-A.
03018 239800 ADD KYA TO SUM-A.
03019 239900 DIVIDE SUM-A BY 2999 GIVING DIVIDEND-HOLD
03020 240000 REMAINDER DIVIDE-HOLD.
03021 240100 DIVIDE DIVIDE-HOLD BY 32 GIVING TRACK-ID.
03022 240200 MOVE CCC TO KYF.
03023 240300 MOVE CODE4 TO KYG.
03024 240400 READER-X.
03025 240500 READ HEAD INVALID KEY MOVE HD-KEY TO ERR
03026 240600 DISPLAY 'HD-KEY ERROR = ', ERR
03027 240700 MOVE ERR-RT TO HD GO TO REXIT.
03028 240800 MOVE HDER TO FDATA.
03029 240900 IF READER-SWITCH = '1' GO TO REXIT.
03030 241000 BUILD-LINE.
03031 241100 PERFORM MOVE-DIRECT.
03032 241200*
03033 241300***** HEAD-COUNT UNEQUAL TO 1 OR 0 SUPPRESSES TH DESCRIPTION
03034 241400***** PREVIOUSLY TAKEN FROM TABLE. MAKE SURE IT IS SET TO PROP
03035 241500***** VALUE BEFORE PERFORMING THIS ROUTINE.
03036 241600*
03037 241700 IF NOT (HEAD-COUNT = 1 OR 0)
03038 241800 MOVE SPACES TO DESCRIPTION.
03039 241900 REXIT. EXIT.
03040 242000 SEVERITY-TEST.
03041 242100 IF SEV (SEVERITY-INDEX) IS = F13705
03042 242200 GO TO PERFORM-SERIOUS.
03043 242300 END-SEVERITY. EXIT.
03044 242400 SERIOUS-TEST.
03045 242500 SET S-INDEX TO SEVERITY-INDEX.
03046 242600 SET GS-INDEX TO S-INDEX.
03047 242700 SET GSERIOUS-INDEX TO SERIOUS-INDEX.
03048 242800 SET SER-IND TO SERIOUS-INDEX.
03049 242900 MOVE F0800101B (3, 1, SER-IND) TO INJURY.
03050 243000 IF INJURY NOT = ZEROS AND INJURY IS NUMERIC
03051 243100 ADD INJURY TO GS (GS-INDEX, GSERIOUS-INDEX)
03052 243200 ADD INJURY TO S (S-INDEX, SERIOUS-INDEX).
03053 243300 END-SERIOUS. EXIT.
03054 243400 TERRAIN-A.
03055 243500 MOVE SPACES TO DUMBO.
03056 243600 END-TERRAIN. EXIT.
03057 243700 C-F-PRINT.
03058 243800 IF F078 (CFF) = SPACES OR (F07801 (CFF) = '84' AND
03059 243900 F0780302 (CFF) = 'J') NEXT SENTENCE ELSE
03060 244000 ADD 1 TO HEAD-COUNT
03061 244100 MOVE SPACES TO HD-KEY
03062 244200 MOVE 061766 TO CCC
03063 244300 MOVE F07801 (CFF) TO HOLD-KEY-1
03064 244400 MOVE F07803 (CFF) TO HOLD-KEY-2
03065 244500 MOVE HOLD-KEY TO CODE4

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03066 244600 MOVE '0' TO READER-SWITCH.
03067 244700 PERFORM READER THRU REXIT.
03068 244800 ADD 1 TO D.
03069 244900 ADD 1 TO CFF.
03070 245000 C-F-EXIT. EXIT.
03071 245100 MOVE-DIRECT.
03072 245200 MOVE DESC (D) TO DESCRIPTION.
03073 245300 MOVE FDATA TO DATAA.
03074 245400 WRITE P-REC FROM P-WORK AFTER POSITIONING 1 EOP
03075 245500 MOVE SPACES TO P-REC
03076 245600 WRITE P-REC AFTER POSITIONING 0
03077 245700 WRITE P-REC AFTER POSITIONING 3.
03078 245800 END-DIRECT. EXIT.
03079 245900 UP-SEARCH.
03080 246000 MOVE ZERO TO LO.
03081 246100 MOVE HISAVE TO HI.
03082 246200 AB. COMPUTE I = (HI + LO) / 2.
03083 246300 IF SEARCH-CODE LESS THAN OP-PH (I)
03084 246400 MOVE I TO HI
03085 246500 GO TO BA.
03086 246600 IF SEARCH-CODE GREATER THAN OP-PH (I)
03087 246700 MOVE I TO LO
03088 246800 GO TO BA.
03089 246900 MOVE '1' TO FOUND-WORD.
03090 247000 GO TO END-OP.
03091 247100 BA. IF I LESS THAN (HI - LO) GO TO AB.
03092 247200 END-OP. EXIT.
03093 247300*
03094 247400***** I IS DEFINED IN OP-SEARCH
03095 247500***** OP IS DEFINED IN LOAD-ARRAY
03096 247600*
03097 247700 SERIOUS-B.
03098 247800 MOVE F08001018 (3,1,OP) TO INJ-01.
03099 247900 IF INJURY NOT = ZERO AND INJURY IS NUMERIC
03100 248000 ADD INJURY TO OP-PH-04 (43, OP)
03101 248100 ADD INJURY TO GTOT-OP (43, OP)
03102 248200 ADD INJURY TO GTOT-OP (1, OP)
03103 248300 ADD INJURY TO OP-PH-04 (1, OP).
03104 248400 IF INJURY NOT = ZERO AND INJURY IS NUMERIC AND
03105 248500 BEEN-THERE = '0'
03106 248600 ADD 1 TO OP-PH-04 (43, 5)
03107 248700 ADD 1 TO GTOT-OP (43, 5)
03108 248800 ADD 1 TO GTOT-OP (1, 5)
03109 248900 ADD 1 TO OP-PH-04 (1, 5)
03110 249000 MOVE '1' TO BEEN-THERE.
03111 249100 DISPLAY 'SERIOUS-B 'INJURY = ' INJURY.
03112 249200 END-SERIOUS-B. EXIT.
03113 249300 TYPE-SEARCH.
03114 249400 MOVE ZERO TO LO.
03115 249500 MOVE HISAVE TO HI.
03116 249600 AC. COMPUTE I = (HI + LO) / 2.
03117 249700 IF SEARCH-TYPE LESS THAN TYP-OP (I)
03118 249800 MOVE I TO HI
03119 249900 GO TO CA.
03120 250000 IF SEARCH-TYPE GREATER THAN TYP-OP (I)
03121 250100 MOVE I TO LO
03122 250200 GO TO CA.
03123 250300 MOVE '1' TO FOUND-WORD.
03124 250400 GO TO END-TYPE.
03125 250500 CA. IF I LESS THAN (HI - LO) GO TO AC.
03126 250600 END-TYPE. EXIT.
03127 250700*
03128 250800***** I IS DEFINED IN TYPE-SEARCH
03129 250900***** OP IS DEFINED IN COLLECT-TYPES
03130 251000*
03131 251100 TYPE-COLLECT.
03132 251200 MOVE F08001018 (3,1,OP) TO INJ-01.
03133 251300 TRANSFORM INJ-01 FROM SPACES TO ZEROS.
03134 251400 IF INJURY NOT = ZERO AND INJURY IS NUMERIC
03135 251500 ADD INJURY TO GTOT-TYP (23, OP)
03136 251600 ADD INJURY TO TYP-TOT (23, OP)
03137 251700 ADD INJURY TO GTOT-TYP (1, OP)
03138 251800 ADD INJURY TO TYP-TOT (1, OP).

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03139 251900 IF INJURY NOT = ZERO AND INJURY IS NUMERIC AND
03140 252000 BEEN-THERE = '0'
03141 252100 ADD 1 TO GTOT-TYP (23, 5)
03142 252200 ADD 1 TO TYP-TOT (23, 5)
03143 252300 ADD 1 TO GTOT-TYP (1, 5)
03144 252400 ADD 1 TO TYP-TOT (1, 5)
03145 252500 MOVE '1' TO BEEN-THERE.
03146 252600 END-COLLECT. EXIT.
03147 252700 C-F-SEARCH.
03148 252800 MOVE 487 TO HISAVE.
03149 252900 IF F078 (CFF) = SPACES GO TO PRE-END-CF.
03150 253000 IF F07801 (CFF) = '64' OR '65' OR '66' OR '67' OR '70' OR
03151 253100 '88'
03152 253200 DISPLAY 'CFF = ' CFF ' F07801 = ' F07801 (CFF)
03153 253300 MOVE F07801 (CFF) TO HOLD-KEY-1
03154 253400 MOVE F07803 (CFF) TO HOLD-KEY-2
03155 253500 PERFORM C-F-ACCESS THRU END-ACCESS
03156 253600 IF FOUND-WORD = '1'
03157 253700 ADD 1 TO CAUSE-492 (1)
03158 253800 ADD 1 TO G-CAUSE (1)
03159 253900 DISPLAY '1 = ' 1 ' CAUSE-492 = ' CAUSE-492 (1)
03160 254000 IF F08001018 (3,1,1) NOT = ZERO
03161 254100 ADD 1 TO G-CAUSE-FAT (1)
03162 254200 ADD 1 TO CAUSE-FATAL (1) ELSE
03163 254300 ADD 1 TO G-CAUSE-NONFAT (1)
03164 254400 ADD 1 TO CAUSE-NON-FAT (1).
03165 254500 PRE-END-CF.
03166 254600 MOVE '0' TO FOUND-WORD.
03167 254700 ADD 1 TO CFF.
03168 254800 END-CF-SEARCH. EXIT.
03169 254900
03170 255000 C-F-ACCESS.
03171 255100 MOVE ZERO TO LO.
03172 255200 MOVE HISAVE TO HI.
03173 255300 AD. COMPUTE 1 = (HI + LO) / 2.
03174 255400 IF HOLD-KEY LESS THAN CAUSE-FACTOR-02R (1)
03175 255500 MOVE 1 TO HI
03176 255600 GO TO DZ.
03177 255700 IF HOLD-KEY GREATER THAN CAUSE-FACTOR-02R (1)
03178 255800 MOVE 1 TO LO
03179 255900 GO TO DZ.
03180 256000 MOVE '1' TO FOUND-WORD.
03181 256100 GO TO END-ACCESS.
03182 256200 DZ. IF 1 LESS THAN (HI - LO) GO TO AD.
03183 256300 END-ACCESS. EXIT.
03184 256400 ***** SEARCH FATAL CAUSE FOR TWO OR FOUR LARGEST TOTALS
03185 256500*
03186 256600 SEARCH-FACTOR.
03187 256700 PERFORM SEARCH-SUB THRU END-SUB C-SV-LIMIT TIMES.
03188 256800 MOVE 1 TO C-SV.
03189 256900 MOVE 1 TO C-TEST.
03190 257000*
03191 257100***** OBTAIN THE ENGLISH MEANING HEADERS FOR A FACTOR
03192 257200*
03193 257300 WRITE-FACTOR.
03194 257400 MOVE SPACES TO CAUSE-FACTOR-5.
03195 257500 MOVE ZERO TO CF-FATALS CF-NONFAT.
03196 257600 MOVE '1' TO READER-SWITCH.
03197 257700 MOVE SPACES TO HD-KEY.
03198 257800 MOVE 061766 TO CCC.
03199 257900 IF C-SAVE-02 (C-SV) = ZERO
03200 258000 GO TO WRITE-FACTOR-TOTALS.
03201 258100 MOVE C-SAVE-02 (C-SV) TO C-SAVE.
03202 258200 IF NOT (CAUSE-FATAL (C-SAVE) = ZERO AND
03203 258300 CAUSE-NON-FAT (C-SAVE) = ZERO)
03204 258400 MOVE CAUSE-FACTOR-02R (C-SAVE) TO CODE4
03205 258500 PERFORM READER THRU REXIT
03206 258600 MOVE CAUSE-FATAL (C-SAVE) TO CF-FATALS
03207 258700 MOVE CAUSE-NON-FAT (C-SAVE) TO CF-NONFAT
03208 258800 MOVE HDER TO CAUSE-FACTOR-5.
03209 258900*
03210 259000***** WRITE FACTOR TOTALS
03211 259100*

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03212 259200 WRITE-FACTOR-TOTALS.
03213 259300 MOVE C-SV TO CF-NO.
03214 259400 MOVE PAGE-5 (4) TO P-WORK-028.
03215 259500 WRITE P-REC FROM P-WORK AFTER POSITIONING 2.
03216 259600 ADD 1 TO C-SV.
03217 259700 IF C-SV GREATER THAN C-SV-LIMIT
03218 259800 MOVE 1 TO C-SV
03219 259900 GO TO END-FACTOR.
03220 260000 GO TO WRITE-FACTOR.
03221 260100 END-FACTOR. EXIT.
03222 260200 SEARCH-SUB.
03223 260300 MOVE '0' TO FOUND-WORD.
03224 260400 MOVE C-INITIAL TO F.
03225 260500 MOVE ZERO TO C-SV.
03226 260600 ADD 1 TO C-SAVE.
03227 260700 MOVE CAUSE-FACTOR-02R (C-INITIAL) TO CAUSE-FACTOR-HOLD.
03228 260800 MOVE FACTOR-02 TO FACTOR-77.
03229 260900 MOVE CAUSE-492 (C-INITIAL) TO CAUSE-FACTOR-77.
03230 261000 PERFORM SEARCH-SUB-A THRU END-SEARCH-A
03231 261100 UNTIL FACTOR-02 NOT = FACTOR-77 OR F GREATER THAN 487.
03232 261200 DISPLAY ' C-SAVE-02-CF = ' C-SAVE-01.
03233 261300 END-SUB. EXIT.
03234 261400 SEARCH-SUB-A.
03235 261500 MOVE CAUSE-FACTOR-02R (F) TO CAUSE-FACTOR-HOLD.
03236 261600 IF FACTOR-02 NOT = FACTOR-77 GO TO END-SEARCH-A.
03237 261700 IF CAUSE-492 (F) GREATER THAN CAUSE-FACTOR-77 OR =
03238 261800 CAUSE-FACTOR-77
03239 261900 MOVE ZERO TO C-SV
03240 262000 PERFORM EXAM-SUB-F THRU END-EXAM
03241 262100 IF FOUND-WORD = '1'
03242 262200 MOVE '0' TO FOUND-WORD
03243 262300 ELSE
03244 262400 MOVE F TO C-SAVE-02 (C-SAVE)
03245 262500 MOVE CAUSE-492 (F) TO CAUSE-FACTOR-77.
03246 262600 ADD 1 TO F.
03247 262700 MOVE F TO C-HI.
03248 262800 END-SEARCH-A. EXIT.
03249 262900 EXAM-SUB-F.
03250 263000 ADD 1 TO C-SV.
03251 263100 IF C-SV GREATER THAN C-SV-LIMIT GO TO END-EXAM.
03252 263200 IF C-SAVE-02 (C-SV) = F
03253 263300 MOVE '1' TO FOUND-WORD
03254 263400 GO TO END-EXAM.
03255 263500 GO TO EXAM-SUB-F.
03256 263600 END-EXAM. EXIT.
03257 263700 PAGE-1-P.
03258 263800 ADD 1 TO D.
03259 263900 MOVE PAGE-1 (D) TO P-WORK-028.
03260 264000 WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
03261 264100 IF NOT (D = 11 OR 13 OR 15)
03262 264200 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03263 264300 END-PG-1. EXIT.
03264 264400 PAGE-2-P.
03265 264500 ADD 1 TO D.
03266 264600 MOVE PAGE-2 (D) TO P-WORK-028.
03267 264700 WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
03268 264800 IF D = 1 OR 3 OR 4 OR 5 OR 6 OR 7 OR 8 OR 10 OR 12 OR 21 OR
03269 264900 23 OR 25 OR 33
03270 265000 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03271 265100 END-PG-2. EXIT.
03272 265200 PAGE-3-P.
03273 265300 ADD 1 TO D.
03274 265400 IF D = 7
03275 265500 MOVE AVG-ANGLE TO AVG-ANGLE-3
03276 265600 MOVE ANGLE-15 TO F0-15
03277 265700 MOVE ANGLE-30 TO F16-30
03278 265800 MOVE ANGLE-45 TO F31-45
03279 265900 MOVE ANGLE-60 TO F46-60
03280 266000 MOVE ANGLE-75 TO F61-75
03281 266100 MOVE ANGLE-90 TO F76-90
03282 266200 MOVE ANGLE-90-PLUS TO F90.
03283 266300 IF D = 13
03284 266400 MOVE AVG-VEL TO AVG-ANGLE-3

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03285 266500 MOVE VEL-30 TO F0-15
03286 266600 MOVE VEL-60 TO F16-30
03287 266700 MOVE VEL-90 TO F31-45
03288 266800 MOVE VEL-120 TO F46-60
03289 266900 MOVE VEL-120-PLUS TO F61-75
03290 267000 MOVE ZERO TO F76-90 F90
03291 267100 MOVE PAGE-3 (7) TO P-WORK-02B
03292 267200 WRITE P-REC FROM P-WORK AFTER POSITIONING 1
03293 267300 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03294 267400 IF D = 18
03295 267500 MOVE AVG-DIST TO AVG-ANGLE-3
03296 267600 MOVE DIST-10 TO F0-15
03297 267700 MOVE DIST-20 TO F16-30
03298 267800 MOVE DIST-30 TO F31-45
03299 267900 MOVE DIST-40 TO F46-60
03300 268000 MOVE DIST-50 TO F61-75
03301 268100 MOVE DIST-60 TO F76-90
03302 268200 MOVE DIST-60-PLUS TO F90
03303 268300 MOVE PAGE-3 (7) TO P-WORK-02B
03304 268400 WRITE P-REC FROM P-WORK AFTER POSITIONING 1
03305 268500 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03306 268600 MOVE PAGE-3 (D) TO P-WORK-02B.
03307 268700 WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
03308 268800 IF D = 7
03309 268900 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03310 269000 IF NOT (D = 4 OR 5 OR 10 OR 11 OR 15 OR 16 OR 19)
03311 269100 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03312 269200 END-PG-3. EXIT.
03313 269300 PAGE-4-P.
03314 269400 ADD 1 TO D.
03315 269500 MOVE PAGE-4 (D) TO P-WORK-02B.
03316 269600 IF PAGE-4 (D) NOT = SPACES
03317 269700 WRITE P-REC FROM P-WORK AFTER POSITIONING 1.
03318 269800 IF NOT (D = 12 OR 13) AND PAGE-4 (D) NOT = SPACES
03319 269900 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 1.
03320 270000 END-PG-4. EXIT.
03321 270100 SKIP-TO-HEAD.
03322 270200 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 0.
03323 270300 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 3.
03324 270400 WRITE P-REC FROM SPACE-LINE AFTER POSITIONING 3.
03325 270500 MOVE ZERO TO D.
03326 270600 END-HEAD. EXIT.
03327 270700 BEGIN-SUB-SEARCH.
03328 270800 MOVE ZERO TO FOUND-WORD.
03329 270900 ADD 1 TO SSS.
03330 271000 IF SAVE-SUB (SSS) = ZERO
03331 271100 MOVE ZERO TO SSS
03332 271200 GO TO END-SUB-SEARCH.
03333 271300 IF OP = SAVE-SUB (SSS)
03334 271400 MOVE '1' TO FOUND-WORD
03335 271500 MOVE ZERO TO SSS
03336 271600 GO TO END-SUB-SEARCH.
03337 271700 GO TO BEGIN-SUB-SEARCH.
03338 271800 END-SUB-SEARCH. EXIT.
03339 271900 LOAD-PG-3.
03340 272000 SET SER-IND TO S-INDEX.
03341 272100 MOVE SPACES TO PAGE-3-031 (SER-IND).
03342 272200 MOVE S (S-INDEX, SERIOUS-INDEX) TO SEV-FAT (SER-IND).
03343 272300 MOVE S (S-INDEX, SERIOUS-INDEX + 1) TO
03344 272400 SEV-SER (SER-IND).
03345 272500 MOVE S (S-INDEX, SERIOUS-INDEX + 2) TO
03346 272600 SEV-MIN (SER-IND).
03347 272700 MOVE S (S-INDEX, SERIOUS-INDEX + 3) TO
03348 272800 SEV-NON (SER-IND).
03349 272900 END-LOAD-3. EXIT.
03350 273000 LOAD-PG-4.
03351 273100 MOVE SPACES TO HD-KEY.
03352 273200 MOVE 042222 TO CCC.
03353 273300 MOVE TERRAIN (TERRAIN-INDEX) TO CHAR1.
03354 273400 MOVE '1' TO READER-SWITCH.
03355 273500 PERFORM READER THRU REXIT.
03356 273600 SET TER-IND TO TERRAIN-INDEX.
03357 273700 MOVE SPACES TO PAGE-4-03H (TER-IND).

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03358 273800 MOVE HDER TO TERR-TYP (ITER-IND).
03359 273900 IF TOT-AC-TYPE NOT = ZERO
03360 274000 DIVIDE TERRAIN-COUNT (ITER-IND) BY TOT-AC-TYPE GIVING
03361 274100 PCNT-OCC ROUNDED ELSE MOVE ZERO TO PCNT-OCC.
03362 274200 MULTIPLY PCNT-OCC BY 100 GIVING PCNTT.
03363 274300 MOVE PCNTT TO PCT-TER (ITER-IND).
03364 274400 MOVE ZERO TO PCNT-OCC PCNTT.
03365 274500 END-LOAD-4. EXIT.
03366 274600 SORT-PG-4.
03367 274700 IF ITER-4 GREATER THAN 13
03368 274800 MOVE PAGE 4 WORK TO PAGE-4-03GROUP
03369 274900 GO TO END-SORT.
03370 275000 ADD 1 TO TER-IND.
03371 275100 IF TER-IND GREATER THAN 13
03372 275110 MOVE PCT-TER (1) TO PCT-HOLD
03373 275200 ADD 1 TO ITER-4
03374 275300 MOVE ZERO TO TER-IND
03375 275400 MOVE SPACES TO PAGE-4-03H (INDEX-HOLD)
03376 275500 GO TO SORT-PG-4.
03377 275600 IF PCT-TER (ITER-IND) = ZERO OR SPACES
03378 275700 MOVE SPACES TO PAGE-4-03H (ITER-IND).
03379 275800 IF PCT-TER (ITER-IND) GREATER THAN PCT-HOLD OR
03380 275810 PCT-TER (ITER-IND) = PCT-HOLD
03381 275900 MOVE PAGE-4-03H (ITER-IND) TO PAGE-4-WO2 (ITER-4)
03382 276000 MOVE TER-IND TO INDEX-HOLD
03383 276100 MOVE PCT-TER (ITER-IND) TO PCT-HOLD.
03384 276200 GO TO SORT-PG-4.
03385 276300 END-SORT. EXIT.
03386 276400 INITIALIZE-COUNTERS.
03387 276500 MOVE ZERO TO
03388 276600 J
03389 276700 TOT-FAT TOT-SER TOT-OCC TOT-MNR AV-OCC
03390 276800 REC-TOT-OCC HEAD-COUNT S-H-INSTALLED TOT-NON
03391 276900 S-H-FAILED HELMET-USED HELMET-UNUSED S-H-USED
03392 277000 TOT-ST-FAIL VEL-30 VEL-60 TOT-ACC-VEL TOT-ST-ACC
03393 277100 VEL-120 VEL-120-PLUS TOT-ACC-VEL VEL-90
03394 277200 AVG-VEL DIST-10 DIST-20 DIST-30 VEL-SUM
03395 277300 DIST-40 DIST-50 DIST-60 DIST-60-PLUS DIST-30
03396 277400 TOT-ACC-DIST DIST-SUM AVG-DIST TOT-STBLT-ACC
03397 277500 TOT-STBLT-FAIL ANGLE-15 ANGLE-30 ANGLE-45
03398 277600 ANGLE-60 ANGLE-75 ANGLE-90 ANGLE-90-PLUS
03399 277700 TOT-ACC-ANG ANGLE-SUM AVG-ANGLE TOT-T-D
03400 277800 TOT-FLY TOT-LDG UP UP-PH-TOT
03401 277900 TYP-TOT-01 CAUSE-01 CAUSE-FATAL-01 FAT-TO
03402 278000 CAUSE-NONFAT-01 PG-1-SERIOUS-01 FAT-INFLT FAT-LOG
03403 278100 TOT-ST-ACC TOT-ST-FAIL TERRAIN-001 SERIOUSNESS
03404 278200 TOT-NR TOT-TS FAT-TS FAT-NR
03405 278300 F INJ-01 C-SAVE-01 TOT-AC-TYPE
03406 278310 TALLY.
03407 278400 MOVE SPACES TO SAV-CARD.
03408 278500 MOVE 1 TO D.
03409 278600 END-INITIALIZE. EXIT.

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A.6 SAMPLE INPUT

011069NREDDING,CALIF P16FZ PA-28 2145 405124281206AAALAJAYA D
 870 23197 005718407R 06FZ VV 02000AR A 00210A ZA 25A
 FA AA A CA A A F 1 641364AC46136602JA 1
 1 2
 LT.FOLLOWED HWY INTO VALLEY WITH LC4 CLOUDS₂.NOT INST RECDN 1/13/69.LOST ON WTE F
 0 B C02 X AX D₂ 039 AKFH C609
 CAF

073159Z JUL81N128Y
BT - PFC PF
CA AA A BA AA A N I
010460 TOUTKEMAN,PA PIPER
CLEMENT AVIA BA A PA-30
PN GARVEY A 00278A
66C226413161J088X94
P INTRD SOLO FLT IN MULTI-ENG ACFT-DIV
FROM BAWY TO INST PANEL TO LOCATE FLAP CONTROL
01 000675
01 0023
026293038

073109Z 000100V05G	011509	NORTHROCK, ILL	PIPER	PA-30	1610	F13124291234AA213
EO A AFFICEP	SS	FLYVESKOL	BA 1	4	HA8832	000680AC D C02423
AA PA A GA GA A	N	1	6AC7080LBC	4	06000A	000007A 32A
1	2	2				1
			000446	F01000EK 33		130010
			02 103			
						CAF

[illegible]

A.7 SAMPLE OUTPUT

Typical individual airplane output data is shown in Figures 12 and 13. Typical grand summary data output is shown in Figure 13. Both Figures are contained in this report on pages 42 through 47.

A.8 DISCUSSION OF PROGRAM AND DATA TAPE

Data Processing Information

This tape is 9 track, unlabeled, blocked 3440 with 80 by 6 record length.

Tape layout

The content of this tape is as follows

Program MTSB0001

Program MTSB0002

Program 1325020D

NTSB record used in MTSB0001 and MTSB0002

Full Print Headers

Job Control to catalog and execute the system

The jobs are separated by one record with five (5) asterisks in column 1-5.
The tape was tested at Cessna by selection and printing 1325020D and the job control and not the remainder.

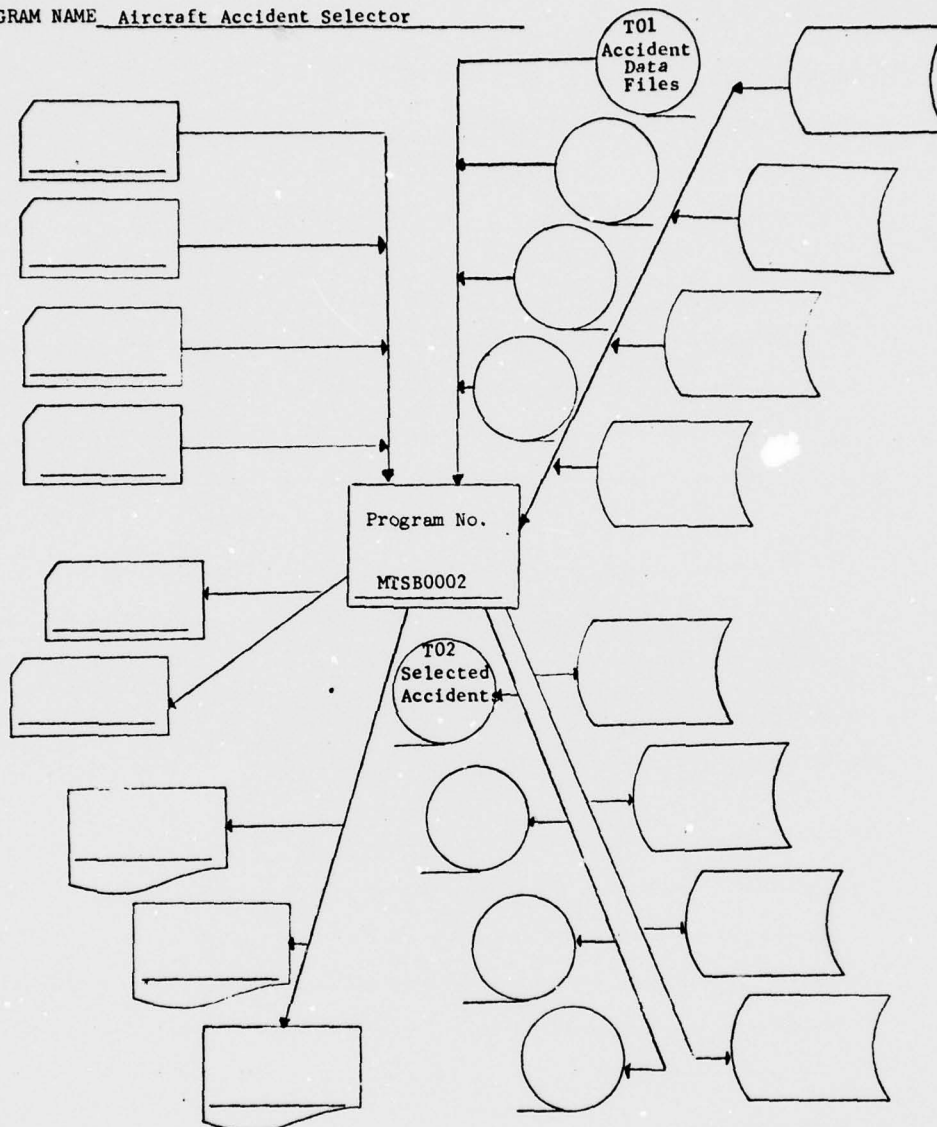
A.9 MACHINE ROOM SET-UP SHEETS

Summary of Three NTSB Accident Data Files

1. MTSB0002 - Aircraft Accident Selector
2. SORT - Sort Accidents
3. 1325020D - Create English Meaning Headers Direct Access File
4. MTSB0001 - Additional Selection and Summarization of Selected Accidents

```
*****
*                                     *
*               T O T A L   R E Q U I R E M E N T S   *
*                                     *
*      I-O                                           *
*                                     *
*      Reader                                           *
*      Printer                                           *
*      Tape Drives - 3                                   *
*      Disk Drives - 2 (1 if 3800 Tracks are Available on Single Drive) *
*                                     *
*      Core                                           *
*      92K                                              *
*                                     *
*****
```

PROGRAM NAME Aircraft Accident Selector



Files:

Sys No.	File Serial	File Name	Disposition
001	N/A	Accident Data Files	Store
002	N/A	Selected Accidents	To Sort

PRINTER SET-UP

Carriage Tape 88 Lines/Page Paper size or form number:
Vertical Alignment Upper Most 14 x 11 1 Part
Horizontal Alignment Left

	<u>Name</u>	<u>Disposition</u>
Cards In:		
Cards		
Out: P1		
P2		
RP3		

CAN JOB BE RESTARTED?

☐ YES

☒ NO

CAN JOB BE RERUN?

☒ YES

☐ NO

If no, see special instructions
for appropriate action.

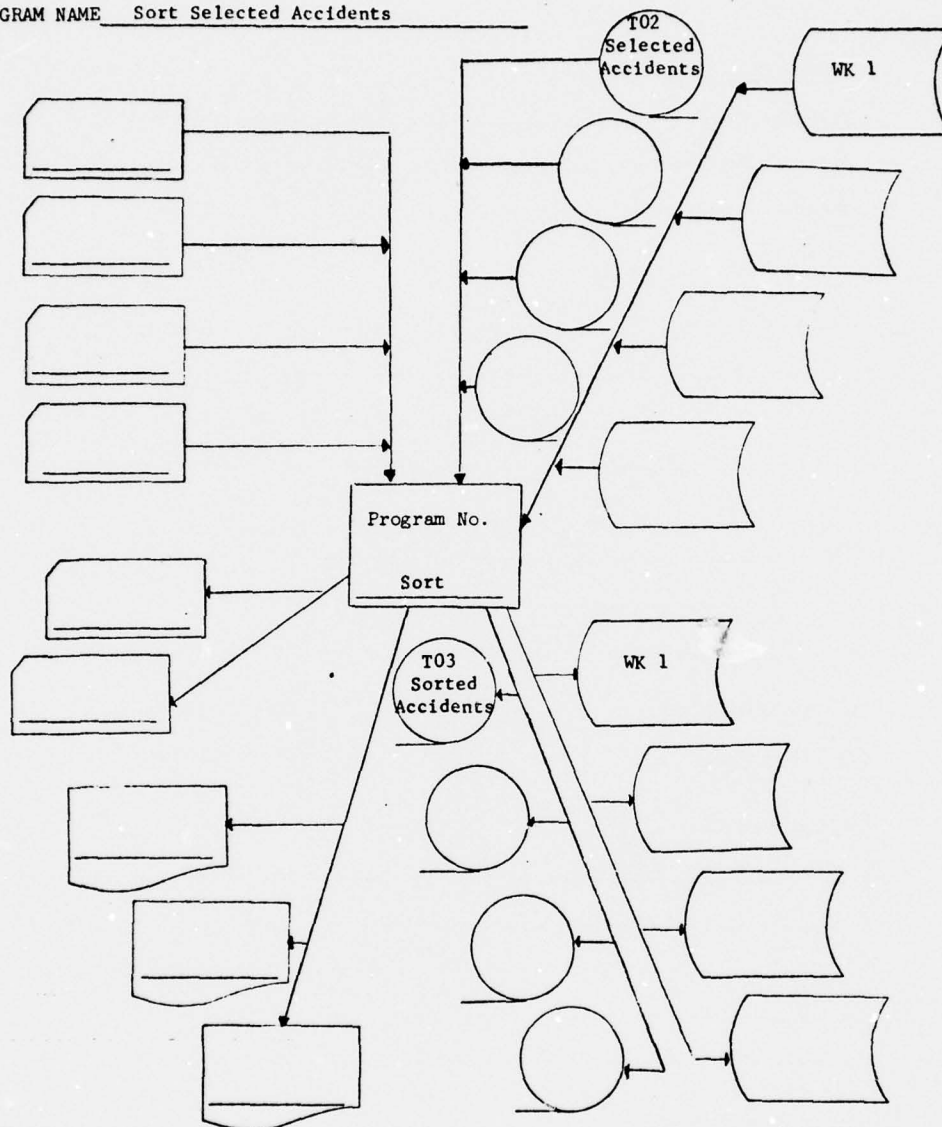
CONSOLE MESSAGE:

ACTION

1. <u>N/A</u>	
2. _____	
3. _____	
4. _____	
5. _____	

Special Instructions:

PROGRAM NAME Sort Selected Accidents



Files:

Sys No.	File Serial	File Name	Disposition
N/A	N/A	N/A	N/A

PRINTER SET-UP

Carriage Tape _____ Paper size or form number: _____
Vertical Alignment _____
Horizontal Alignment _____

	<u>Name</u>	<u>Disposition</u>
Cards In:	_____	_____
	_____	_____
	_____	_____
	_____	_____

Cards		
Out: P1	_____	_____
P2	_____	_____
RP3	_____	_____

CAN JOB BE RESTARTED?

☐ YES

☒ NO

CAN JOB BE RERUN?

☒ YES

☐ NO

If no, see special instructions
for appropriate action.

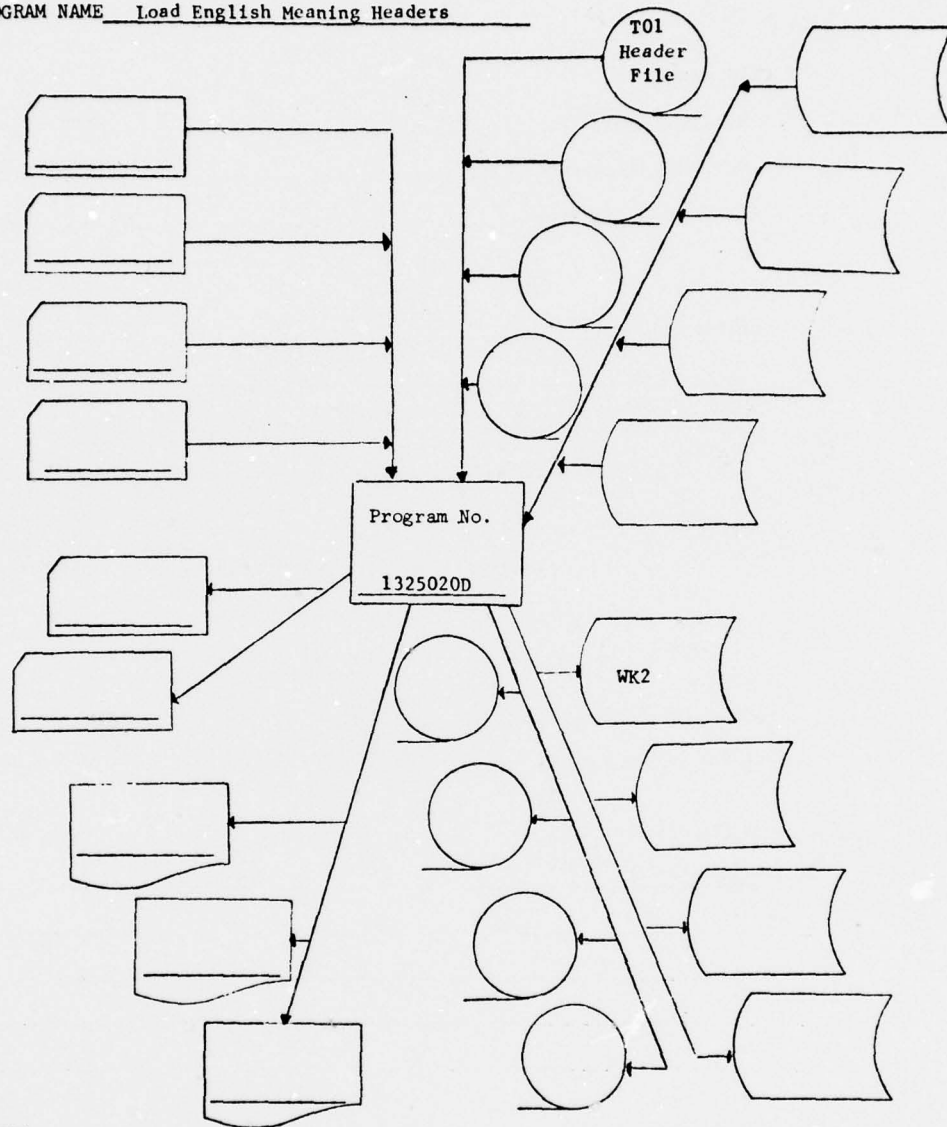
CONSOLE MESSAGE:

ACTION

1. See User's Manual _____
2. _____
3. _____
4. _____
5. _____

Special Instructions:

PROGRAM NAME Load English Meaning Headers



Files:

Sys No.	File Serial	File Name	Disposition
010	325020	NTSB Headers	Store

PRINTER SET-UP

Carriage Tape _____ Paper size or form number: _____
Vertical Alignment _____
Horizontal Alignment _____

	<u>Name</u>	<u>Disposition</u>
Cards In:	_____	_____
	_____	_____
	_____	_____
	_____	_____

Cards		
Out: P1	_____	_____
P2	_____	_____
RP3	_____	_____

CAN JOB BE RESTARTED?

☐ YES

☒ NO

CAN JOB BE RERUN?

☒ YES

☐ NO

If no, see special instructions
for appropriate action.

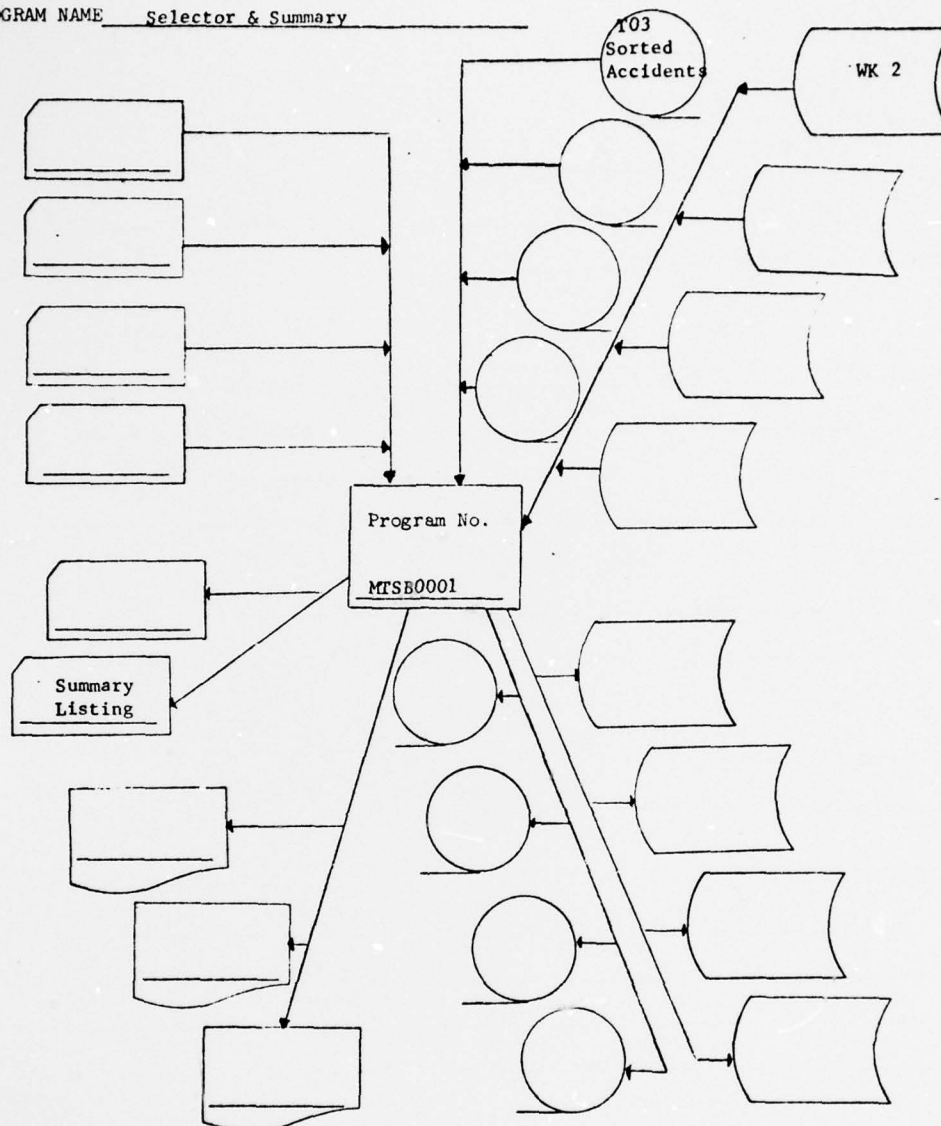
CONSOLE MESSAGE:

ACTION

1.	_____	_____
2.	_____	_____
3.	_____	_____
4.	_____	_____
5.	_____	_____

Special Instructions:

PROGRAM NAME Selector & Summary



Files:

Sys No.	File Serial	File Name	Disposition
018	N/A	N/A	Store or Recycle
019	N/A	NTSB	N/A

PRINTER SET-UP

Carriage Tape 88 Lines/Page Paper size or form number:
Vertical Alignment Upper Most 14 x 11 1 Part
Horizontal Alignment Left

Name Disposition
Cards In: N/A

Cards
Out: P1 N/A
P2 _____
RP3 _____

CAN JOB BE RESTARTED?

☐ YES

☒ NO

CAN JOB BE RERUN?

☒ YES

☐ NO

If no, see special instructions
for appropriate action.

CONSOLE MESSAGE:

ACTION

1. _____
2. _____
3. _____
4. _____
5. _____

Special Instructions:

APPENDIX B

REPRESENTATIVE GENERAL AVIATION AIRPLANE STRUCTURE

B.1 INTRODUCTION

This appendix describes the structure that is representative of two different types of general aviation light fixed-wing airplanes. In addition typical cross sections, from which basic area properties (A , I_{yy} , I_{zz}) are obtained, are shown. The structure material properties (E , G), combined with the area properties, are used to determine member stiffnesses.

B.2 AIRPLANE A

Airplane A is a category 1 type of airplane with the following general description:

- o Single-engine, high-wing configuration
- o Side by side seats (two occupants)
- o Used for training, sport or aerobatic purposes
- o Stall speed (flaps down) ≤ 42 knots
- o Cruise speed (75% power) ≤ 102 knots
- o Flight design load factor of; $+4.4g$'s and $-1.76g$'s (utility)
 $+6.0g$'s and $-3.00g$'s (aerobatic)
- o Maximum takeoff weight = 1600 pounds
- o Wing span = 384 inches
- o Length = 280 inches

Figure B-1a shows an overall view of the airplane and Figure B-1b shows the mathematical model used to represent the structure for crash analysis.

Figures B-2 through B-12 show different structures and approximate cross sections for the respective structure. Table B-1 describes the Airplane A Structure with regard to material properties, strength, design concepts, size and attachments.

B.3 AIRPLANE B

Airplane B is a category 3 type airplane with the following general description:

- o Single engine low wing configuration
- o Single seat
- o Used for application of chemicals or seeding crops
- o Stall speed (flaps down) ≤ 50 knots
- o Cruise speed (75% power) ≤ 122 knots
- o Flight design load factor of; $+3.8g$'s and $-1.52g$'s
- o Maximum takeoff weight = 3300 pounds (4000 pounds in restricted category)
- o Wing span = 474 inches
- o Length = 273 inches

Figure B-13a shows an overall view of the airplane and Figure 13b shows the mathematical model used to represent the structure for crash analysis. Figures B-14 through B-20 show different structure and approximate cross sections used to represent the structure. Table B-2 describes the airplane B structure with regard to material properties, strength, design concept, size and attachments. Table B-3 presents the cross sectional dimensions of the fuselage tubular framework.

TABLE B-1 DESCRIPTION OF AIRPLANE A STRUCTURE				
Structure	Materials and Properties	Concepts and Size	Attachments	Applicable Figures
1. Engine Mount Assembly and Nose Landing Gear	4130 Steel E = 30×10^6 psi G = 11×10^6 psi F _{ty} = 75×10^3 psi F _{tu} = 95×10^3 psi	Tubular members .75 in. x .049 in. .50 in. x .049 in. Hydraulic cylinder nose gear	Bolt attachments to fire wall, 4 places, to engine 4 places.	B-2
2. Main Landing Gear	6150H Steel E = 30×10^6 psi G = 11×10^6 psi F _{ty} = 205×10^3 psi F _{tu} = 245×10^3 psi	Flat steel spring. Tapered cross section. Average cross section are shown in Figure B-3	Single bolt attachment inboard to fuselage	B-3
3. Landing Gear Bulkhead	2024-T3 E = 10.5×10^6 psi G = 4×10^6 psi F _{ty} = 37×10^3 psi F _{tu} = 63×10^3 psi	Two formed bulkheads with skin attachment above and below. Dimensions are shown in Figure B-5	Landing gear forgings attached between bulkheads by means of bolts	B-4, B-5
4. Firewall	Stainless Steel E = 27×10^6 psi G = 11×10^3 psi F = 58×10^3 psi (avg. of F _{ty} and F _{tc}) F _{tu} = 124×10^3 psi	Beaded flat aluminized iron sheet, a peripheral stiffener and attaching fuselage skin. Thickness = .025 in.	Steel rivets	B-4, B-5
5. Upper and Lower Engine Mount Stringer	2043-T3 Aluminum E = 10.5×10^6 G = $4. \times 10^6$ psi F _{ty} = 37×10^3 psi F _{tu} = 63×10^3 psi	Upper mount stringer is a tapered U channel section. Average section shown in Figure B-5, Lower Mount Stringer is a Channel with J edges, as shown in Figure B-5	Rivets	B-4, B-5

TABLE B-1 DESCRIPTION OF AIRPLANE A STRUCTURE (Cont'd)				
Structure	Materials and Properties	Concepts and Size	Attachments	Applicable Figures
6. Upper Cabin Area	Same as No. 5	This area is comprised of a root rib-upper door jam, cabin top skin and two stringers. It extends from the forward door post to aft door post. Dimensions are shown in Figure B-5.	Rivets	B-4, B-5
7. Forward Floor Bulkhead	Same as No. 5	Consists of formed bulkhead stiffener on aft side, floor-board on top and skin on bottom. Average cross section, as shown in Figure B-7.	Rivets	B-6, B-7
8. Forward Door Post	Same as No. 5	Assemblage of three pieces, as shown in Figure B-7. Maximum cross-section is shown.	Rivets, screws and bolts	B-6, B-7
9. Fuselage Carry thru Structure	Same as No. 5	Formed channels, same dimension front and rear. Approximate dimensions are shown in Figure B-7	Rivets and bolts	B-6, B-7
10. Rear Door Post	Same as No. 5	Assemblage of three pieces, doorpost, jam and skin. Dimensions along uniform length are shown in Figure B-9.	Rivets, screws and bolts	B-8, B-9
11. Upper and Lower Aft Fuselage	Same as No. 5	Upper sections consists of skin-stringer arrangement. Lower section is a semi-monocoque structure. Approximate dimensions are shown in Figure B-9	Rivets	B-8, B-9

TABLE B-1 DESCRIPTION OF AIRPLANE A STRUCTURE (Cont'd)

Structure	Materials and Properties	Concepts and Size	Attachments	Applicable Figures
12. Tail Cone	Same as No. 5	Tapered semi-monocoque section. Approximate average section is shown in Figure B-10	Rivets	B-8, B-10
13. Bulkhead at F.S. 95	Same as No. 5	Formed one piece sheet metal Bulb angle reinforce lower section. Approximate cross-section is shown in Figure B-10.	Bolts at wing attachment. Rivets at forward section.	B-8, B-10
14. Wing	6061-T6 $E = 10.5 \times 10^6$ psi $G = 4 \times 10^6$ psi $F_{ty} = 32 \times 10^3$ psi $F_{tu} = 38 \times 10^3$ psi	Two spar arrangement. Average cross section at constant chord line and for tapered expanse is used.	Bolted to strut and fuselage top	B-11, B-12
15. Wing Strut	Same as No. 14	Extruded tube Uniform cross section	Forged attachment fittings single bolted at each end of strut extrusion	B-11, B-12

F_{ty} = Tensile yield stress

F_{cy} = Compressive yield stress

F_{tu} = Tensile ultimate stress

E = Modulus of Elasticity

G = Modulus of Rigidity

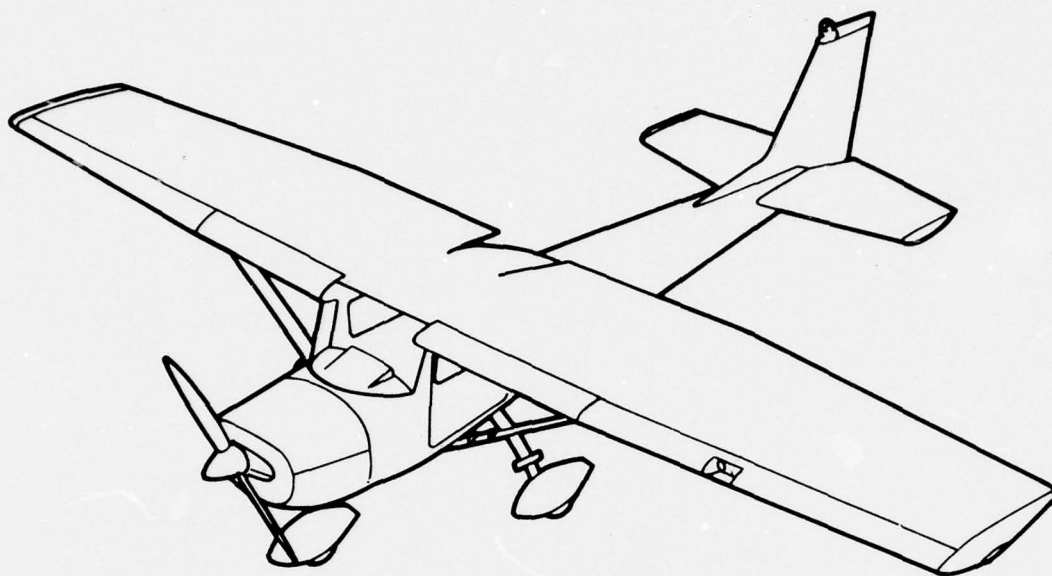
TABLE B-2 DESCRIPTION OF AIRPLANE B STRUCTURE				
Structure	Materials and Properties	Concepts and Size	Attachments	Applicable Figures
1. Fuselage	4130 Steel ⁶ E = 30×10^6 psi G = 11×10^6 psi F _{ty} = 75×10^3 psi F _{tu} = 95×10^3 psi	Tubular members of various sizes. See Table B-3.	Pin joints (bolt through clevis) for strut and wing attachments. Bolted joints for Firewall and tail cone attachments	B-14
2. Engine Mounts	4130 Steel ⁶ E = 30×10^6 psi G = 11×10^6 psi F _{ty} = 75×10^3 psi F _{tu} = 95×10^3 psi	Tubular members: .75 inch x .049 inch .875 inch x .049 inch Arrangements and attachments are shown in Figure B-15	Bolted to firewall, 4 places. Isolator mounted to engine, 4 places	B-15
3. Wing Strut	2024-T3 Aluminum E = 10.5×10^6 psi G = 4.0×10^6 psi F _{ty} = 37×10^3 psi F _{tu} = 63×10^3 psi	Constant cross section. See Figure B-12 for dimensions	Pin joints at fuselage and wing.	B-16
4. Wing	2024-T3 Aluminum E = 10.5×10^6 psi G = 4.0×10^6 psi F _{ty} = 37×10^3 psi F _{tu} = 63×10^3 psi	Two spar arrangement Rib spacing is approximately 26 inches. Skin thickness = .035 to .032 inches. Average dimensions are shown in Figure B-17.	Pin joint to the fuselage at front and rear spars	B-17
5. Landing Gear	6150 H Steel E = 30×10^6 psi G = 11×10^6 psi F _{ty} = 205×10^3 psi F _{tu} = 245×10^3 psi	Tapered spring. Average section = 4.5 inches wide. Spring provides all landing gear stiffness.	Four bolts at fuselage each side. One bolt to axle.	B-18

TABLE B-2 DESCRIPTION OF AIRPLANE B STRUCTURE (Cont'd)				
Structure	Materials and Properties	Concepts and Size	Attachments	Applicable Figures
6. Vertical Tail	2024-T3 Aluminum E = 10.5 x 10 ⁶ psi G = 4.0 x 10 ⁶ psi F _{ty} = 37 x 10 ³ psi F _{tu} = 63 x 10 ³ psi	Front and rear spar Spar thickness = .040 inches. Shim thickness = .025 inches. Cross section is shown in Figure B-19	Bolt attachment at front and rear spars to tail cone	B-19
7. Fuselage Tailcone	2024-T3 Aluminum E = 10.5 x 10 ⁶ psi G = 4.0 x 10 ⁶ psi F _{ty} = 37 x 10 ³ psi F _{tu} = 63 x 10 ³ psi	Intermediate bulkheads, stiffened-shim arrangement. Thickness of skin, bulkhead and stiffener = .032 inches. Cross sections and attachments are shown in Figure B-20	Bolted to aft bulkhead, 4 places.	B-20
Notes: F _{ty} = Tensile yield stress F _{tu} = Tensile ultimate stress E = Modulus of Elasticity G = Modulus of Rigidity				

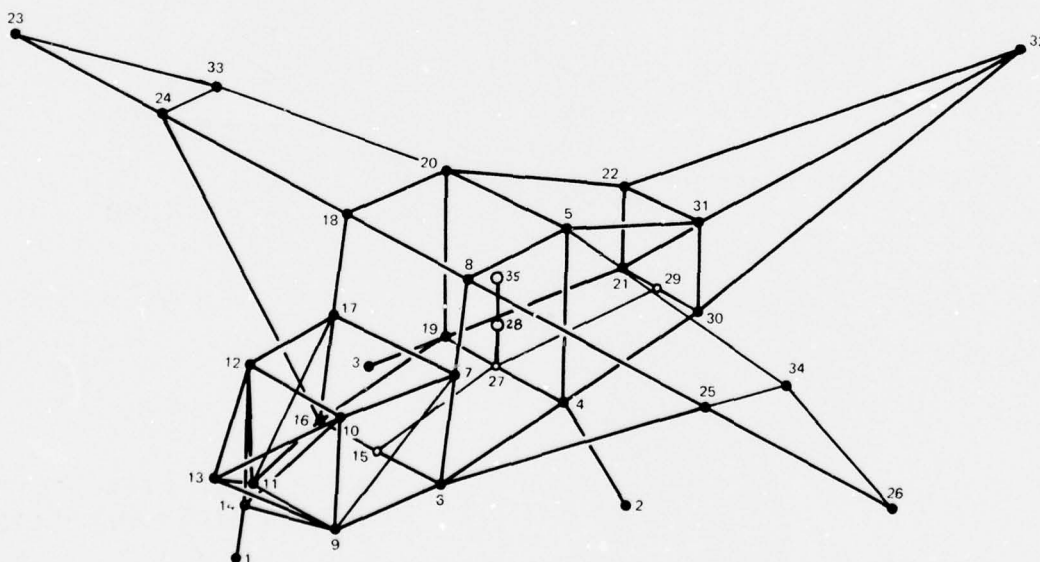
TABLE B-3 AIRPLANE B FUSELAGE STRUCTURE
TUBULAR MEMBER SIZES

Member	i^{th} Node (a)	j^{th} Node (a)	Tube Size (diameter and thickness), Inches
8	22	32	.750 x .058
9	4	32	.875 x .049
10	32	33	.50 x .035
11	6	33	.875 x .049
12	23	33	1.125 x .049
13	27	33	1.375 x .083
14	5	6	1.375 x .058
15	4	5	.75 x .035
16	5	17	1.0 x .049
17	5	7	1.0 x .049
18	5	17	.625 x .035
19	6	8	1.0 x .049
20	6	18	1.25 x .049
21	6	26	.875 x .049
22	7	8	.875 x .049
23	7	9	1.00 x .065
24	7	37	1.5 x .058
25	24	26	1.0 x .049
26	25	27	1.0 x .049
27	8	10	.625 x .049
28	8	15	1.0 x .049

- (a) See Figure B-13 for i^{th} and j^{th} node designations
(b) Tube sizes for left side are shown, right side has same dimensions
(c) Diagonal member sizes are 1.0 inch x .049 inch



(a) OVERALL VIEW



(b) MATH MODEL

Figure B-1. Airplane A

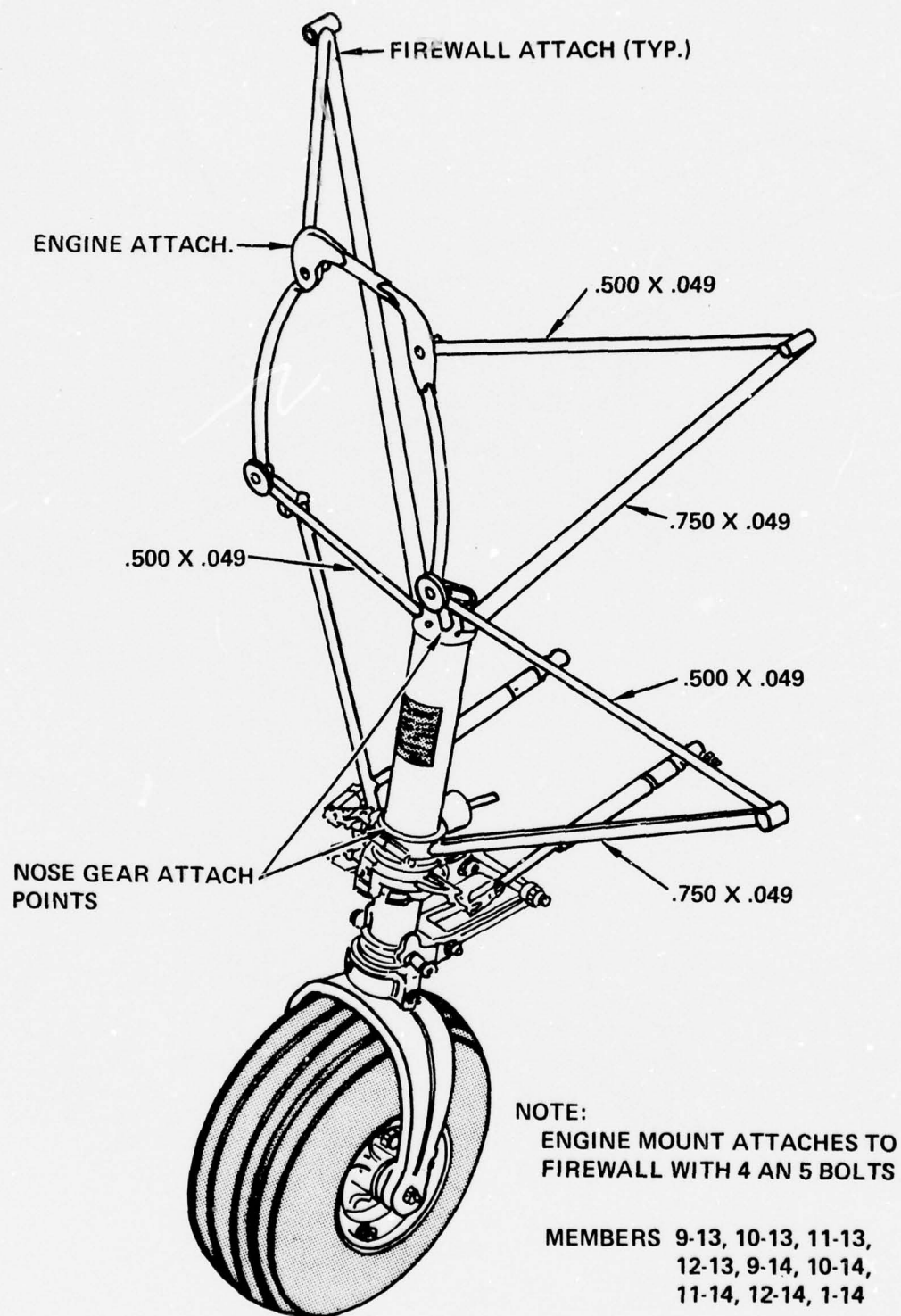


Figure B-2. Engine Mount and Nose Gear Assembly

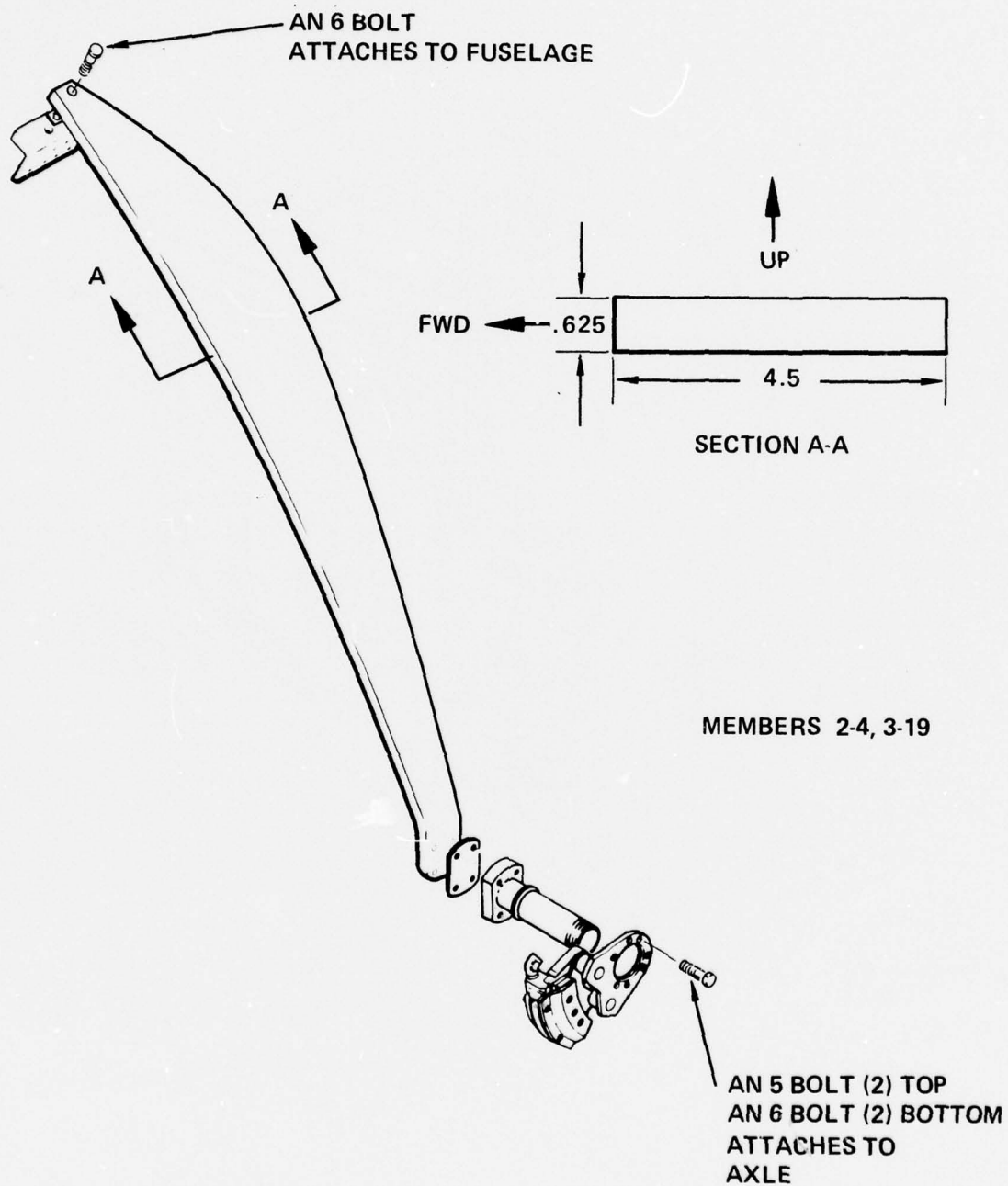


Figure B-3 Main Landing Gear Cantilever Spring Cross-Section

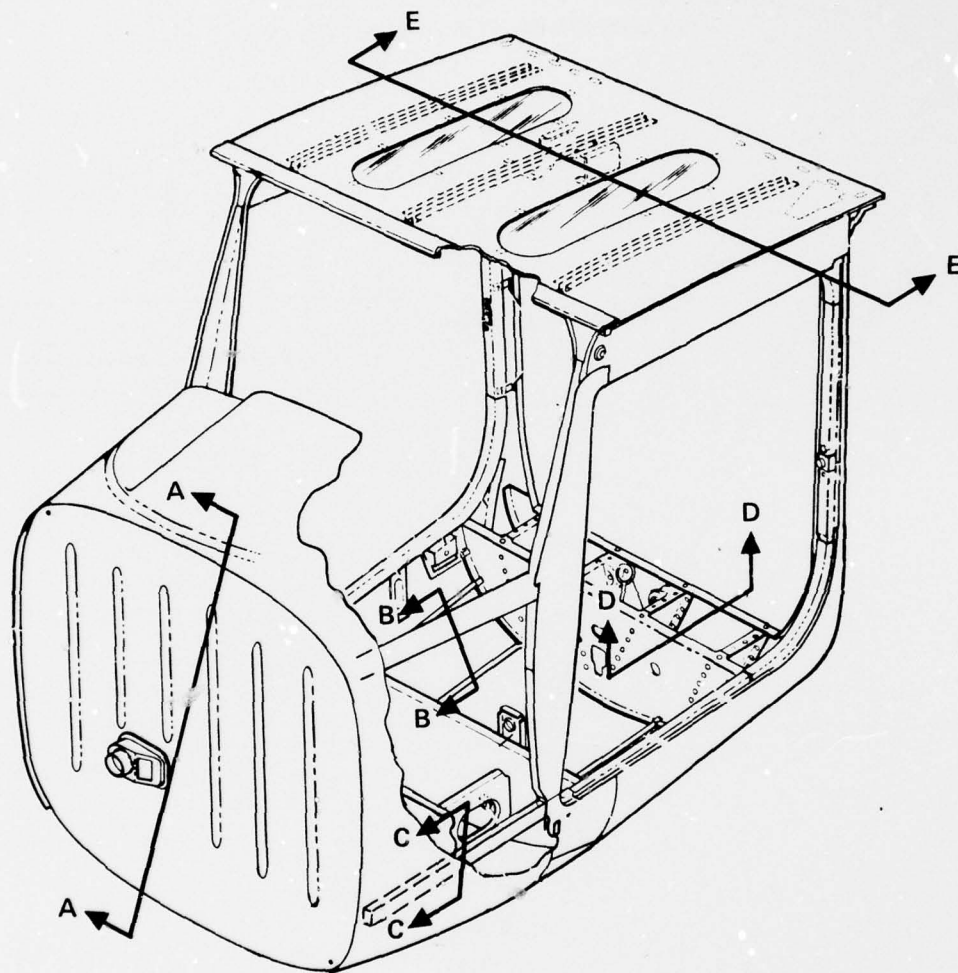


Figure B-4. Fuselage Front and Center Section Assembly

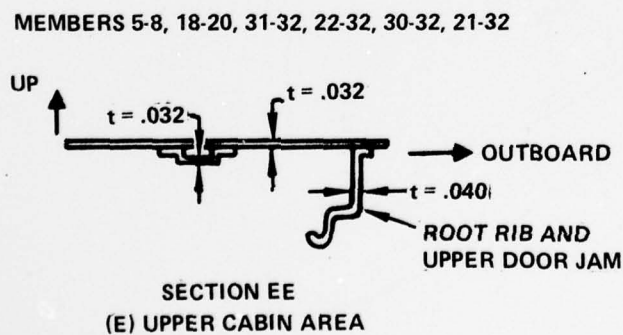
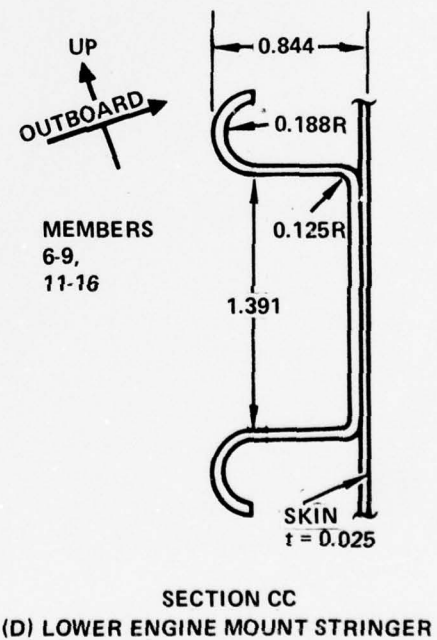
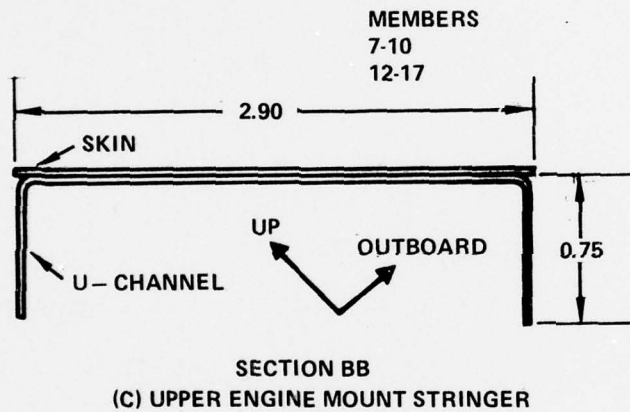
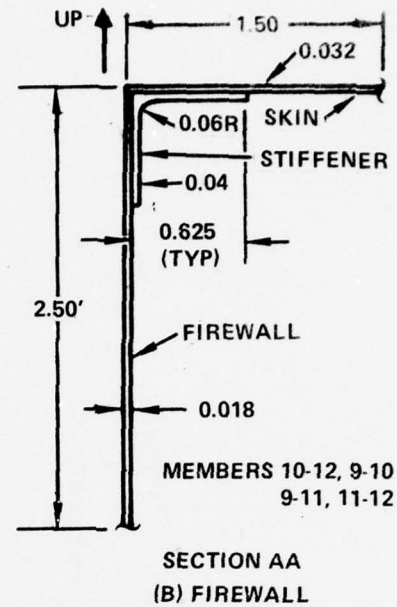
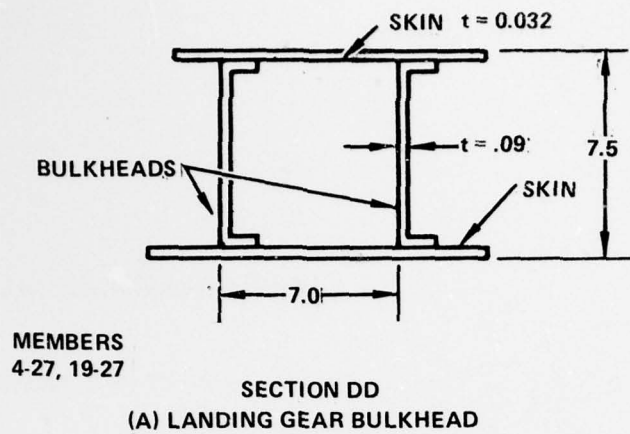


Figure B-5 Fuselage Front and Center Structure Cross Sections

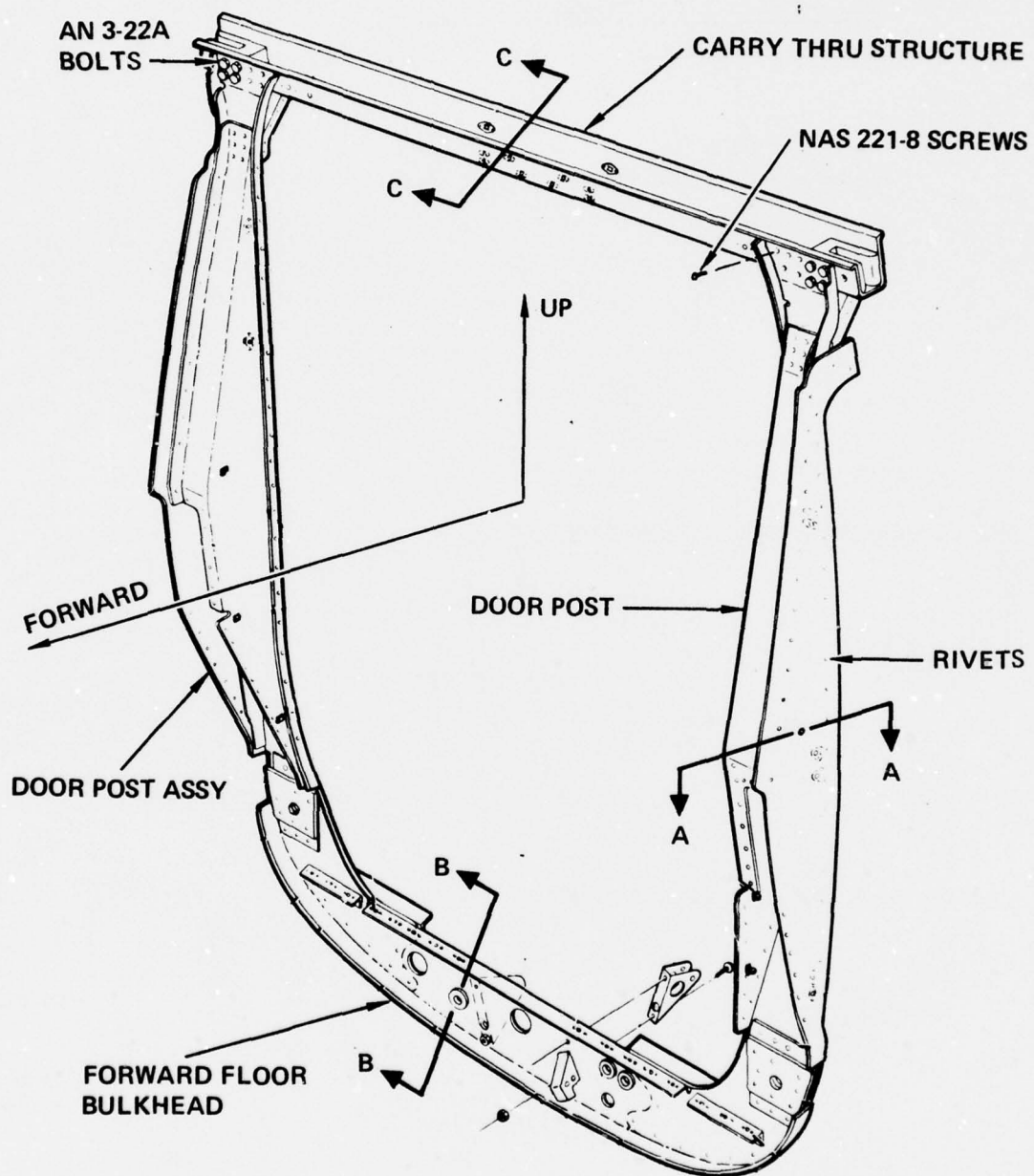


Figure B-6. Forward Door Post, Forward Floor Bulkhead, and Carry Thru Structure

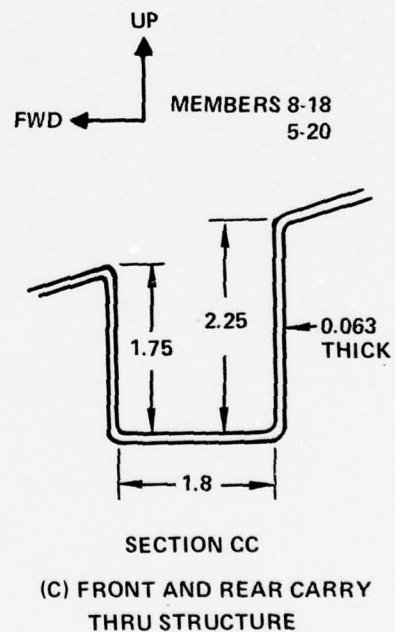
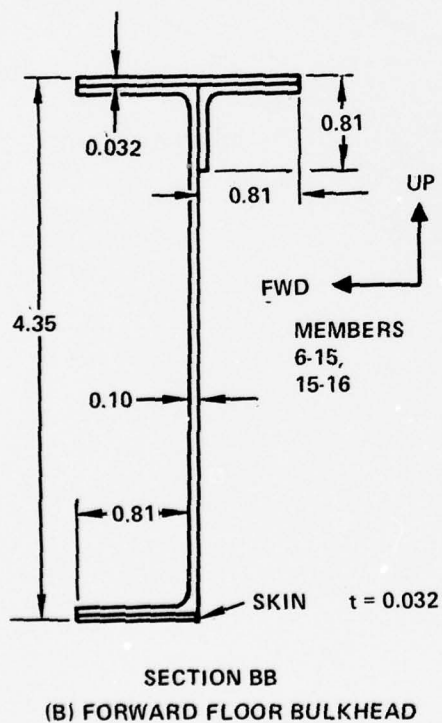
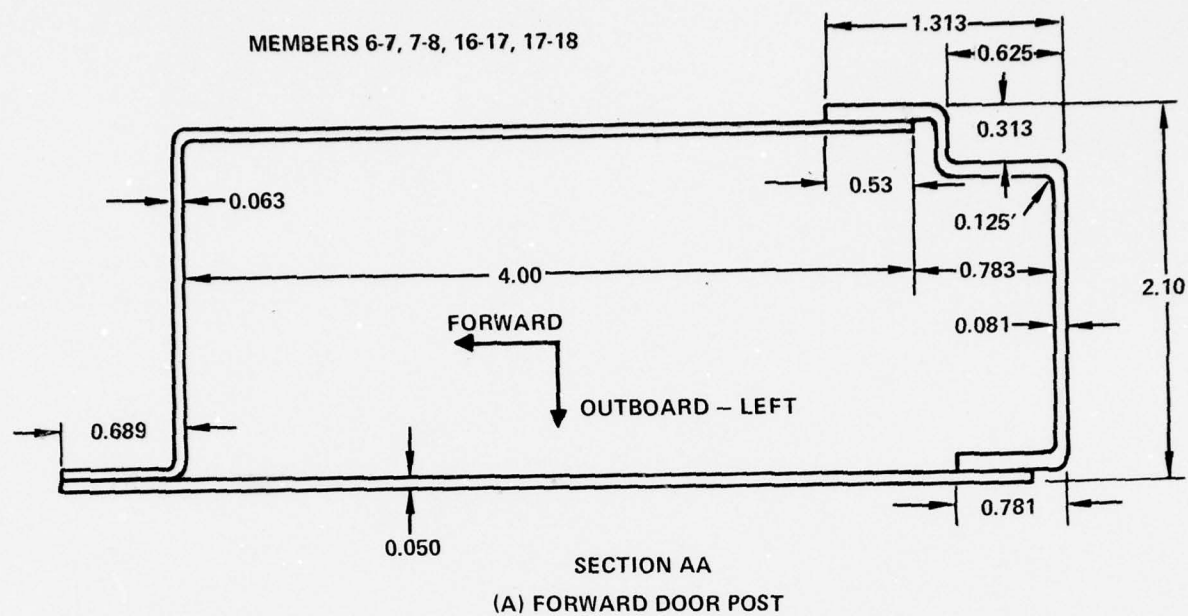


Figure B-7 Forward Door Post, Forward Floor Bulkhead, and Carry Thru Structure Cross Sections

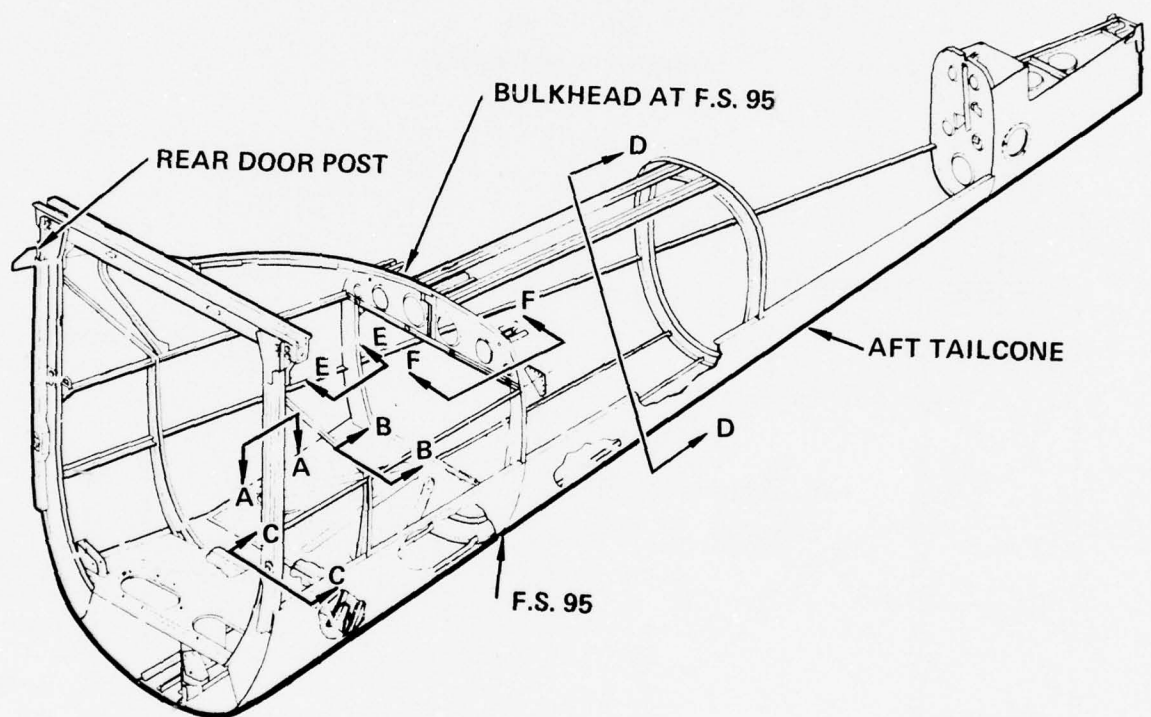
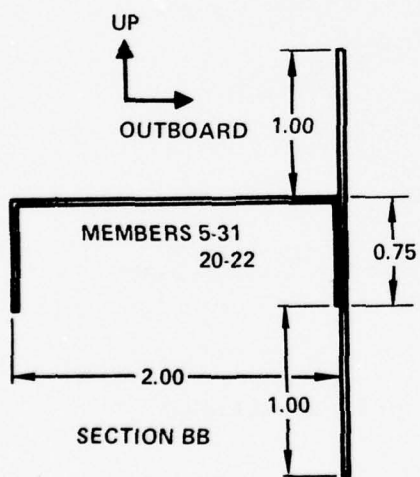
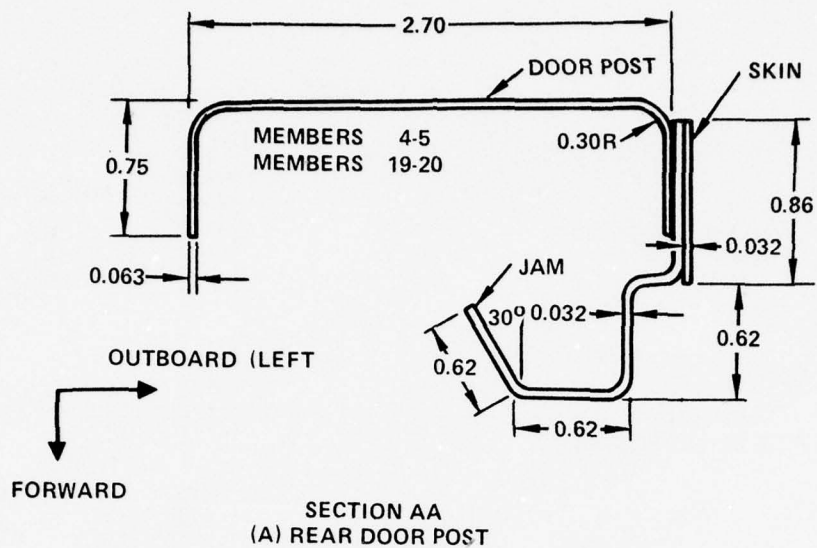
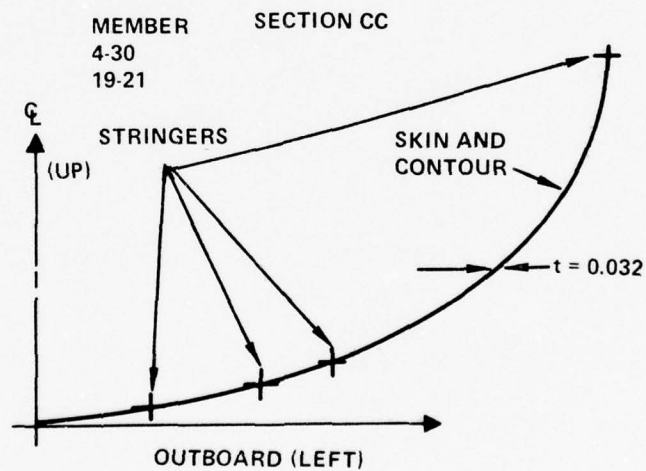


Figure B-8. Aft Fuselage Structure



(B) UPPER AFT FUSELAGE



(C) LOWER AFT FUSELAGE

Figure B-9 Aft Fuselage Structure Cross Sections

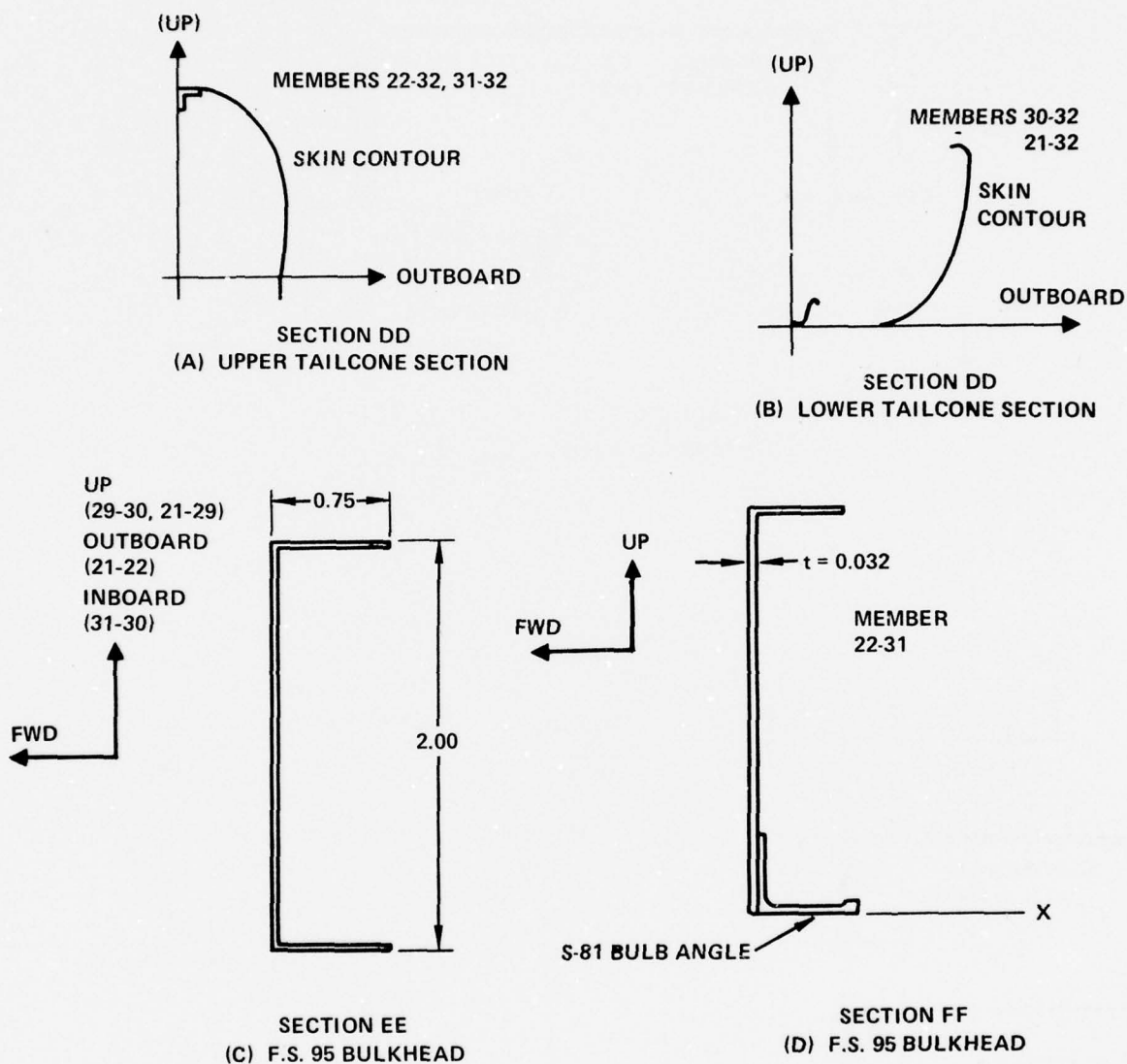


Figure B-10. Tail Cone and F.S. 95 Bulkhead Structure Cross Sections

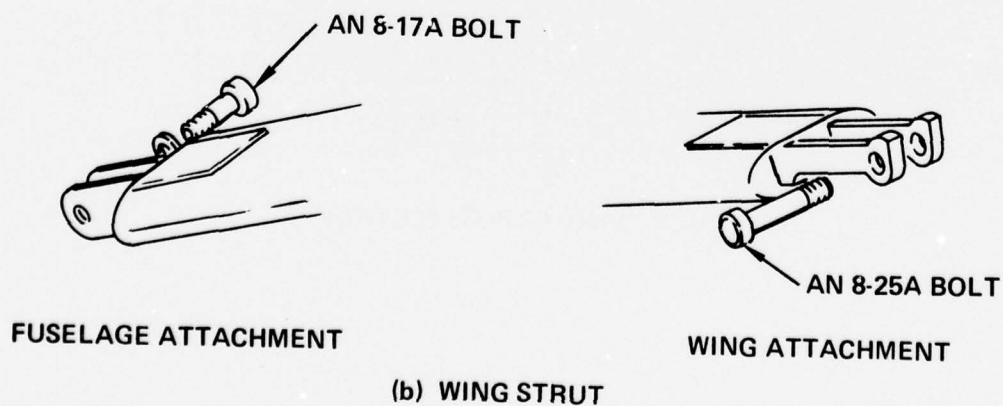
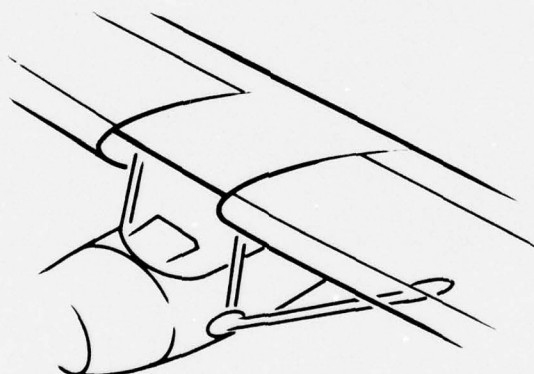
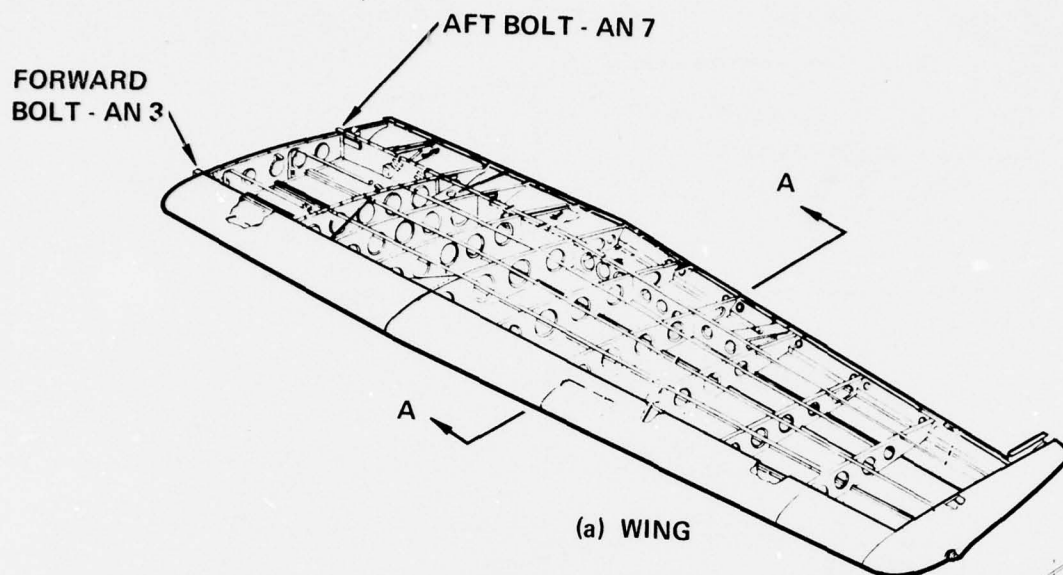
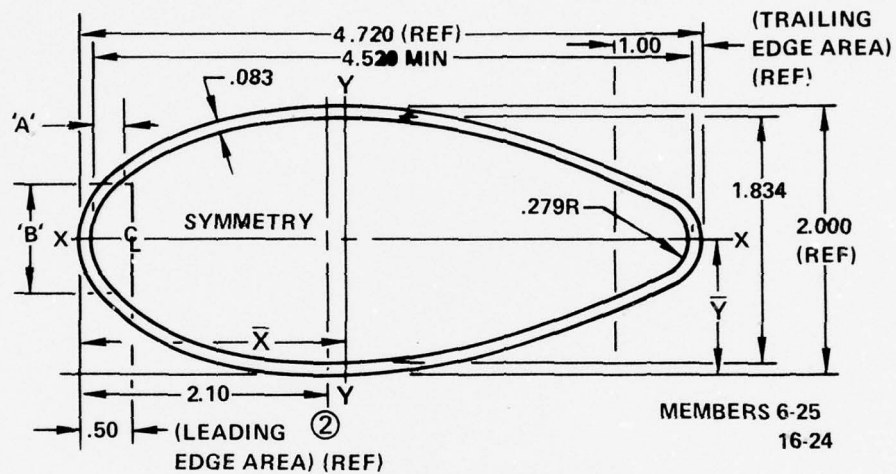


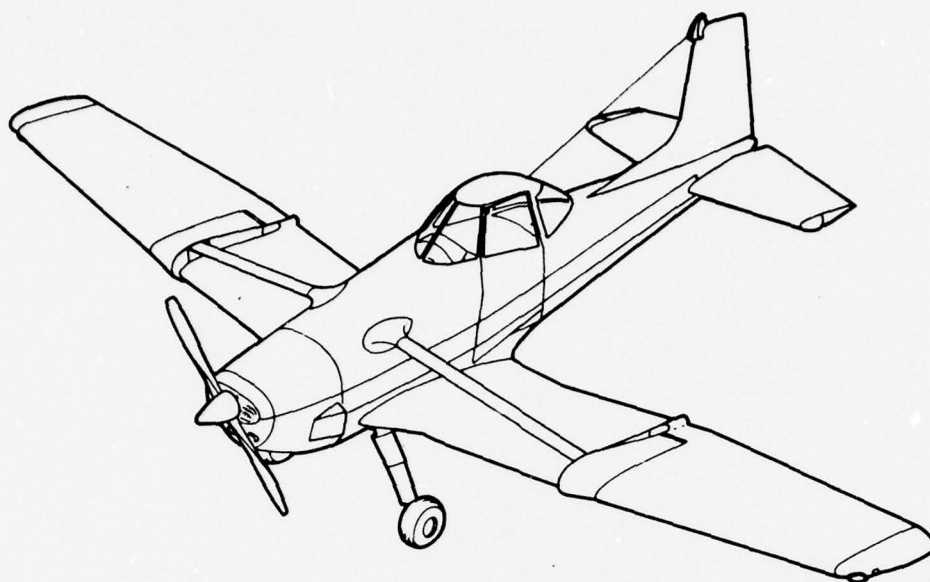
Figure B-11. Wing and Wing Strut Structure



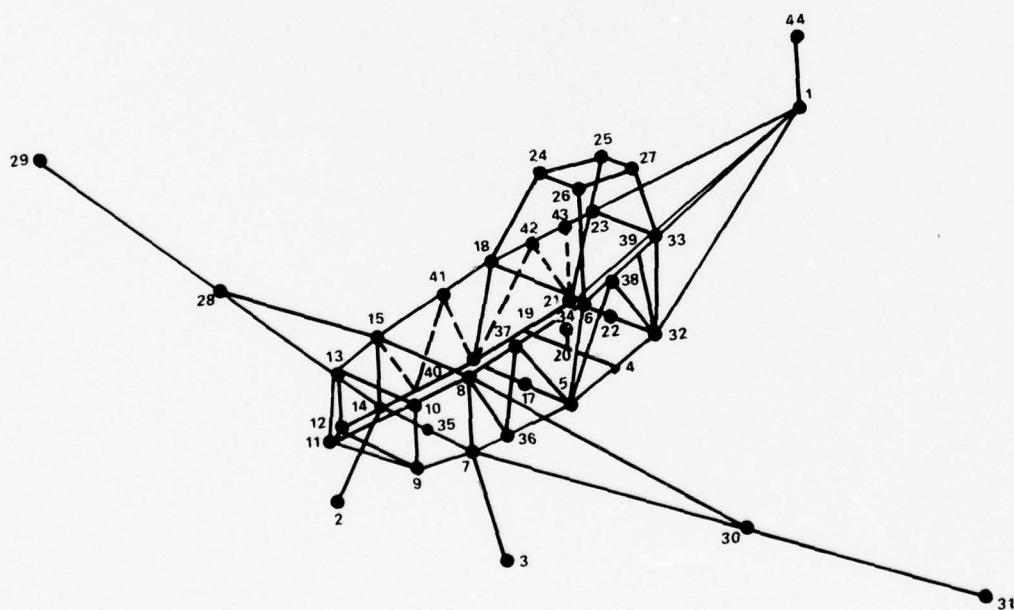
'A'	'B' MIN
.255	.955
.825	1.565
3.040	1.470
3.755	1.070

AREA SQ. IN.	\bar{X}	\bar{Y}	$\sum X^2$	$\sum Y^2$	WEIGHT LBS. PER 100 IN.
.897	2.27	1.0	4.645	1.8686	8.97

Figure B-12. Wing and Wing Strut Structure Cross Sections



(a) OVERALL VIEW



(b) MATH MODEL

Figure B-13. Airplane B

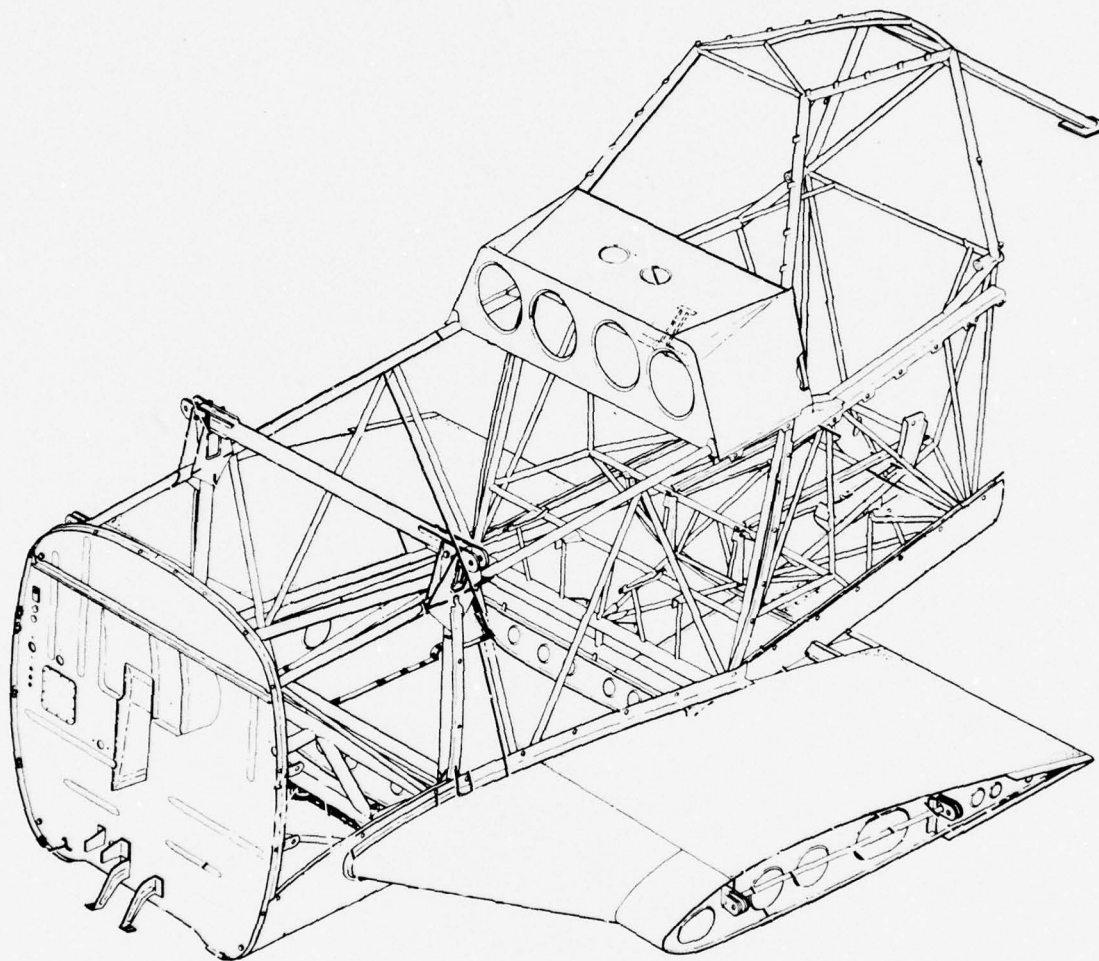
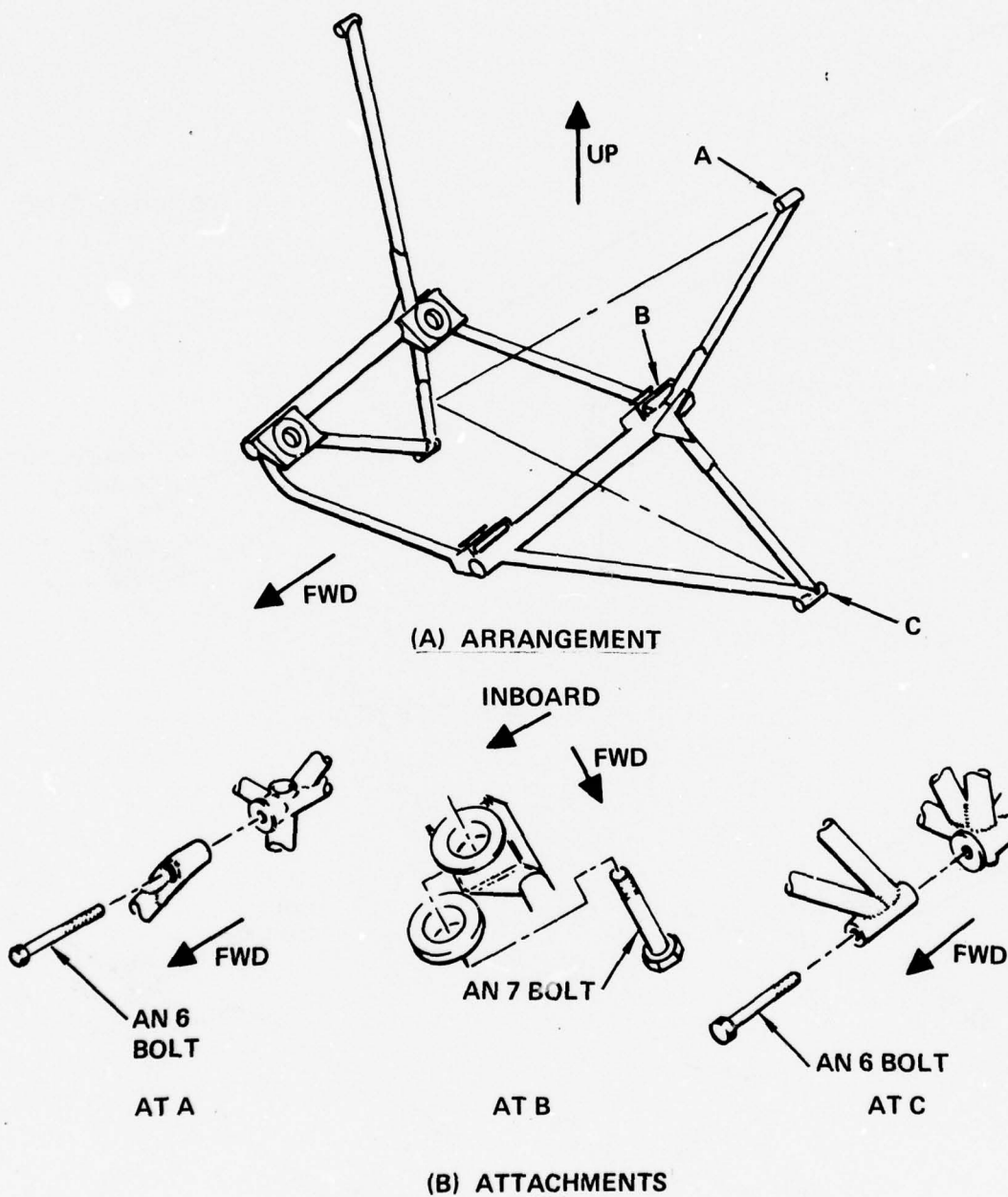


Figure B-14. Fuselage Structure



MEMBERS 9-11, 10-11, 11-12, 11-13

Figure B-15. Engine Mount Arrangement

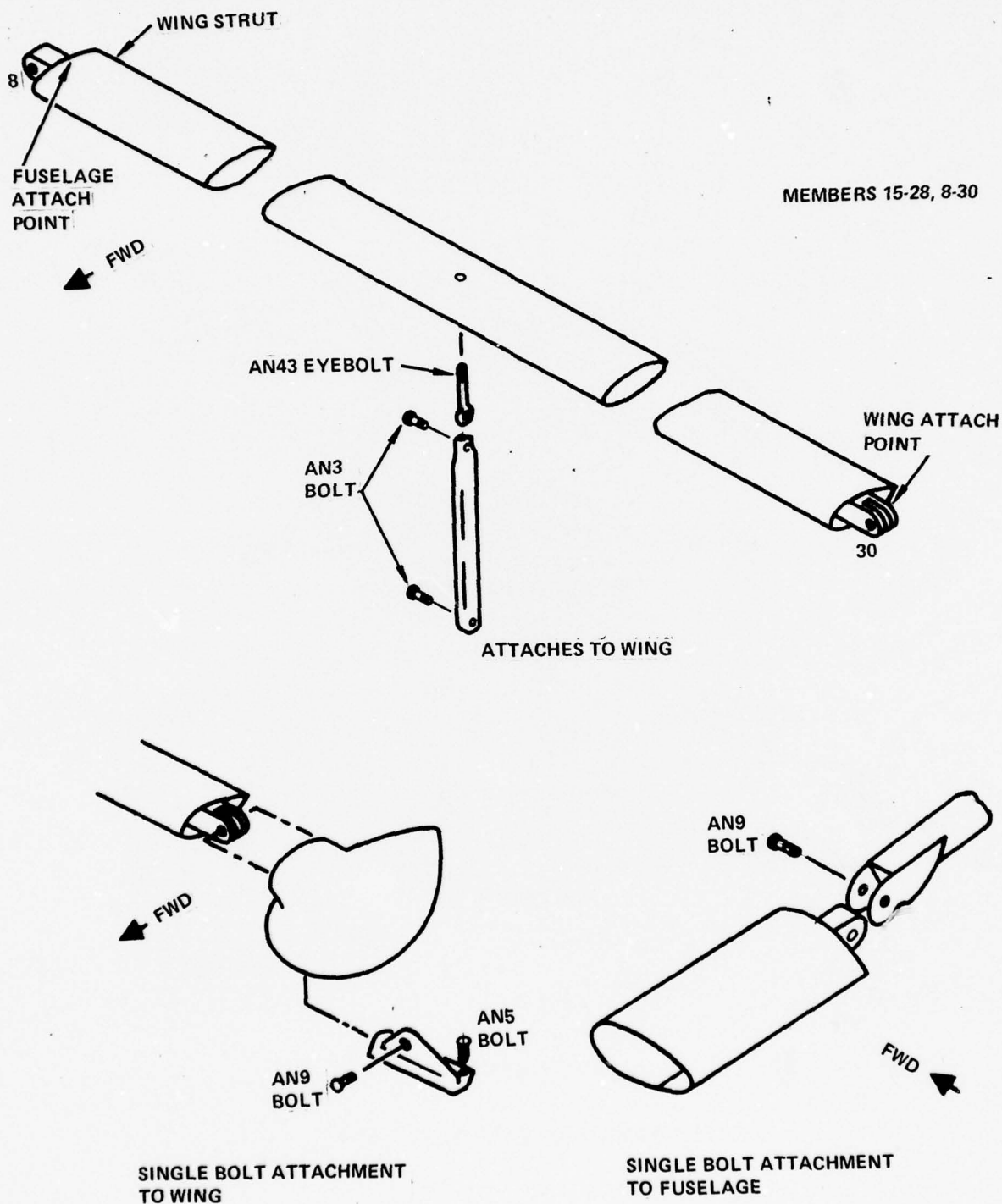


Figure B-16. Wing Strut Structure and Attachments

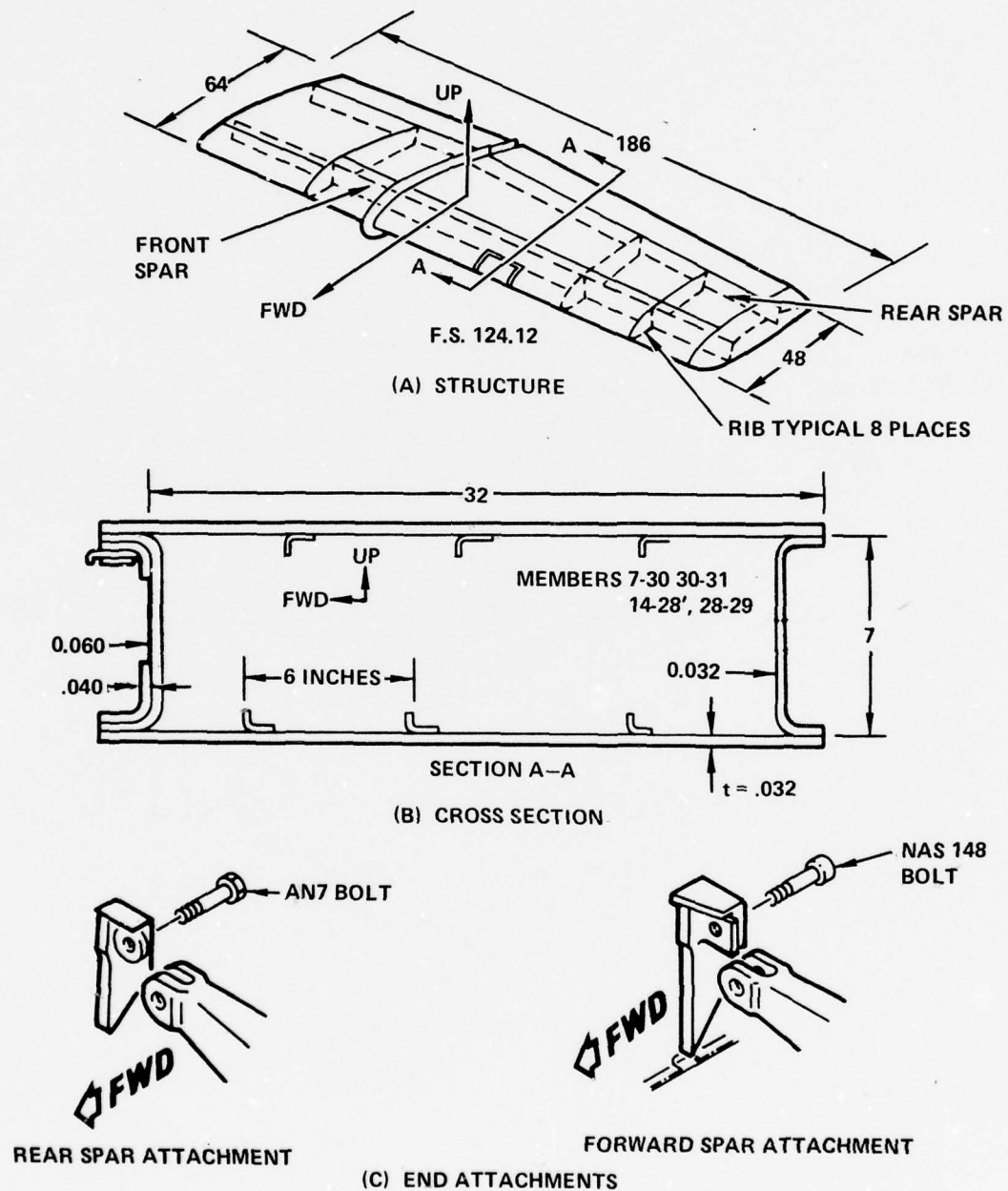


Figure B-17. Wing Structure, Cross Section and Attachments

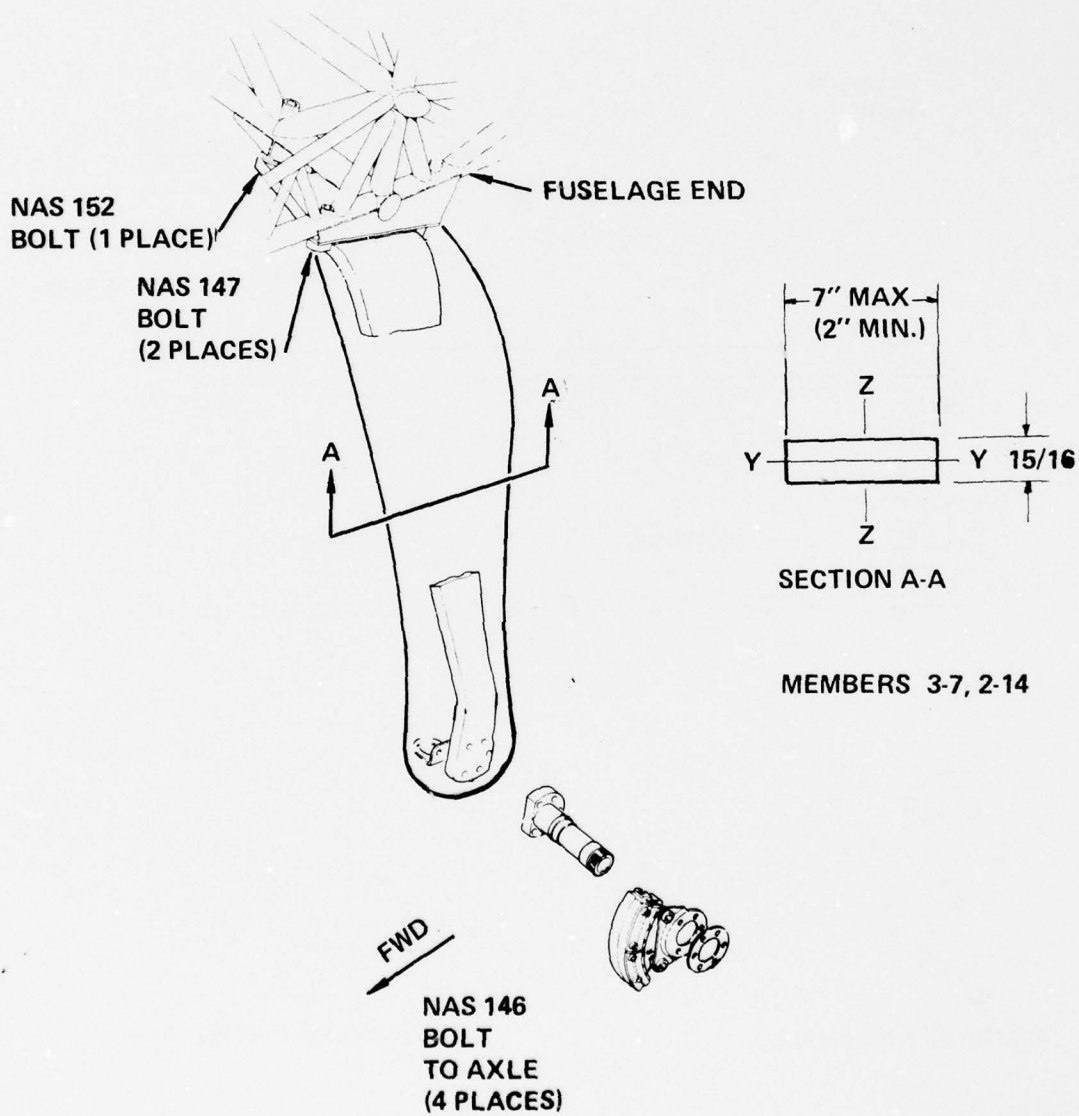
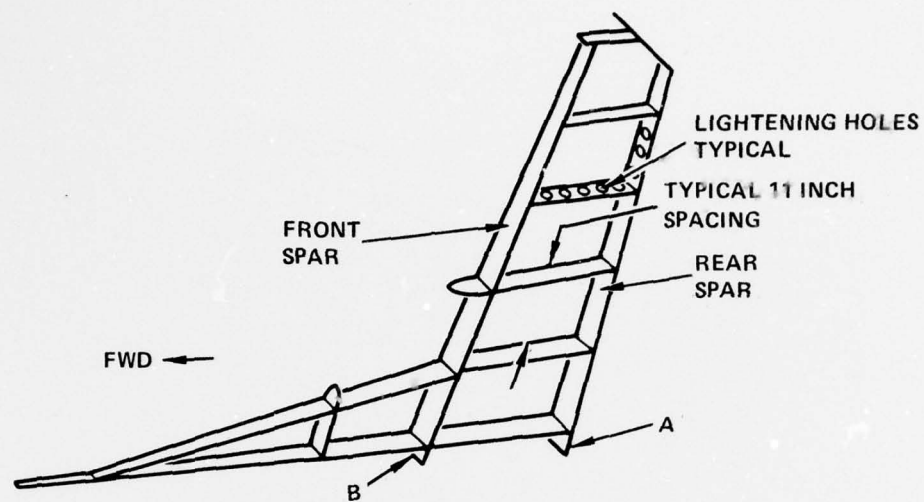
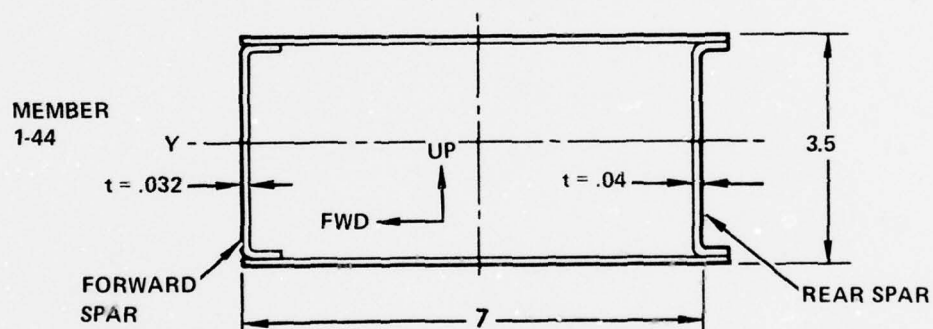


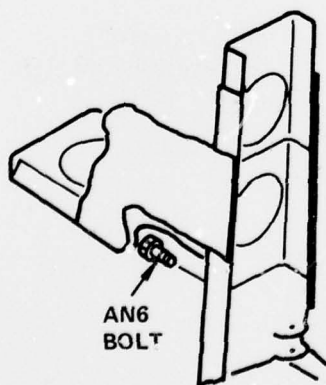
Figure B-18. Main Landing Gear Structure Cantilever Spring Cross Section



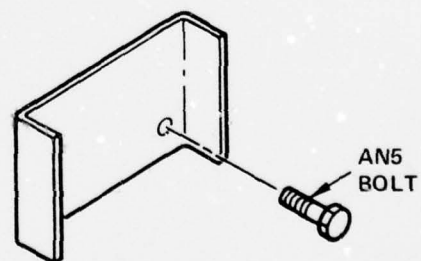
(A) STRUCTURE



(B) AVERAGE CROSS SECTION AT WL 50.



DETAIL B



DETAIL A

(C) ATTACHMENTS

Figure B-19. Vertical Tail Structure, Cross Section and Attachments

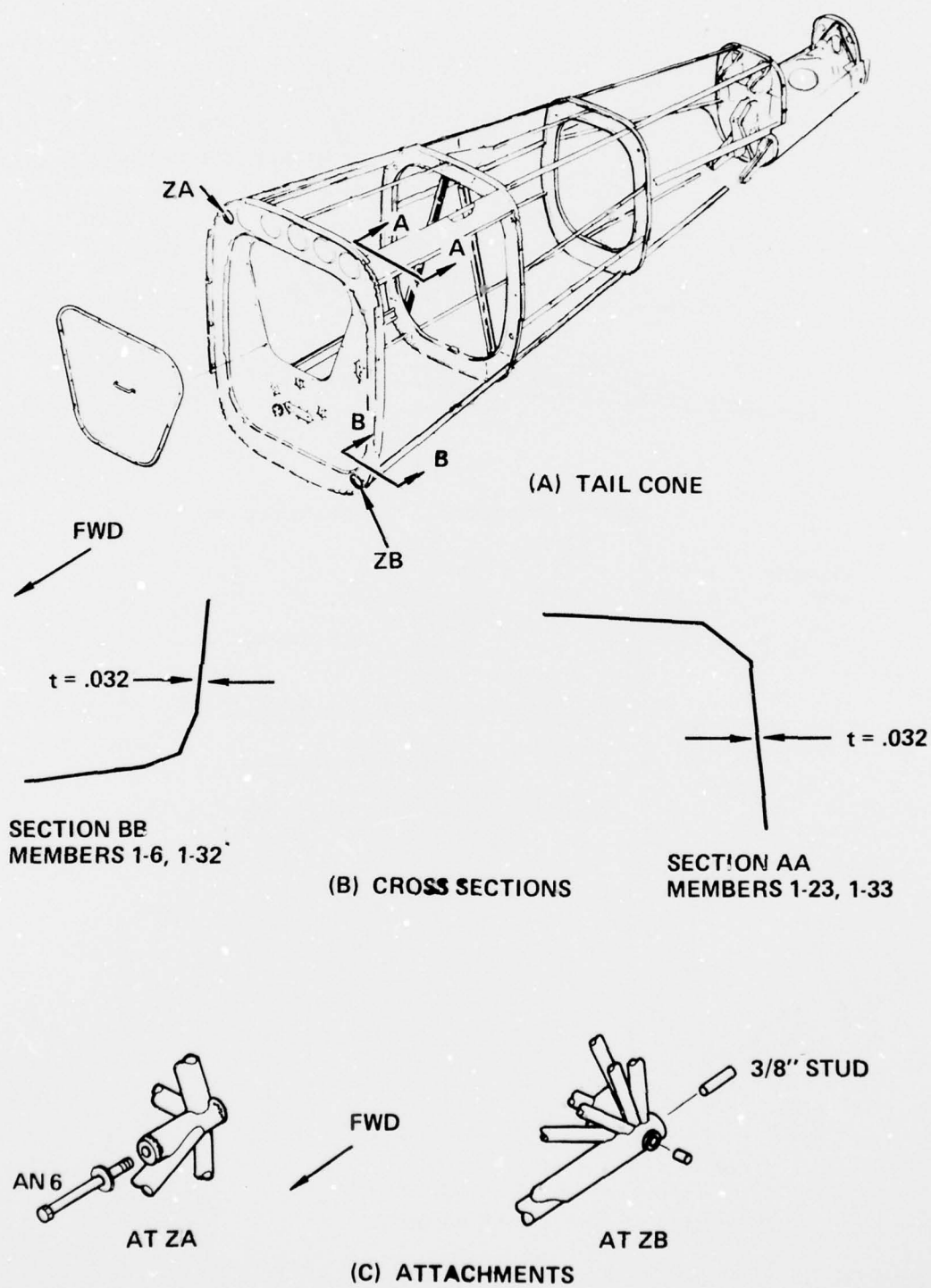


Figure B-20. Fuselage Tail Cone, Cross Section and Attachments

APPENDIX C

AIRPLANE MATH MODEL AND FILM DATA

C.1 INTRODUCTION

This appendix contains three sets of data for each of the two airplanes that were modeled as part of the assessment of program KRASH, modified as described in Section 4.0. Included in this appendix are airplane test data, film analysis data and model mass property, member property and model parameter data.

C.2 AIRPLANE A

C.2.1 Test Data

During the normal course of certifying general aviation airplanes for commercial use a series of tests are performed to show that the airplane is adequately designed to meet FAR 23 requirements. The results of these tests, where available and applicable are presented in Tables C-1 and C-2.

C.2.2 Film Analysis Data

The motion of Airplane A during the crash test was analyzed from 47 frame/second movie film. The test results indicated that the fuselage structure between F.S. 56 and 95 remained intact during the test. Consequently two locations, one located at F.S. 95 and WL 11.50 and the other located at F.S. 56.7 and W.L. 19.10, were used as reference points from which longitudinal and vertical displacements were obtained as a function of time. The change in displacement in a given time frame yields the velocity during that time period. A scale factor is used to translate film measurement into real displacement values. From the displacement data the longitudinal and vertical velocities in feet/second, for the two specified fuselage locations, are calculated. Positive values for displacement and velocity in

the longitudinal direction depict forward motion. Positive values for displacement and velocity in the vertical direction indicate upward motion. Figure C-1 shows a profile view of airplane A and the approximate location of the two fuselage reference points. The film analysis results for the aft door post (Reference point 1 in Figure C-1) are shown in Table C-3. Impact of the airplane with the dirt slope occurs at frame 8 or 9. Each frame represents 21.2 milliseconds of time. The data in Table C-3 indicate a change in forward (longitudinal) velocity of 6.2 ft/sec after nose gear impact. This reduction in speed is due, not to the nose gear impact resulting in the absorption of any significant energy, but to the fact that after the tow cable is released the airplane slows down just before impacting the slope. This is confirmed by the data which shows that the vertical velocity is still zero at spinner impact (frame 8). Table C-4 shows the film analysis results for the aft window (Reference point 2 in Figure C-1). The initial spinner impact velocity is within 2 percent of the value obtained from the aft doorpost film analysis. A 45 ft/sec initial spinner impact velocity was used in the analysis.

Table C-5 shows the results of the film analysis showing the rotation of the tailcone. The data is presented for 600 milliseconds after impact and is substantially more time than is required to evaluate the significant aspects of a crash of this nature. The rotation of the tailcone indicates that a failure occurs after approximately 60 milliseconds.

Table C-6 shows the results of the film analysis depicting fuselage rotation and rotational velocity. The two reference points are joined by a straight line which makes an angle of 11.22 degrees with respect to the airplane water line. The incremental change in this rotational angle is computed for each frame of film analysis. Thus at any instant in time the angle between the aircraft waterline and the ground is determined from the total angle less the reference 11.22 degrees. The rotational velocity is simply the change in rotation divided by the increment in time.

The cabin volume change sequence could not be accurately determined from the film analysis. The deformation of the forward doorpost with

respect to the assumed non-deformed aft doorpost was measured and was considered to represent longitudinal deformation. The upper and lower doorpost deformation was difficult to ascertain due to the absence of a fixed or non-deformable reference point. Consequently, deformation measurements were recorded at two approximate locations; W.L. 2.40 and W.L. 19.1, respectively (See Figure C-1). These locations correspond to the lower aft corner of the doorpost, the door latch and the upper aft corner of the doorpost, respectively. This data is presented in Table C-7.

C.2.2 Math Model Data

Airplane A math model data is presented in Figures C-2 through C-6 for the 35 mass, 69 member model and Figures C-7 through C-11 for the 21 mass, 32 member model. The sequence of presentation for each model is as follows:

- Mass coordinates and properties
- Member properties
- Member damping values
- Member frequencies
- Initial conditions, overall mass and C.G. properties

C.3 AIRPLANE B

C.3.1 Test Data

Applicable test data is presented in Tables C-8 and C-9.

C.3.2 Film Analysis Data

The motion of the Airplane B turnover test was analyzed from 24 frames/second movie film. Two locations on the fuselage, in what is considered non-deformable structure, were selected for performing the film analysis; these locations at F.S. 0.0, W.L. -13.8 and F.S. 110., W.L. 45. are shown in the profile view of Airplane B in Figure C-12. For each frame (every 41.7 milliseconds) longitudinal and vertical displacements were measured with respect to a fixed reference point. A scale factor was established for the purpose of translating film measurements into real displacement values. From the

displacement data the longitudinal and vertical velocities for the two locations on the fuselage were calculated. Positive values for displacement and velocity in the longitudinal direction depict forward motion. Positive values in the vertical direction indicate upward motion. Table C-10 presents the results of the film analysis. The pitch angle at any time of interest can be obtained by taking the rotation value shown in Table C-10 and subtracting 28.19 degrees. Initial impact is shown at time = 0.0. The angle at impact is approximately 38.6 degrees. The c.g. velocity is obtained from rigid body relationships as follows:

$$\dot{X}_{C.G.} = \dot{X}_i - (\cos \theta r_{zi} - \sin \theta r_{xi}) \dot{\theta}$$

$$\dot{Z}_{C.G.} = \dot{Z}_i + (\sin \theta r_{zi} + \cos \theta r_{xi}) \dot{\theta}$$

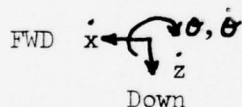
where

$\dot{X}_{C.G.}, \dot{Z}_{C.G.}$ = longitudinal and vertical velocity at C.G., respectively

r_x, r_z = longitudinal and vertical distance from c.g. to location of interest, respectively (+ forward, + down, from c.g.)

$\theta, \dot{\theta}$ = pitch angle (radians) and rate (radians/sec), respectively.

Positive coordinates for $\dot{X}, \dot{Z}, \theta, \dot{\theta}$ are shown below.



The position of the camera used for the film analysis, relative to the airplane is such that after the airplane rotates over onto its turnover structure the angle of impact is difficult to judge. For the airplane to be in a position for both the vertical tail and the forward turnover structure to contact the ground simultaneously the angle theta (θ), shown in Table C-10, should be greater than 190 degrees, (when the reference angle is included). The data presented in Table C-10 is intended to include the turnover contact at approximately 1500 milliseconds after impact. However, the angle associated with this impact (178.55) is distorted due to the positioning of the 24 frame/second camera relative to the airplane. Consequently, still photographs of the airplane at different positions during the latter stages of the overturn (obtained from 1000 frame/second film) and a geometry layout of the

airplane were used to complement the 24 frame/second analysis. Thus, the second impact was determined to occur at approximately 1.5 seconds after impact with an impact angle of 162 degrees and an initial rotational pitch rate of 89.4 degrees/second. The pitch rate corresponds to the average value between 1460 and 1540 milliseconds after impact.

C.3.3 Math Model Data

Airplane B math model data is presented in Figures C-13 through C-17 for the 44 mass, 81 member model and Figures C-18 through C-22 for the 25 mass, 38 member model. These models were used in analyzing the initial impact condition. The sequence of presentation for each model is as follows:

- o Mass coordinates and properties
- o Member properties
- o Member damping values
- o Member frequencies
- o Initial conditions, overall mass and c.g. properties.

Twenty-four mass (37 member) and 43 mass (80 member) math models were used to analyze the second (turnover structure) impact. The 24 mass model is the same as the 25 mass model except for the representation of mass 25 for the vertical tail. Similarly, the 44 mass model differs from the 43 mass model due to the representation of the vertical tail. Consequently, the data for the 24 and 43 mass models are not presented. The initial conditions, mass and c.g. properties for both the 24 mass and 43 mass models are presented in Figures C-23 and C-24, respectively.

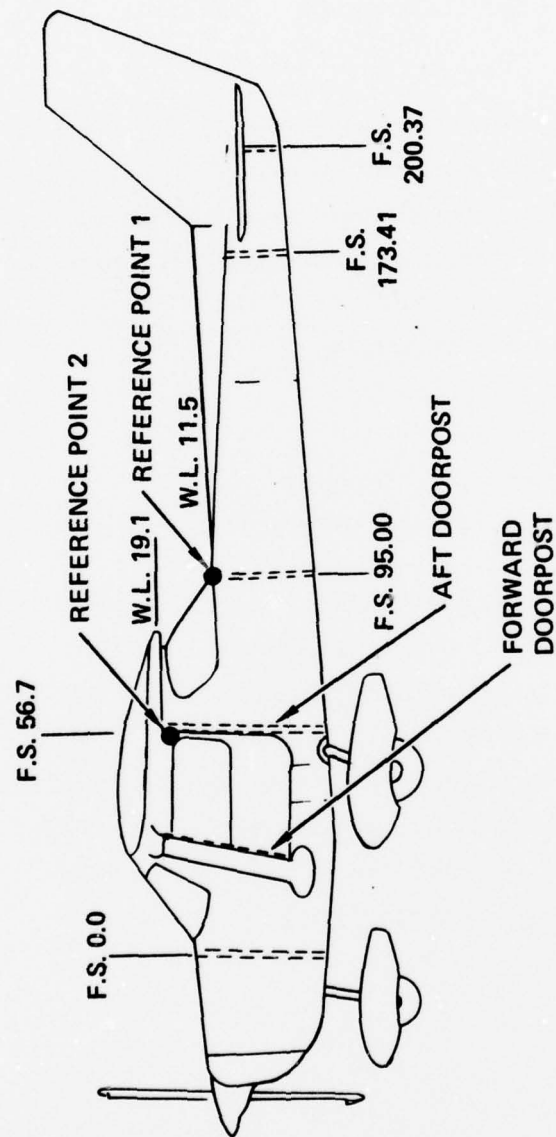


Figure C-1. Profile View of Airplane A

TABLE C-1. AIRPLANE A STRUCTURE TEST LOAD-DEFLECTION DATA

Structure	Design Load (lb.)	Deflection at Design Load (in.)	Rotation at Design Load (deg.)
Engine Mount ^(e)			
Longitudinal	-	-	-
Side	820	.81	.77 (Yaw) ^(d)
Vertical	2456	.41	.76 (Pitch)
Main Landing Gear ^(f)			
Longitudinal	1277	.45	-
Side	1200	-	-
Vertical	3519	5.43	-
Nose Landing Gear ^(g)			
Longitudinal	908	.69	-
Side	794	.32	-
Vertical	1134	-	-
Wing			
Bending (j)	463281 ^(a)	7.56	2.25 (Roll)
Torsion (j)	47826 ^(a)	4.2 ^(b)	5.47
Shear (j)	6155	7.56	2.25 (Roll)
Tailcone ^(h)			
Vertical	591	1.71	.50 (Pitch) ^(c)
Side	542	2.55	.68 (Yaw)

(a) Units: in-lb.

(b) Measured at wing station 180 front spar, relative to wing station 100.

(c) Referenced to F.S. 57.

(d) Referenced to F.S. 0.0

(e) Load point (F.S. 18.5, WL-8.6, B.L. 0.0), deflections and rotations measured relative to firewall (F.S. 0.0)

(f) Load point (F.S. 47.25, WL 34.75, B.L. 38.5), deflections and rotations measured relative to firewall.

(g) Load point (F.S. 10.75, W.L. 45.17, B.L. 0.0), deflections and rotations measured relative to firewall

(h) Load point (F.S. 200), deflections and rotations measured relative to F.S. 57.

(i) Airplane axes apply for all structures except wing.

(j) Load applied at wing station 20.5.

TABLE C-2. AIRPLANE A FUSELAGE TEST VERTICAL LOAD-DEFLECTION DATA

Fuselage Station (F.S.)	Design Load (lb)	Deflection at Design Load (in)	Rotation at Design Load (deg)
0	1083	.09	0
18.5	3396	.125	-
56.	3914	.202	-
71	-	.234	-
95	152	.375	.11 (pitch) ^(a)

(a) Referenced to Firewall F.S. 0.0

TABLE C-3. AIRPLANE A FILM ANALYSIS DATA (Aft Door Post)				
Frame	Vertical (g) Displacement	Vertical (a) Velocity	(g)Longitudinal Displacement	Longitudinal (a) Velocity
5	0.00	0.000	0.635	49.107
6	0.00	0.000	0.635	49.107
7(b)	--	--	0.67	51.814
8(c)	0.00	0.000	0.59	45.627
9(d)	0.02	1.547	0.55	42.534
10	0.07	5.413	0.50	38.667
11	0.11	8.507	0.42	32.481
12	0.09	6.960	0.39	30.161
13	0.08	6.187	0.36	27.841
14	0.09	6.960	0.25	19.334
15	0.15	11.600	0.17	13.147
16	0.12	9.280	0.18	13.920
17	0.06	4.640	0.10	7.734
18	0.10	7.734	0.08	6.187
19	0.07	5.413	0.03	2.320
20	0.10	7.734	0.04	3.093
21	0.07	5.413	0.00	0.000
22	0.06	4.640	0.01	0.773
23	0.08	6.187	0.05	3.867
24	0.05	3.867	0.07	5.413
25	0.08	6.187	0.00	0.000
26	0.05	3.867	-0.03	-2.320
27	0.06	4.640	0.01	0.773
28	0.03	2.320	0.05	3.867
29	0.02	1.547	0.04	3.093
30	-0.01	-0.773	0.01	0.773
(a) $V \text{ (ft/sec)} = \frac{(19.745)(47) \text{ (Displacement)}}{12}$ (b) Nose Gear Impact (c) Spinner Impact (d) Forward Lower Cowl Impact (e) Positive Directions are up and forward (f) Only Frame 5 through 30 Shown (g) Incremental values				

TABLE C-4. AIRPLANE A FILM ANALYSIS DATA (Aft Window)

Frame	Vertical (g) Displacement	Vertical (a) Velocity	(g)Longitudinal Displacement	Longitudinal (a) Velocity
5	--	--	0.605	46.787
6	0.00	0	0.605	46.787
7(b)	0.00	0	0.60	46.400
8(c)	0.00	0	0.60	46.400
9(d)	0.00	0	0.53	40.987
10	0.05	3.867	0.49	37.894
11	0.02	1.547	0.44	34.027
12	0.29	22.427	0.35	27.067
13	0.43	33.254	0.29	22.427
14	0.32	24.747	0.23	17.787
15	0.31	23.974	0.18	13.920
16	0.30	23.200	0.17	13.147
17	0.26	20.107	0.15	11.600
18	0.16	12.374	0.14	10.827
19	0.20	15.467	0.10	7.734
20	0.17	13.147	0.07	5.413
21	0.17	13.147	0.05	3.867
22	0.08	6.187	0.10	7.734
23	0.08	6.187	0.11	8.507
24	0.13	10.054	0.16	12.374
25	0.08	6.187	0.09	6.960
26	0.06	4.640	0.08	6.187
27	0.04	3.093	0.03	2.320
28	0.04	3.093	0.02	1.547
29	0.01	0.773	0.06	4.640
30	0.06	4.640	0.01	0.773
(a) $V(\text{ft/sec}) = \frac{(19.745)(47)(\text{Displacement})}{12}$ (b) Nose Gear Impact (c) Spinner Impact (d) Forward Lower Cowl Impact (e) Positive Directions are Up and Forward (f) Only Frames 5 through 30 Shown (g) Incremental values				

TABLE C-5. AIRPLANE A TAIL CONE FILM ANALYSIS

Time After Spinner Impact(Milliseconds)	Tail Cone Rotation (Degrees) (a)
30	0.0
60	-3.5
90	-13.0
120	-20.5
150	-33.0
180	-42.5
210	-50.5
240	-57.0
270	-62.0
300	-68.5
330	-74.0
360	-80.0
390	-79.0
420	-76.5
450	-76.0
480	-73.0
510	-72.0
540	-72.0
570	-72.0
600	-65.5

(a) Tailcone rotation is with respect to the fuselage. Positive indicates nose down rotation. Negative sign indicates the tail cone angle is below the instantaneous fuselage reference line (water line).

(b) Only Frames 5 through 30 Shown

TABLE C-6. AIRPLANE A FILM ANALYSIS OF FUSELAGE
ROTATION AND ROTATIONAL VELOCITY

Frame	Rotation, θ (a) (Degrees) (b)	Rotational Velocity, $\dot{\theta}$, (Degrees/Second)(b)
5	11.22	0
6	11.22	0
7	11.22	0
8(c)	10.64	0
9	10.64	-4.98
10	10.53	22.64
11	11.01	89.94
12	12.92	98.56
13	15.02	-213.43
14	10.48	-494.67
15	-.04	-321.11
16	-6.87	-218.14
17	-11.51	-258.11
18	-17.00	-298.03
19	-23.34	-157.87
20	-26.70	-168.01
21	-30.27	-112.42
22	-32.66	-175.10
23	-36.39	-68.49
24	-37.85	-76.45
25	-39.48	-165.86
26	-43.01	-109.18
27	-45.33	-31.60
28	-46.00	+52.21
29	-44.89	-31.34
30	-45.56	10.03
(a) Fuselage rotation angle = θ - 11.22°		
(b) Positive indicates nose down rotation		
(c) Spinner Impact		
(d) Only Frames 5 through 30 Shown		

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A METHOD OF ANALYSIS FOR GENERAL AVIATION AIRPLANE STRUCTURAL C--ETC(U)
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TABLE C-7. AIRPLANE A FILM ANALYSIS FOR
CABIN DEFORMATION CHANGE (a)

Time After Impact (Seconds)	Deflection (inches)			
	Incremental at WL 19.10	Cumulative at WL 19.10	Incremental at WL 2.40	Cumulative at WL 2.40
0.0000	0.00	0.00	0.00	0.00
0.0156	0.21	0.20	2.29	2.29
0.0312	0.76	0.97	3.12	5.42
0.0468	0.38	1.35	1.15	6.56
0.0624	0.22	1.57	0.42	6.98
0.0780	0.16	1.73	0.63	7.61
0.0936	0.22	1.95	0.63	8.24
0.1092	0.22	2.17	0.52	8.76
0.1248	0.27	2.44 ^(c)	0.73	9.49
0.1404	-0.06	2.38	0.73	10.22 (c)
0.1560	-0.16	2.22	-0.42	9.84
0.1716	-0.16	2.06	-0.31	9.49
0.1872	-0.11	1.95	-0.21	9.28
0.2028	-0.11	1.84	-0.10	9.18
0.2184	-0.11	1.73	-0.21	8.97
0.2340	0.00	1.73	-0.10	8.87
<p>(a) Deformation of the forward doorpost with respect to the aft doorpost (assumes negligible aft doorpost deformation)</p> <p>(b) Final deflections are:</p> <p>1.20 inches at WL 19.10</p> <p>7.91 inches at WL 2.40</p> <p>7.03 inches at WL -8.00</p> <p>(c) Peak deflection</p>				

MASS DATA

WEIGHTS			MASS COORDINATES F.S.,W.L.,B.L.			MASS MOMENTS OF INERTIA (LB-IN-SEC**2)		
I	W	X**	Y**	Z**	IX	IV	I2	
1	1.030000 01	-1.075000 01	0.00	-3.459000 01	6.400000-01	1.410000 00	6.400000-01	
2	2.025000 01	4.760000 01	3.979000 01	-3.459000 01	8.120000-01	1.797000 00	8.120000-01	
3	2.025000 01	4.760000 01	3.979000 01	-3.459000 01	8.120000-01	1.797000 00	8.120000-01	
4	2.610000 01	5.315000 01	1.400000 01	-1.944000 01	3.780000 00	5.820000 00	5.900000 00	
5	4.519500 01	5.792000 01	2.125000 01	2.544000 01	7.280000 01	4.640000 01	5.040000 01	
6	1.970000 01	2.098000 01	1.628000 01	-1.766000 01	4.900000 00	1.130000 01	1.190000 01	
7	1.970000 01	2.098000 01	1.628000 01	6.440000 00	4.900000 00	1.130000 01	1.190000 01	
8	5.165000 01	2.652000 01	2.125000 01	2.615000 01	8.370000 01	5.968000 01	6.545000 01	
9	2.274400 01	0.00	1.450000 01	-1.972000 00	7.127000 00	1.128000 01	8.850000 00	
10	2.274400 01	0.00	1.450000 01	6.440000 00	7.127000 00	1.128000 01	8.850000 00	
11	2.274400 01	0.00	-1.450000 01	-1.972000 01	7.127000 00	1.128000 01	8.850000 00	
12	2.274400 01	0.00	-1.450000 01	6.440000 00	7.127000 00	1.128000 01	8.850000 00	
13	2.774910 02	-1.642000 01	0.00	-1.850000 00	5.800000 01	7.473000 01	7.648000 01	
14	2.120000 01	-7.500000 00	0.00	-2.296000 01	2.480000 00	2.740000 00	4.820000-01	
15	3.320000 01	2.698000 01	0.00	-1.766000 01	7.318000 00	1.699000 01	1.787000 01	
16	1.970000 01	2.098000 01	-1.628000 01	-1.766000 01	4.900000 00	1.130000 01	1.190000 01	
17	1.970000 01	2.098000 01	-1.628000 01	6.440000 00	4.900000 00	1.130000 01	1.190000 01	
18	5.165000 01	2.652000 01	-2.125000 01	2.615000 01	8.370000 01	5.968000 01	6.545000 01	
19	2.610000 01	5.315000 01	-1.400000 01	-1.944000 01	3.780000 00	5.820000 00	5.900000 00	
20	4.519500 01	5.792000 01	-2.125000 01	2.544000 01	7.280000 01	4.640000 01	5.040000 01	
21	9.637000 00	9.500000 01	-1.200000 01	-1.165000 01	1.510000 00	1.975000 01	1.953000 01	
22	9.637000 00	9.500000 01	-1.200000 01	9.500000 00	1.510000 00	1.975000 01	1.953000 01	
23	3.897000 00	2.652000 01	-1.919700 02	2.712000 01	4.500000-01	1.780000 00	2.147000 00	
24	7.181500 01	2.652000 01	-8.224000 01	2.712000 01	4.680000 02	3.540000 01	5.020000 02	
25	7.181500 01	2.652000 01	8.224000 01	2.712000 01	4.680000 02	3.540000 01	5.020000 02	
26	3.897000 00	2.652000 01	1.919700 02	2.712000 01	4.500000-01	1.780000 00	2.147000 00	
27	6.890000 01	5.315000 01	0.00	-1.944000 01	2.900000 00	4.500000 00	4.500000 00	
28	1.872000 02	5.315000 01	0.00	-7.440000 00	9.300000 00	6.700000 00	1.120000 01	
29	4.000000 01	9.500000 01	0.00	-1.165000 01	1.453000 01	7.310000 01	1.493000 01	
30	9.637000 00	9.500000 01	1.200000 01	-1.165000 01	1.510000 00	1.975000 01	1.953000 01	
31	9.637000 00	9.500000 01	1.225000 01	9.500000 00	1.510000 00	1.975000 01	1.953000 01	
32	6.340000 01	2.003800 02	0.00	5.700000 00	2.670000 01	3.436000 01	4.266000 01	
33	6.000000 01	2.872000 01	-8.224000 01	2.712000 01	3.910000 02	3.020000 01	4.195000 02	
34	6.000000 01	2.872000 01	8.224000 01	2.712000 01	3.910000 02	3.020000 01	4.195000 02	
35	1.360000 02	5.313000 01	0.00	9.560000 00	4.000000 00	3.700000 00	3.300000 00	

Figure C-2 Airplane A 35 Mass, 69 Member Math Model Mass Data

BEAM UNCOUPLED, UNDAMPED FREQUENCIES (CPS)									
I	J	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
1	1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15	15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16	16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
17	17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
18	18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
19	19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20	20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21	21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
22	22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
25	25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
26	26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
27	27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
28	28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
29	29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30	30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
31	31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
32	32	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
33	33	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
34	34	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
35	35	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
36	36	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
37	37	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
38	38	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
39	39	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40	40	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
41	41	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
42	42	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
43	43	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
44	44	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
46	46	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
47	47	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
48	48	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
49	49	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50	50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
51	51	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
52	52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
53	53	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
54	54	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
55	55	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
56	56	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
57	57	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
58	58	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
59	59	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60	60	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
61	61	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
62	62	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
63	63	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
64	64	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
65	65	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
66	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
67	67	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
68	68	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
69	69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Figure C-5 Airplane A 35 Mass, 69 Member Math Model Frequency Data

VEHICLE INITIAL CONDITIONS

VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)
 VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)
 EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)

XGDOT	YGDOT	ZGDOT
P.	Q.	R.
PHI.	THETA.	PSI.
5.40000 02	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0

GENERALIZED SURFACE DATA

BETA = 45.0 DEGREES
 XGIN = 0.0
 ZGIN = 0.0

MODEL PARAMETERS

VEHICLE WT = 1.601820D C3

VEHICLE CG POSITION

X (FS) = 3.65220D 01
 Y (BL) = 5.67750D-16
 Z (WL) = 3.38240D C0

VEHICLE INERTIAS (IN-LR-SEC**2)

I(XX) = 9.43552D 03
 I(VV) = 1.02132D 04
 I(ZZ) = 1.65440D 04

VEHICLE CG INITIAL GROUND COORDINATES

XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE CG, +FORWARD
 ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG, +DOWN
 XCG = -2.97024D 01
 ZCG = -4.29735D 01

Figure C-6 Airplane A 35 Mass, 69 Member Math Model Initial Conditions, Overall Mass and c.g. Properties

MASS DATA

WEIGHTS		MASS COORDINATES F.S.,W.L.,E.L.			MASS MOMENTS OF INERTIA (LB-IN-SEC**2)			
I	W	X**	Y**	Z**	IX	IY	IZ	I
1	1.030000 01	-1.075000 01	0.0	-3.459000 01	6.400000-01	1.410000 00	6.400000-01	1
2	2.021000 01	4.760000 01	3.979000 01	-3.459000 01	8.120000-01	1.797000 00	8.120000-01	2
3	2.024500 01	4.760000 01	-3.979000 01	-3.459000 01	8.120000-01	1.797000 00	8.120000-01	3
4	1.191000 02	5.313000 01	0.0	-1.744000 01	1.404000 01	2.030000 01	1.818000 01	4
5	9.039000 01	5.313000 01	0.0	2.544000 01	1.414000 02	1.159400 02	1.256800 02	5
6	7.260000 01	2.098000 01	0.0	-1.5660 01	1.458600 01	3.384000 01	3.560000 01	6
7	3.540000 01	2.404000 01	0.0	6.440000 00	1.458600 01	3.384000 01	3.560000 01	7
8	1.033000 02	2.652000 01	0.0	2.615000 01	1.983400 02	1.390000 02	1.547200 02	8
9	4.545000 01	0.0	0.0	-1.772000 01	1.425400 01	2.256000 01	1.770000 01	9
10	4.545000 01	0.0	0.0	6.440000 00	1.425400 01	2.256000 01	1.770000 01	10
11	5.927000 01	9.500000 01	0.0	-5.650000 00	3.020000 00	3.904000 01	3.904000 01	11
12	1.527000 01	9.500000 01	0.0	9.500000 00	3.020000 00	3.904000 01	3.904000 01	12
13	2.774900 02	-1.642000 01	0.0	-1.850000 00	5.800000 01	7.473000 01	7.648000 01	13
14	2.120000 01	-7.390000 01	0.0	-2.240000 01	2.480000 00	2.740000 00	4.800000-01	14
15	1.318000 02	2.652000 01	8.224000 01	2.712000 01	6.590000 02	6.560000 01	9.215000 02	15
16	1.318000 02	2.652000 01	-8.224000 01	2.712000 01	6.590000 02	6.560000 01	9.215000 02	16
17	6.340000 01	2.003000 02	0.0	5.700000 00	2.670000 01	3.436000 01	4.266000 01	17
18	1.872000 02	5.313000 01	0.0	-5.440000 00	9.300000 00	6.700000 00	1.120000 01	18
19	3.900000 00	2.652000 01	1.915700 02	2.712000 01	4.500000-01	1.780000 00	2.150000 00	19
20	3.900000 00	2.652000 01	-1.915700 02	2.712000 01	4.500000-01	1.780000 00	2.150000 00	20
21	1.360000 02	5.313000 01	0.0	1.156000 01	4.000000 00	3.700000 00	3.300000 00	21

Figure C-7. Airplane A 21 Mass, 32 Member, Math Model Mass Data

INTERNAL BEAM DATA

BEAM		MODULUS OF ELASTICITY	AREA	MODULUS OF RIGIDITY	MOMENTS OF INERTIA			LENGTH	DAMPING RATIO	BEAM	
IJ	I J	E	A	G	JX	I (YY)	I (ZZ)	XLP	CRAR	IJ	J
1	1	3.00000	7.24100-02	1.10000	1.13300-01	5.66800-02	5.66800-02	1.21060	2.00000-02	1	1
2	2	3.00000	2.07000	1.10000	3.04970	6.84000-02	2.98130	0.0	2.00000-02	2	2
3	3	3.00000	2.07000	1.10000	3.04970	6.84000-02	2.98130	0.0	2.00000-02	3	3
4	4	1.05000	1.04200	4.00000	1.48760	7.40000-01	7.40000-01	4.28800	2.00000-02	4	4
5	5	1.05000	2.95000-01	4.00000	1.79960	8.35200	9.64400	0.1	2.00000-02	5	5
6	6	1.05000	1.62000	4.00000	1.33320	5.48600	7.84600	0.1	2.00000-02	6	6
7	7	1.05000	1.34000	4.00000	3.96000	3.00000	9.60000	0.0	2.00000-02	7	7
8	8	1.05000	3.62000-01	4.00000	3.14000-01	1.90000-01	1.24000-01	4.48020	2.00000-02	8	8
9	9	1.05000	1.71700	4.00000	5.26000	1.20000	4.06000	0.0	2.00000-02	9	9
10	10	1.05000	3.75000-01	4.00000	2.23600-01	6.88000-02	1.54800-01	2.23110	2.00000-02	10	10
11	11	1.05000	1.71700	4.00000	5.25400	1.20000	4.05400	0.0	2.00000-02	11	11
12	12	1.05000	4.00000-01	4.00000	5.32600-01	3.60000-02	4.96600-01	2.40400	2.00000-02	12	12
13	13	1.05000	3.14500	4.00000	4.65820	3.27500	4.33070	0.2	2.00000-02	13	13
14	14	1.05000	3.16500	4.00000	4.65820	3.27500	4.33070	0.2	2.00000-02	14	14
15	15	3.00000	2.92000-01	1.10000	1.82000-01	1.32000-01	5.00000-02	2.41600	2.00000-02	15	15
16	16	3.00000	1.40000-01	1.10000	1.44000	7.20000-01	7.20000-01	2.31980	2.00000-02	16	16
17	17	3.00000	2.16000-01	1.10000	2.68000-02	1.34000-02	1.34000-02	9.04920	2.00000-02	17	17
18	18	3.00000	1.40000-01	1.10000	1.44000	7.20000-01	7.20000-01	1.68420	2.00000-02	18	18
19	19	3.00000	2.16000-01	1.10000	2.68000-02	1.34000-02	1.34000-02	3.63150	2.00000-02	19	19
20	20	1.05000	2.27400-01	4.00000	1.52000-01	1.40000-01	1.20000-02	1.91500	2.00000-02	20	20
21	21	1.05000	6.00000-01	4.00000	1.40000	7.00000	7.00000	1.06490	2.00000-02	21	21
22	22	1.05000	6.00000-01	4.00000	1.70000	7.00000	7.00000	1.05450	2.00000-02	22	22
23	23	3.00000	4.00000-01	1.10000	2.03000	1.50000	5.50000	0.0	2.00000-02	23	23
24	24	1.05000	1.74400	4.00000	2.33300	0.0	4.65000-01	9.28670	2.00000-02	24	24
25	25	1.05000	1.74400	4.00000	2.33300	0.0	4.65000-01	9.28670	2.00000-02	25	25
26	26	1.05000	3.06800	4.00000	2.60600	1.99200	2.40760	0.2	2.00000-02	26	26
27	27	1.05000	3.06800	4.00000	2.60600	1.99200	2.40760	0.2	2.00000-02	27	27
28	28	1.05000	3.06800	4.00000	3.63400	2.64000	3.57000	0.2	2.00000-02	28	28
29	29	1.05000	3.06800	4.00000	3.63400	2.64000	3.57000	0.2	2.00000-02	29	29
30	30	1.05000	4.00000-01	4.00000	0.0	0.0	0.0	3.40830	2.00000-02	30	30
31	31	1.05000	2.25200-03	5.00000	2.00000	1.00000	1.00000	1.70000	1.94600-01	31	31
32	32	1.05000	6.00000-01	4.00000	0.0	0.0	0.0	5.46300	2.00000-02	32	32

Figure C-8. Airplane A 21 Mass, 32 Member, Math Model Member Property Data

DAMPING TERMS (LD/IN/SEC, TRANSLATIONS (1))-(3) AND LB-IN-SEC, ROTATIONS (4))-(6))		(1)	(2)	(3)	(4)	(5)	(6)
1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2
3	3	3	3	3	3	3	3
4	4	4	4	4	4	4	4
5	5	5	5	5	5	5	5
6	6	6	6	6	6	6	6
7	7	7	7	7	7	7	7
8	8	8	8	8	8	8	8
9	9	9	9	9	9	9	9
10	10	10	10	10	10	10	10
11	11	11	11	11	11	11	11
12	12	12	12	12	12	12	12
13	13	13	13	13	13	13	13
14	14	14	14	14	14	14	14
15	15	15	15	15	15	15	15
16	16	16	16	16	16	16	16
17	17	17	17	17	17	17	17
18	18	18	18	18	18	18	18
19	19	19	19	19	19	19	19
20	20	20	20	20	20	20	20
21	21	21	21	21	21	21	21
22	22	22	22	22	22	22	22
23	23	23	23	23	23	23	23
24	24	24	24	24	24	24	24
25	25	25	25	25	25	25	25
26	26	26	26	26	26	26	26
27	27	27	27	27	27	27	27
28	28	28	28	28	28	28	28
29	29	29	29	29	29	29	29
30	30	30	30	30	30	30	30
31	31	31	31	31	31	31	31
32	32	32	32	32	32	32	32
1	1	4.85390 00	1.22510 00	1.22510 00	1.44907 01	6.10795 01	5.16359 01
2	2	2.05730 01	2.72747 00	4.13129 01	1.62549 02	6.71317 01	5.04581 02
3	3	2.86573 01	2.72747 00	4.13129 01	1.62549 02	6.71317 01	5.05127 02
4	4	1.52364 01	1.01858 00	1.01339 00	1.78721 02	3.97409 02	4.79130 02
5	5	8.74323 00	1.70072 01	1.58271 01	1.01325 03	3.07146 03	3.26769 03
6	6	1.72370 01	9.72768 00	8.13417 00	6.07216 02	2.26642 03	2.63013 03
7	7	2.04005 01	7.17512 00	1.26646 01	1.50251 03	4.39401 03	2.60714 03
8	8	6.21018 00	2.81034 01	3.47876 01	9.04433 01	2.10161 02	1.74387 02
9	9	1.50691 01	4.62446 00	2.51414 00	3.25942 02	4.94420 02	6.06312 02
10	10	7.56203 00	1.00954 00	6.73024 01	4.42530 01	1.11218 02	1.61821 02
11	11	2.31697 01	6.28270 00	3.37771 00	5.68129 02	6.37611 02	1.70738 03
12	12	8.67240 01	1.45810 00	3.38954 01	6.39471 01	7.53370 01	2.72010 02
13	13	1.84440 01	5.77840 00	2.68859 00	2.72411 03	5.31913 03	1.95134 04
14	14	1.84440 01	9.77647 00	2.68859 00	2.72411 03	5.31913 03	1.95134 04
15	15	1.16438 01	6.82812 01	1.12731 00	6.85080 01	2.17557 02	1.06432 02
16	16	1.50691 01	5.27479 00	5.27242 00	3.03249 02	7.61424 02	7.07165 02
17	17	1.40021 01	1.33929 00	1.33929 00	2.94100 01	8.47652 01	7.08921 01
18	18	1.71755 01	7.20281 00	7.20281 00	3.20777 02	8.44872 02	8.12311 02
19	19	7.65723 00	2.18740 01	2.18740 01	1.67790 01	4.63360 01	3.77824 01
20	20	6.37131 00	2.64750 01	9.04314 01	6.29792 01	1.95855 02	1.59481 01
21	21	5.48477 00	6.09404 01	6.09404 01	1.60980 02	5.63407 02	5.96755 02
22	22	4.52483 00	6.06840 01	5.07210 01	1.75312 02	5.72218 02	7.21267 02
23	23	3.55024 01	3.74478 01	6.29907 01	4.35276 02	2.54558 03	1.40685 03
24	24	1.31097 01	2.41968 01	0.0	2.13760 02	0.0	5.10941 02
25	25	1.31097 01	2.41968 01	0.0	2.13760 02	0.0	5.10941 02
26	26	1.79134 01	3.54332 00	1.03374 00	1.01215 03	3.23800 03	1.16690 04
27	27	1.79134 01	3.54332 00	1.03374 00	1.01215 03	3.23800 03	1.16690 04
28	28	8.09944 00	1.50981 00	4.22595 01	1.19480 03	1.28763 03	2.86477 03
29	29	8.09944 00	1.50981 00	4.22595 01	1.19480 03	1.28763 03	2.86477 03
30	30	6.37131 00	0.0	0.0	0.0	0.0	0.0
31	31	1.52425 01	5.70346 01	1.13660 03	1.97283 03	2.23100 03	2.23100 03
32	32	1.45837 00	0.0	0.0	0.0	0.0	0.0

Figure C-9. Airplane A 21 Mass, 32 Member, Math Model Damping Data

BEAM UNCOUPLED, UNDAMPED FREQUENCIES (CPS)							
		(1)		(2)		(3)	
		(4)		(5)		(6)	
I	J	(1)	(2)	(3)	(4)	(5)	(6)
1	1	2.36660 02	5.97510 01	5.97510 01	2.89180 01	5.85610 01	1.12730 02
2	2	3.15840 02	3.61600 01	4.55320 00	3.61920 01	1.46770 01	1.04520 02
3	3	3.15840 02	3.60600 01	4.55320 00	3.61920 01	1.46770 01	1.04520 02
4	4	1.11710 02	7.46740 00	7.42940 00	4.23450 00	1.16090 01	1.13550 01
5	4	7.00460 01	1.36250 02	1.26650 02	1.40650 02	2.25770 02	2.43410 02
6	4	1.46420 02	8.37570 01	7.00370 01	1.36350 02	1.51970 02	1.85060 02
7	5	1.63350 02	5.68560 01	1.00560 02	1.99100 01	6.85780 01	3.69910 01
8	5	6.44750 01	3.53590 00	4.87210 00	1.95560 00	5.39560 00	4.22800 00
9	6	2.65600 02	6.34130 01	3.44750 01	2.86160 01	2.90770 01	5.21450 01
10	6	1.24360 02	1.31190 01	8.75290 00	6.10440 00	7.84610 00	1.21070 01
11	7	2.45360 02	6.68160 01	5.63520 01	1.12190 01	1.92820 01	3.37750 01
12	7	1.57000 02	2.27760 01	6.13230 00	8.82240 00	5.31480 00	2.03060 01
13	8	1.29630 02	6.36680 01	1.75630 01	2.32570 01	4.55030 01	7.21470 01
14	8	1.29630 02	6.36680 01	1.75630 01	2.32570 01	4.55030 01	7.21470 01
15	9	1.97400 02	1.17120 01	1.90300 01	8.58070 00	1.91650 01	1.33300 01
16	9	7.45320 01	2.50710 01	2.50710 01	1.54720 01	3.11400 01	3.16500 01
17	9	5.22840 02	3.08430 01	3.08430 01	7.01840 00	1.33310 01	1.57260 01
18	10	6.21470 01	5.42500 01	3.42500 01	1.71670 01	3.45530 01	3.51190 01
19	10	1.77030 02	5.03860 00	5.03860 00	3.83670 00	7.28750 00	8.59690 00
20	11	1.24590 02	5.17720 00	1.76830 01	1.15390 01	9.98060 00	2.92200 00
21	11	6.16680 01	7.62960 00	7.62960 00	2.11700 01	3.08660 01	2.92570 01
22	12	1.78670 02	1.12740 01	9.43220 00	2.34440 01	3.10190 01	3.51410 01
23	4	1.78670 02	1.87740 02	3.15840 02	1.42110 02	3.75130 02	2.13760 02
24	6	9.85030 01	1.87070 00	0.0	1.70700 00	0.0	2.35920 00
25	6	9.85030 01	1.87070 00	0.0	1.70700 00	0.0	2.35920 00
26	15	1.46150 02	4.06740 01	1.16990 01	1.67350 01	5.35380 01	5.02710 01
27	16	1.46150 02	4.06740 01	1.16990 01	1.67350 01	5.35380 01	5.02710 01
28	5	1.31920 02	2.44930 01	6.68330 00	3.22770 01	3.50660 01	1.20300 02
29	5	1.31920 02	2.44930 01	6.68330 00	3.22770 01	3.50660 01	1.20300 02
30	7	1.14140 02	0.0	0.0	0.0	0.0	0.0
31	18	6.48680 00	4.78540 01	2.78540 01	3.34710 01	7.75720 01	6.56960 01
32	5	8.67990 01	0.0	0.0	0.0	0.0	0.0

Figure C-10 Airplane A 21 Mass, 32 Member Math Model Frequency Data

VEHICLE INITIAL CONDITIONS

VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)
 VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)
 EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)

XGDOT	YGDOT	ZGDOT
P.	Q.	R.
PHI.	THETA.	PSI.
5.400000 02	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0

GENERALIZED SURFACE DATA

BETA = 45.0 DEGREES
 XGIN = 0.0
 ZGIN = 0.0

MODEL PARAMETERS

VEHICLE WT = 1.6018000 03

VEHICLE CG POSITION

X (FS) = 3.610930 01
 Y (BL) = 0.0
 Z (WL) = 4.155810 00

VEHICLE INERTIAS (IN-LB-SEC**2)

I(XX) = 9.645770 03
 I(YY) = 1.015880 04
 I(ZZ) = 1.618660 04

VEHICLE CG INITIAL GROUND COORDINATES

XCG IS THE DISTANCE FROM SLOPE/CGGROUND INTERSECTION TO VEHICLE CG,+FORWARD
 ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG,+DOWN
 XCG = -2.928970 01
 ZCG = -4.374060 01

Figure C-11. Airplane A 21 Mass, 32 Member Math Model Initial Conditions, Overall Mass and c.g. properties

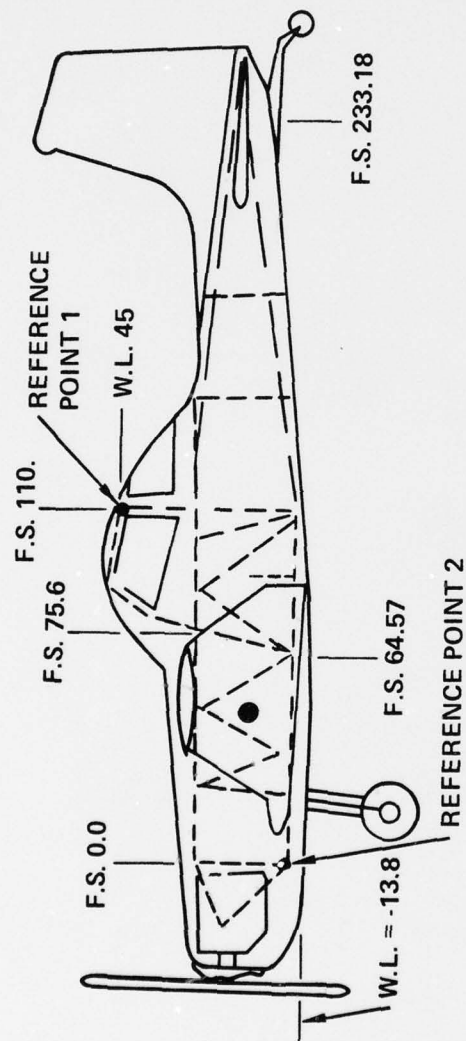


Figure C-12. Profile View of Airplane B

TABLE C-8. AIRPLANE B STRUCTURE TEST LOAD-DEFLECTION DATA

Structure	Design Load (lb.)	Deflection at Design Load (in.)	Rotation at Design Load (deg.)
Engine Mount ^(e)			
longitudinal	716	NA	
side	1221	.24	.75 (yaw)
vertical	3489	.65	2.03 (pitch) ^(d)
Main Landing Gear ^(f)			
longitudinal	2427	2.44 ^(j)	NA
side	2475	NA	NA
vertical	7755	NA	NA
Tail Gear ^(g)			
longitudinal	542	NA	NA
side	794	4.04	NA
vertical	2364	3.06	NA
Wing ⁽ⁱ⁾			
bending	921,365 ^(a)	10.25 ^(b)	3.17 (roll)
torque	73,200	3.44	6.33 (pitch)
shear	8,616	10.25	3.17 (roll)
Tailcone Bending ^(h)			
vertical	802	4.75	1.48 (pitch) ^(c)
side	918	4.04	1.26 (roll)

(a) Units: in-lb

(b) Measured at wing station 238 Front spar, relative to wing station 192

(c) Referenced to F.S. 49

(d) Referenced to F.S. 0.0

(e) Loads points are: (F.S. 18.35, W.L. 3.9, LBL 3.8), deflection and rotations referenced to F.S. 0.0.

(f) Loads points are: (F.S. 17.84, W.L. 44.95, LBL 47.97), deflection and rotations referenced to F.S. 0.0.

(g) Loads points are: (F.S. 26.4, W.L. 4.76, BL 0.0), deflection and rotations referenced to F.S. 0.0.

(h) Loads points are: (F.S. 217.0, W.L. 47.47), deflections and rotations measured relative to F.S. 49.

(i) Airplane axes apply for all structures except wing.

(j) NA means not available

TABLE C-9. AIRPLANE B FUSELAGE TEST VERTICAL LOAD-DEFLECTION DATA

Fuselage Station F.S.	Design Load (lb)	Deflection at Design Load (in)	Rotation at Design Load (deg)
-12.18	7603	1.68	.52
33.58	1544	1.25	.39
59.15	2359	1.81	.56 ^(a)
96.63	1479	2.11	.66
157.61	163	3.00	.93
(a) Referenced to F.S. 49 (pitch direction)			

TABLE C-10. AIRPLANE B FILM ANALYSIS DATA

Time, Milliseconds	Reference Point 1(b)		Reference Point 2(c)		Rotation, Degrees (g)	Rotational Velocity (θ) (Deg/sec) (g)
	V_L (ft/sec) (e)	V_V (ft/sec) (f)	V_L (ft/sec) (e)	V_V (ft/sec) (f)		
875.0	44.55	0.60	44.55	0.60	28.19 (a)	0.0
750.0	39.92	-0.60	39.92	2.34	29.31	14.64
625.0	39.92	1.15	39.92	2.88	30.83	7.92
500.0	34.16	-2.26	37.27	3.39	33.98	33.84
375.0	31.65	-4.98	33.66	3.32	39.87	40.08
250.0	28.21	-3.21	36.78	5.88	46.08	62.88
125.0	22.28	-3.56	35.65	5.08	55.15	80.64
0.0 (d)	13.73	-4.90	35.31	2.45	66.80	119.28
-125.0	14.57	-1.98	27.69	1.98	79.20	72.24
-250.0	6.26	6.99	19.74	6.00	87.65	69.12
-375.0	7.66	7.53	27.24	4.02	94.64	51.36
-500.0	7.19	0.00	16.77	0.00	100.36	48.96
-625.0	3.83	1.02	21.98	-3.57	106.01	46.56
-750.0	0.96	0.51	14.85	-6.13	114.64	81.60
-875.0	4.31	1.53	14.37	-10.22	124.80	82.76
-1000.0	5.75	-4.60	6.23	-11.76	131.39	30.48
-1125.0	5.27	1.53	22.45	-11.25	139.96	93.10
-1250.0	5.27	0.51	11.98	-15.34	153.57	117.60
-1375.0	8.14	-1.53	8.62	-13.80	167.31	84.96
-1500.0	1.92	-7.16	1.44	-18.91	178.55	83.52
-1540.0	0.48	1.02	0.48	-15.85	182.54	95.76

(a) Initial Reference Rotation angle is 28.19 Degrees. Pitch Angle at anytime $\theta = 28.19^\circ$
(b) Reference Point 1 is located at F.S. 0.0, WL -13.80
(c) Reference Point 2 is located at F.S. 110.0, WL 45.0
(d) Time = 0.0 occurs at nose impact. Negative sign refers to post impact period.
(e) V_L = Longitudinal Velocity (positive in forward direction)
(f) V_V = Vertical Velocity (positive in up direction)
(g) Positive θ indicates nose down pitch

MASS DATA

WEIGHTS		MASS COORDINATES F.S.,W.L.,E.L.			MASS MOMENTS OF INERTIA (LE-IN-SEC**2)			
I	W	X**	Y**	Z**	IX	IY	IZ	
1	1.230000 02	2.331870 02	0.0	1.500000 01	2.669300 01	3.436000 01	4.266000 01	1
2	3.970000 01	1.737700 01	-4.042500 01	-4.716500 01	2.310000 01	2.477000 01	1.646700 01	2
3	3.970000 01	1.737700 01	4.042500 01	-4.716500 01	2.310000 01	2.477000 01	1.646700 01	3
4	1.694000 01	8.925000 01	1.673700 01	-8.963000 00	7.956000 00	4.542000 00	1.396000 00	4
5	1.092500 02	6.457000 01	2.000000 01	-1.027500 01	8.360000 01	1.730000 01	9.113000 01	5
6	4.088000 01	7.209000 01	1.975000 01	2.050000 01	4.750000 00	7.216000 00	6.600000 00	6
7	7.094000 01	2.357000 01	1.802600 01	-8.917000 00	1.386000 02	5.806000 01	1.160000 02	7
8	7.924000 01	2.357000 01	1.932000 01	1.455400 01	1.043300 02	1.008000 01	1.042700 02	8
9	2.200000 01	8.750000-01	1.619000 01	-1.818500 01	3.310000 00	1.068700 01	1.068700 01	9
10	1.112200 02	8.750000-01	1.844000 01	1.184900 01	4.830000 00	2.240400 01	1.910000 01	10
11	5.597000 02	-1.903200 01	0.0	3.072000 00	2.285360 02	2.793860 02	3.536100 02	11
12	9.624000 01	8.750000-01	-1.619000 01	-1.818500 01	4.160000 00	1.661000 01	1.545400 01	12
13	8.920000 01	8.750000-01	-1.844000 01	1.164900 01	1.717100 02	7.196500 01	1.427700 02	13
14	7.094000 01	2.357000 01	-1.802600 01	-8.917000 00	1.695870 02	1.206300 01	1.695870 02	14
15	7.924000 01	2.357000 01	-1.932000 01	1.455400 01	1.003670 02	2.076000 01	1.093580 02	15
16	1.092500 02	6.457000 01	-2.000000 01	-1.027500 01	3.100000 00	5.470000 00	4.777000 00	16
17	7.924000 01	6.457000 01	0.0	-1.027500 01	5.710000 00	8.658000 00	7.928000 00	17
18	3.084000 01	7.209000 01	-1.975000 01	2.050000 01	2.960000 00	4.542000 00	1.369000 00	18
19	1.694000 01	8.925000 01	-1.673700 01	-8.963000 00	2.092000 01	4.360000 01	1.853000 01	19
20	3.000000 01	8.087000 01	0.0	-2.360000 00	3.196000 00	1.077400 01	9.708000 00	20
21	1.385000 01	1.101800 02	-1.375800 01	-7.850000 00	7.393000 00	1.700000 01	1.086300 01	21
22	1.779000 01	1.101800 02	0.0	-7.850000 00	2.963000 00	1.191400 01	1.017800 01	22
23	1.438000 01	1.101800 02	-1.509000 01	2.480000 01	6.845000 00	6.083000 00	4.196000 00	23
24	1.566000 01	8.463000 01	-8.580000 00	4.731000 01	1.175000 00	2.312000 00	2.462000 00	24
25	5.900000 00	1.101800 02	-6.740000 00	4.581000 01	6.845000 00	6.083000 00	4.196000 00	25
26	1.569000 01	8.463000 01	8.580000 00	4.731000 01	1.175000 00	2.312000 00	2.462000 00	26
27	5.910000 00	1.101800 02	6.740000 00	4.581000 01	4.680000 02	3.540000 01	5.020000 02	27
28	9.306000 01	3.358000 01	1.210700 02	-2.500000 00	4.500000-01	1.780000 00	2.150000 00	28
29	1.770000 01	4.300000 01	2.369800 02	1.045000 01	4.680000 02	3.540000 01	5.020000 02	29
30	9.306000 01	3.358000 01	-1.210700 02	-2.500000 00	4.500000-01	1.780000 00	2.150000 00	30
31	1.770000 01	4.300000 01	2.369800 02	1.045000 01	3.196000 00	1.077400 01	9.708000 00	31
32	1.325000 01	1.101800 02	1.376000 01	-7.850000 00	2.963000 00	1.191400 01	1.017800 01	32
33	1.438000 01	1.101800 02	1.509000 01	2.480000 01	6.845000 00	6.083000 00	4.196000 00	33
34	1.700000 02	8.087000 01	0.0	-2.360000 00	3.196000 00	1.077400 01	9.708000 00	34
35	3.450000 01	2.357000 01	0.0	-8.917000 00	1.272000 00	2.656000 00	2.656000 00	35
36	1.650000 01	3.657000 01	1.876000 01	-9.400000 00	6.630000 01	1.853700 01	6.233000 01	36
37	1.650000 01	4.357000 01	1.950000 01	1.750000 01	6.630000 01	1.853700 01	6.233000 01	37
38	9.700000 00	8.154000 01	1.630000 01	2.160000 01	2.300000 00	8.300000 00	4.700000 00	38
39	9.700000 00	1.007000 02	1.860000 01	2.370000 01	2.300000 00	8.300000 00	4.700000 00	39
40	1.650000 01	3.657000 01	-1.870000 01	-9.400000 00	6.630000 01	1.853700 01	6.233000 01	40
41	1.650000 01	4.357000 01	-1.950000 01	1.750000 01	6.630000 01	1.853700 01	6.233000 01	41
42	9.700000 00	8.154000 01	1.630000 01	2.160000 01	2.300000 00	8.300000 00	4.700000 00	42
43	9.700000 00	1.007000 02	-1.876000 01	-9.400000 00	2.300000 00	8.300000 00	4.700000 00	43
44	1.470000 01	2.332000 02	0.0	7.700000 01	6.400000 00	1.420000 01	6.400000 00	44

Figure C-13. Airplane B 44 Mass, 81 Member Math Model Mass Data.

BEAM			MODULUS OF ELASTICITY	AREA	MODULUS OF RIGIDITY	MOMENTS OF INERTIA			LENGTH	DAMPING RATIO	BEAM		
IJ	I	J	E	A	G	IX	I(YY)	I(ZZ)	XLB	CBAR	IJ	I	J
1	1	32	1.05000 07	1.01050 00	4.00000 06	5.25000 01	2.59500 01	6.49000 00	1.25870 02	1.00000-02	1	1	32
2	1	33	1.05000 07	1.57070 00	4.00000 06	5.25000 01	4.07100 01	1.19700 01	1.24320 02	1.00000-02	2	1	33
3	1	21	1.05000 07	1.01050 00	4.00000 06	5.25000 01	2.59500 01	6.49000 00	1.25670 02	1.00000-02	3	1	21
4	1	23	1.05000 07	1.57070 00	4.00000 06	5.25000 01	4.07100 01	1.19700 01	1.24320 02	1.00000-02	4	1	23
5	2	14	3.00000 07	3.43620 00	1.10000 07	5.31100 00	1.89000-01	5.12160 00	4.47550 01	1.00000-02	5	2	14
6	3	7	3.00000 07	3.43620 00	1.10000 07	5.31100 00	1.89000-01	5.12160 00	4.47550 01	1.00000-02	6	3	7
7	4	5	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.49290 01	1.00000-02	7	4	5
8	4	32	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.11700 01	1.00000-02	8	4	32
9	4	20	2.90000 07	1.26100-01	1.10000 07	1.52000-02	7.60000-03	7.60000-03	1.98420 01	1.00000-02	9	4	20
10	5	6	2.90000 07	1.78300-01	1.10000 07	3.81120 00	3.47560 00	3.35600-01	3.16810 01	1.00000-02	10	5	6
11	5	36	2.90000 07	2.92800-01	1.10000 07	2.10050 00	2.05940 00	4.11000-02	2.80440 01	1.00000-02	11	5	36
12	5	17	2.90000 07	6.55500-01	1.10000 07	8.40270 00	7.98370 00	4.19000-01	2.00000 01	1.00000-02	12	5	17
13	6	37	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.86780 01	1.00000-02	13	6	37
14	6	18	2.90000 07	2.11300-01	1.10000 07	8.89550 00	8.41690 00	4.78600-01	3.95000 01	1.00000-02	14	6	18
15	6	26	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	3.16350 01	1.00000-02	15	6	26
16	6	38	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	1.01200 01	1.00000-02	16	6	38
17	7	8	2.90000 07	3.17100-01	1.10000 07	3.21510 00	7.11000-02	3.14400 00	2.35070 01	1.00000-02	17	7	8
18	7	9	2.90000 07	3.18100-01	1.10000 07	2.36160 00	2.32260 00	3.90000-02	2.45630 01	1.00000-02	18	7	9
19	7	30	1.05000 07	3.10240 00	4.00000 06	6.36670 02	2.59400 01	6.10730 02	1.39600 02	1.00000-02	19	7	30
20	7	35	2.90000 07	1.24460 00	1.10000 07	8.64070 01	2.57890 01	6.12180 01	1.80260 01	1.00000-02	20	7	35
21	8	10	2.90000 07	2.35100-01	1.10000 07	8.74400-01	6.78000-01	1.96400-01	2.28730 01	1.00000-02	21	8	10
22	8	15	2.90000 07	4.67300-01	1.10000 07	3.76000-01	1.88000-01	1.88000-01	3.86400 01	1.00000-02	22	8	15
23	8	30	2.90000 07	1.36680 00	1.10000 07	5.26270 00	0.00	4.21710 00	1.41780 02	1.00000-02	23	8	30
24	9	10	2.90000 07	3.08700-01	1.10000 07	3.76000-02	1.88000-02	1.88000-02	3.01110 01	1.00000-02	24	9	10
25	9	11	2.90000 07	3.62300-01	1.10000 07	1.90000-01	9.50000-02	9.50000-02	3.33210 01	1.00000-02	25	9	11
26	9	12	2.90000 07	1.29700-01	1.10000 07	2.40040 00	2.39400 00	6.40000-03	3.23800 01	1.00000-02	26	9	12
27	10	11	2.90000 07	1.27200-01	1.10000 07	1.90000-01	9.50000-02	9.50000-02	2.85190 01	1.00000-02	27	10	11
28	10	13	2.90000 07	7.86000-02	1.10000 07	1.00000-02	5.00000-03	5.00000-03	3.68600 01	1.00000-02	28	10	13
29	11	12	2.90000 07	3.62300-01	1.10000 07	1.90000-01	9.50000-02	9.50000-02	3.33210 01	1.00000-02	29	11	12
30	11	13	2.90000 07	1.27200-01	1.10000 07	1.90000-01	9.50000-02	9.50000-02	2.85190 01	1.00000-02	30	11	13
31	12	13	2.90000 07	1.79200-01	1.10000 07	3.60000-02	1.80000-02	1.80000-02	3.01180 01	1.00000-02	31	12	13
32	12	14	2.90000 07	3.18100-01	1.10000 07	2.36160 00	2.32260 00	3.90000-02	2.45630 01	1.00000-02	32	12	14
33	13	15	2.90000 07	2.35100-02	1.10000 07	8.74600-01	6.78000-01	1.96600-01	2.28730 01	1.00000-02	33	13	15
34	14	15	2.90000 07	3.17100-01	1.10000 07	6.35910 00	3.21510 00	3.14400 00	2.35070 01	1.00000-02	34	14	15
35	14	40	2.90000 07	2.92800-01	1.10000 07	2.10050 00	2.05940 00	4.11000-02	2.80440 01	1.00000-02	35	14	40
36	14	28	1.05000 07	1.02400-01	4.00000 06	6.36670 02	2.59400 01	6.10730 02	1.39600 02	1.00000-02	36	14	28
37	15	41	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.02170 01	1.00000-02	37	15	41
38	15	28	2.90000 07	1.36680 00	1.10000 07	5.26270 00	0.00	4.21710 00	1.41780 02	1.00000-02	38	15	28
39	16	17	2.90000 07	6.55000-01	1.10000 07	8.40270 00	7.98370 00	4.19000-01	2.00000 01	1.00000-02	39	16	17
40	16	18	2.90000 07	1.78300-01	1.10000 07	3.81250 00	3.47560 00	3.35600-01	3.16810 01	1.00000-02	40	16	18
41	16	19	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.49290 01	1.00000-02	41	16	19
42	16	42	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	1.01200 01	1.00000-02	42	16	42
43	18	24	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	3.16350 01	1.00000-02	43	18	24
44	19	20	2.90000 07	1.26100-01	1.10000 07	1.52000-02	7.60000-03	7.60000-03	1.98420 01	1.00000-02	44	19	20
45	19	21	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.11700 01	1.00000-02	45	19	21
46	21	22	2.90000 07	6.49000-02	1.10000 07	5.60000-03	2.80000-03	2.80000-03	1.37580 01	1.00000-02	46	21	22
47	21	23	2.90000 07	1.29800-01	1.10000 07	2.05720 00	1.91960 00	1.37600-01	1.37580 01	1.00000-02	47	21	23
48	23	25	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.26080 01	1.00000-02	48	23	25
49	24	25	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.86960 01	1.00000-02	49	24	25
50	24	26	2.90000 07	2.25000-01	1.10000 07	9.09100-01	6.64200-01	2.44900-01	1.72600 01	1.00000-02	50	24	26
51	25	27	2.90000 07	1.16000-01	1.10000 07	1.49400-01	1.43000-01	6.40000-03	1.74800 01	1.00000-02	51	25	27
52	26	27	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.56800 01	1.00000-02	52	26	27
53	28	29	1.05000 07	3.10240 00	4.00000 06	6.36670 02	2.59400 01	6.10730 02	1.39600 02	1.00000-02	53	28	29
54	30	31	1.05000 07	3.10240 00	4.00000 06	6.36670 02	2.59400 01	6.10730 02	1.39600 02	1.00000-02	54	30	31
55	32	33	2.90000 07	1.29800-01	1.10000 07	2.05720 00	1.91960 00	1.37600-01	1.37580 01	1.00000-02	55	32	33
56	22	32	2.90000 07	6.49000-02	1.10000 07	5.60000-03	2.80000-03	2.80000-03	1.37600 01	1.00000-02	56	22	32
57	23	33	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	3.01180 01	1.00000-02	57	23	33
58	27	33	2.90000 07	6.49000-02	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.26080 01	1.00000-02	58	27	33
59	14	35	2.90000 07	1.24460 00	1.10000 07	8.64070 01	2.57890 01	6.12180 01	1.80260 01	1.00000-02	59	14	35
60	20	34	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	1.43800 01	1.00000-02	60	20	34
61	7	36	2.90000 07	1.78300-01	1.10000 07	3.81120 00	3.47560 00	3.35600-01	1.30260 01	1.00000-02	61	7	36
62	8	36	2.90000 07	1.78300-01	1.10000 07	3.81120 00	3.47560 00	3.35600-01	2.72610 01	1.00000-02	62	8	36
63	36	37	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.78070 01	1.00000-02	63	36	37
64	5	37	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	3.48240 01	1.00000-02	64	5	37
65	8	37	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.02170 01	1.00000-02	65	8	37
66	38	39	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	1.94110 01	1.00000-02	66	38	39
67	33	39	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	1.01690 01	1.00000-02	67	33	39
68	32	38	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	4.11580 01	1.00000-02	68	32	38
69	32	39	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	3.32970 01	1.00000-02	69	32	39
70	5	38	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	3.63000 01	1.00000-02	70	5	38
71	18	41	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.86780 01	1.00000-02	71	18	41
72	16	40	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.80440 01	1.00000-02	72	16	40
73	15	40	2.90000 07	1.46400-01	1.10000 07	3.32000-02	1.66000-02	1.66000-02	2.72610 01	1.00000-02	73	15	40
74	40	41</											

DAMPING TERMS (LB/IN/SEC, TRANSLATIONS (1)-(3) AND LB-IN-SEC, ROTATIONS (4)-(6))									
I	J	(1)	(2)	(3)	(4)	(5)	(6)		
1	1	32	3.450050 00	2.406370-01	4.811810-01	1.127220 02	3.945600 02	2.114820 02	
2	1	33	4.345970 00	3.343110-01	6.165310-01	1.427270 02	5.032120 02	2.919590 02	
3	1	21	3.457640 00	2.411670-01	4.822410-01	1.127220 02	3.945610 02	2.114970 02	
4	1	23	4.345970 00	3.343110-01	6.165310-01	1.427270 02	5.032120 02	2.919630 02	
5	2	14	1.625120 01	1.535680 00	2.950050-01	2.744450 02	1.951340 02	8.080270 02	
6	3	7	1.625120 01	1.535680 00	2.950050-01	2.509230 02	1.778820 02	7.415800 02	
7	4	5	4.719270 00	2.208200-01	2.208200-01	2.237850 01	2.663080 01	5.346170 01	
8	4	32	2.504890 00	1.380200-01	1.380200-01	6.617840 00	2.346570 01	2.008760 01	
9	4	20	2.994250 00	1.283370-01	1.283370-01	1.171380 01	2.260060 01	2.001520 01	
10	5	6	5.039110 00	7.559180-01	2.432640 00	2.268200 02	3.537690 02	2.088950 02	
11	5	36	6.281560 00	2.907080-01	2.057810 00	2.220850 02	3.506370 02	1.021540 02	
12	5	17	1.362580 01	1.886880 00	8.236420 00	2.051640 02	1.267230 03	3.053350 02	
13	6	37	2.967010 00	1.206810-01	1.206810-01	1.902030 01	2.630140 01	4.303410 01	
14	6	18	3.395610 00	4.481760-01	1.879480 00	1.254170 02	3.215900 02	9.037530 01	
15	6	26	2.804940 00	1.034250-01	1.034250-01	7.202250 00	1.747690 01	1.677270 01	
16	6	38	4.689380 00	5.405150-01	5.405150-01	1.080240 01	3.324310 01	2.927170 01	
17	7	8	7.802890 00	3.620750 00	5.444930-01	3.637060 02	1.846460 02	6.524840 02	
18	7	9	6.011890 00	2.966300-01	2.289130 00	7.426870 02	5.508740 02	9.736920 01	
19	7	30	6.297460 00	2.192480 00	4.518520-01	8.427030 02	1.373080 03	6.733450 03	
20	7	35	1.479160 01	1.993570 01	1.278780 01	1.131630 03	3.011480 03	4.324090 03	
21	8	10	7.670390 00	1.061790 00	1.972790 00	1.355580 02	2.117480 02	2.215260 02	
22	8	15	7.589500 00	4.315670-01	4.315670-01	3.079070 01	2.486730 02	2.466460 02	
23	8	30	7.065460 00	3.032380-01	0.0	9.582460 01	0.0	9.086270 02	
24	9	10	6.405980 00	1.818270-01	1.818270-01	1.279540 01	1.535450 01	3.094960 01	
25	9	11	1.378710 01	7.339710-01	7.339710-01	8.668490 01	1.879030 02	2.057580 02	
26	9	12	3.772770 00	8.965910-02	1.734070 00	1.435630 02	3.275790 02	1.964970 01	
27	10	11	9.483210 00	9.954590-01	9.954590-01	8.981170 01	2.043560 02	2.367200 02	
28	10	13	3.582890 00	8.488020-02	8.488020-02	6.822460 00	7.520180 00	1.474340 01	
29	11	12	1.464050 01	7.794020-01	7.794020-01	9.052310 01	1.998390 02	2.135530 02	
30	11	13	9.326290 00	9.789860-01	9.789860-01	8.930540 01	2.030560 02	2.355150 02	
31	12	13	5.758420 00	2.099100-01	2.099100-01	1.572080 01	2.984940 01	4.373820 01	
32	12	14	8.063100 00	3.978380-01	3.070160 00	2.875650 02	7.401210 02	1.143800 02	
33	13	15	7.213370 00	9.990320-01	1.855250 00	1.709470 02	1.993410 02	2.715420 02	
34	14	15	7.802890 00	3.620750 00	3.661460 00	6.090780 02	1.471730 03	7.256990 02	
35	14	40	7.685550 00	7.657300-01	5.420320 00	4.105540 02	8.165660 02	1.733000 02	
36	14	28	1.144110 00	2.192480 00	4.518520-01	9.009380 02	1.410100 03	6.677860 03	
37	15	41	4.564670 00	2.633760-01	2.633760-01	4.127630 01	3.415370 01	9.401640 01	
38	15	28	7.065460 00	3.032380-01	0.0	9.852630 01	0.0	9.562920 02	
39	16	17	1.362060 01	1.886880 00	8.236420 00	2.202010 02	1.384350 03	3.330890 02	
40	16	18	4.867700 00	7.316170-01	2.349890 00	2.485250 02	3.875270 02	2.294080 02	
41	16	19	4.719270 00	2.208200-01	2.208200-01	2.444910 01	2.869090 01	5.846410 01	
42	18	42	4.198250 00	4.839050-01	4.839050-01	1.146390 01	3.479350 01	3.095490 01	
43	18	24	2.543060 00	9.376880-02	9.376880-02	7.602840 00	1.831260 01	1.811960 01	
44	19	20	2.994250 00	1.283370-01	1.283370-01	1.171350 01	2.260190 01	1.996540 01	
45	19	21	2.529640 00	1.393820-01	1.393820-01	6.619920 00	2.346540 01	2.606370 01	
46	21	22	2.117920 00	1.107650-01	1.107650-01	7.052800 00	9.999720 00	1.393760 01	
47	21	23	1.835770 00	2.003710-01	7.483960-01	7.422790 01	1.295660 02	6.657320 01	
48	23	25	1.986620 00	1.074990-01	1.024990-01	9.114200 00	1.187330 01	2.184700 01	
49	24	25	1.922710 00	8.740360-02	6.740360-02	6.755850 00	1.587250 01	1.414270 01	
50	24	26	3.514780 00	7.402430-01	1.219070 00	5.325340 01	1.568020 02	7.454650 01	
51	25	27	1.747650 00	1.054910-01	4.986500-01	1.501640 01	3.401070 01	1.041510 01	
52	26	27	1.924490 00	8.748470-02	8.748470-02	6.755850 00	1.587250 01	1.414160 01	
53	28	29	5.652880 00	2.348060 00	4.839160-01	6.307210 02	1.316870 03	6.811250 03	
54	30	31	5.652880 00	2.348060 00	4.839160-01	6.307210 02	1.316870 03	6.811240 03	
55	32	33	1.816150 00	1.982310-01	7.404030-01	7.422790 01	1.295680 02	6.657330 01	
56	22	32	2.097590 00	1.096860-01	1.096860-01	7.052790 00	9.998990 00	1.393660 01	
57	23	33	2.047630 00	3.250360-02	3.250360-02	4.410670 00	5.050790 00	9.561650 00	
58	27	33	1.323040 00	1.025240-01	1.025240-01	9.114200 00	1.187330 01	2.184700 01	
59	14	35	1.479160 01	1.993570 01	1.276790 01	1.254540 03	3.349630 03	4.787680 03	
60	20	34	7.827630 00	6.345530-01	6.345530-01	3.923420 01	1.010400 02	6.119760 01	
61	7	36	5.997430 00	2.188090 00	7.041570 00	5.131120 02	9.759780 02	4.817470 02	
62	8	36	4.338060 00	7.562670-01	2.433770 00	3.209370 02	4.137560 02	3.110400 02	
63	36	37	2.285040 00	9.585360-02	9.585360-02	2.563470 01	3.257350 01	6.024770 01	
64	5	37	3.985960 00	1.335150-01	1.335150-01	2.526270 01	2.817940 01	5.782380 01	
65	8	37	4.564670 00	2.633760-01	2.633760-01	3.510310 01	3.302620 01	7.969070 01	
66	38	39	2.096950 00	1.260100-01	1.260100-01	6.025580 00	2.553270 01	1.925860 01	
67	33	39	3.227860 00	3.702780-01	3.702780-01	1.013980 01	3.734450 01	3.346260 01	
68	32	38	1.566320 00	4.439120-02	4.439120-02	5.990360 00	1.884060 01	1.358000 01	
69	32	39	1.741430 00	6.100600-02	6.100600-02	7.776470 00	1.939800 01	1.407470 01	
70	5	38	3.797050 00	1.220150-01	1.220150-01	1.933840 01	2.452070 01	4.209370 01	
71	18	41	2.694970 00	1.096160-01	1.096160-01	1.914900 01	2.702760 01	4.344520 01	
72	16	40	4.441740 00	1.847520-01	1.847520-01	2.944090 01	3.296730 01	6.866850 01	
73	15	40	3.930890 00	1.681970-01	1.681970-01	3.531300 01	2.962660 01	8.142510 01	
74	40	41	2.285040 00	9.585360-02	9.585360-02	2.563470 01	3.257350 01	6.019910 01	
75	16	41	3.985960 00	1.335150-01	1.335150-01	2.669130 01	2.950890 01	6.103630 01	
76	42	43	2.096300 00	1.258920-01	1.258920-01	6.032850 00	2.551310 01	1.924990 01	
77	23	43	3.222330 00	3.683770-01	3.683770-01	1.018530 01	3.718830 01	3.341590 01	
78	16	42	3.797050 00	1.220150-01	1.220150-01	2.110510 01	2.622010 01	4.671780 01	
79	21	42	1.586660 00	4.496750-02	4.496750-02	5.990370 00	1.884050 01	1.364200 01	
80	21	43	1.763650 00	6.175660-02	6.175660-02	7.776060 00	1.933750 01	1.473030 01	
81	1	44	4.906180 00	2.259990 00	3.008870-01	4.897830 02	1.256580 02	7.791500 02	

Figure C-15. Airplane B 44 Mass, 81 Member Math Model Damping Data.

BEAM UNCOUPLED, UNDAMPED FREQUENCIES (CPS)

IJ	I	J	(1)	(2)	(3)	(4)	(5)	(6)
1	1	32	7.77780 01	5.42490 00	1.08480 01	2.95580 01	6.97120 01	3.23650 01
2	1	33	9.71690 01	7.47470 00	1.37850 01	3.80500 01	8.67690 01	4.40310 01
3	1	21	7.76070 01	5.41300 00	1.08240 01	2.95580 01	6.97120 01	3.23650 01
4	1	23	9.71690 01	7.47470 00	1.37850 01	3.80500 01	8.67690 01	4.40310 01
5	2	14	4.51170 02	4.26340 01	8.19000 00	1.30280 01	1.15190 01	4.67380 01
6	3	7	4.51170 02	4.26340 01	8.19000 00	1.42990 01	1.24490 01	5.12440 01
7	4	5	1.14870 02	5.37500 00	5.37500 00	2.07050 00	9.46460 00	4.59850 00
8	4	32	2.54850 02	1.40430 01	1.40430 01	6.42790 00	1.22650 01	1.44050 01
9	4	20	1.95930 02	8.39800 00	8.39800 00	2.99000 00	4.83510 00	7.51550 00
10	5	6	1.03100 02	1.54660 01	4.97710 01	1.94780 01	1.14670 02	1.78460 01
11	5	36	1.53440 02	7.10090 00	5.02650 01	1.17990 01	7.75950 01	5.29730 00
12	5	17	2.72040 02	3.07480 01	1.34220 02	3.67450 01	2.26960 02	2.53350 01
13	6	37	1.58830 02	6.46020 00	6.46020 00	2.13070 00	8.12660 00	4.96730 00
14	6	18	1.45430 02	1.91940 01	8.04940 01	7.74530 01	1.98600 02	4.95030 01
15	6	26	1.52300 02	5.61570 00	5.61570 00	5.02180 00	1.07670 01	1.19500 01
16	6	38	2.84780 02	3.28240 01	3.28240 01	1.13870 01	1.76250 01	2.06530 01
17	7	8	1.59590 02	7.40550 01	1.11360 01	1.25250 01	1.14210 01	4.22390 01
18	7	9	1.98690 02	9.80340 00	7.56540 01	1.37340 01	6.35460 01	6.06590 00
19	7	30	1.17950 02	4.10640 01	8.46290 00	2.76000 01	4.59910 01	8.67820 01
20	7	35	4.30900 02	5.80750 02	3.72530 02	9.77180 01	2.60050 02	2.90000 02
21	8	10	1.23700 02	1.71240 01	3.18160 01	9.87830 00	5.17810 01	1.43010 01
22	8	15	1.47100 02	8.36450 00	8.36450 00	3.14620 00	2.54090 01	7.22520 00
23	8	30	1.25960 02	5.40590 00	0.0	4.25110 00	0.0	1.20070 01
24	9	10	1.47700 02	4.19230 00	4.19230 00	6.53710 00	7.44490 00	7.64690 00
25	9	11	7.28020 01	3.87570 00	3.87570 00	2.61780 00	5.37400 00	4.79540 00
26	9	12	9.80080 01	2.32910 00	4.50470 01	2.56970 01	5.86350 01	3.71410 00
27	10	11	4.34160 01	4.55740 00	4.55740 00	2.82040 00	5.69490 00	5.12450 00
28	10	13	5.49110 01	1.30090 00	1.30090 00	2.89900 00	3.19540 00	3.39540 00
29	11	12	6.85580 01	3.64960 00	3.64960 00	2.48880 00	5.02410 00	4.66460 00
30	11	13	4.41470 01	4.63410 00	4.63410 00	2.82440 00	5.75040 00	5.14980 00
31	12	13	9.53820 01	3.47690 00	3.47690 00	3.21960 00	5.04080 00	6.17110 00
32	12	14	1.48140 02	7.30950 00	5.64080 01	1.15780 01	4.72270 01	5.17320 00
33	13	15	1.31540 02	1.82180 01	3.38320 01	7.83080 00	5.51150 01	1.16830 01
34	14	15	1.59590 02	7.40550 01	7.48870 01	1.48610 01	6.91570 01	3.54710 01
35	14	40	2.69980 02	2.68990 01	1.90410 02	1.37390 01	7.16440 01	6.72320 00
36	14	28	2.14280 01	4.10640 01	8.46290 00	2.68760 01	4.29090 01	8.49610 01
37	15	41	1.46450 02	8.44980 00	8.44980 00	1.39280 00	8.87950 00	3.22540 00
38	15	28	1.25960 02	5.40590 00	0.0	4.02760 00	0.0	1.14080 01
39	16	17	2.21960 02	3.07480 01	1.34220 02	3.36360 01	2.11460 02	2.32240 01
40	16	18	1.06730 02	1.60410 01	5.15240 01	1.77790 01	1.04680 02	1.63220 01
41	16	19	1.14870 02	5.37500 00	5.37500 00	1.89510 00	8.79370 00	4.20360 00
42	18	42	3.18090 02	3.66640 01	3.66640 01	1.06830 01	1.68590 01	1.95360 01
43	18	24	1.67980 02	6.19400 00	6.19400 00	4.87600 00	1.07770 01	1.12770 01
44	19	20	1.95930 02	8.39800 00	8.39800 00	2.98970 00	4.83510 00	7.52060 00
45	19	21	2.52360 02	1.39050 01	1.39050 01	8.42510 00	1.22650 01	1.44220 01
46	21	22	2.05610 02	1.07530 01	1.07530 01	3.27270 00	4.64010 00	5.39170 00
47	21	23	1.99740 02	2.18020 01	8.14300 01	5.33680 01	8.72240 01	2.49440 01
48	23	25	3.00890 02	1.55240 01	1.55240 01	9.94390 00	1.23150 01	1.30650 01
49	24	25	2.73920 02	1.24520 01	1.24520 01	6.70450 00	1.50470 01	1.68970 01
50	24	26	3.44370 02	7.25280 01	1.19440 02	3.28370 01	9.66870 01	7.06890 01
51	25	27	4.54540 02	2.74370 01	1.29690 02	3.62500 01	8.21040 01	1.68320 01
52	26	27	2.73670 02	1.24410 01	1.24410 01	6.70450 00	1.50470 01	1.68970 01
53	28	29	1.56770 02	6.51170 01	1.34200 01	3.43050 01	7.96460 01	1.04950 02
54	30	31	1.56770 02	6.51170 01	1.34200 01	3.43050 01	7.96460 01	1.04950 02
55	32	33	2.01900 02	2.20370 01	8.23100 01	5.33680 01	8.72240 01	2.49440 01
56	22	32	2.07570 02	1.08540 01	1.08540 01	3.27250 00	4.63980 00	5.39130 00
57	23	33	2.18690 02	3.47140 00	3.47140 00	2.95370 00	3.38240 00	3.65950 00
58	27	33	2.00290 02	1.55210 01	1.55210 01	9.94390 00	1.23150 01	1.30650 01
59	14	35	4.30900 02	5.80750 02	3.72530 02	8.78700 01	2.34570 02	2.61950 02
60	20	34	1.20140 02	9.74550 00	9.74550 00	3.03320 00	4.21850 00	4.73120 00
61	7	36	7.10680 02	7.68640 01	2.47360 02	1.99460 01	1.01170 02	2.06030 01
62	8	36	1.39180 02	2.42630 01	7.80820 01	1.51090 01	1.14410 02	1.47350 01
63	36	37	2.12690 02	8.92200 00	8.92200 00	1.58390 00	6.87840 00	3.75110 00
64	5	37	9.73620 01	3.26130 00	3.26130 00	1.33120 00	6.25170 00	3.02110 00
65	8	37	1.46450 02	8.44980 00	8.44980 00	1.63760 00	9.18200 00	3.05550 00
66	38	39	3.32010 02	1.99510 01	1.99510 01	1.01780 01	1.23030 01	1.63500 01
67	33	39	4.11740 02	4.72320 01	4.72320 01	1.31470 01	1.54040 01	1.79560 01
68	32	38	2.09630 02	5.94130 00	5.94130 00	6.39490 00	7.88230 00	9.06930 00
69	32	39	2.33070 02	8.16500 00	8.16500 00	7.10980 00	8.76350 00	1.00830 01
70	5	38	9.80500 01	3.15080 00	3.15080 00	1.72240 00	7.24490 00	3.74450 00
71	18	41	1.74860 02	7.11230 00	7.11230 00	2.11650 00	7.90830 00	4.92010 00
72	16	40	1.08500 02	4.51280 00	4.51280 00	1.40680 00	6.65280 00	3.18280 00
73	15	40	1.26110 02	5.39620 00	5.39620 00	1.19940 00	7.64660 00	2.77760 00
74	40	41	2.12690 02	8.92200 00	8.92200 00	1.58390 00	6.87840 00	3.75110 00
75	16	41	9.73620 01	3.26130 00	3.26130 00	1.76250 00	5.97010 00	2.85620 00
76	42	43	3.31910 02	1.99330 01	1.99330 01	1.01750 01	1.22990 01	1.63450 01
77	23	43	4.11040 02	4.69900 01	4.69900 01	1.31250 01	1.53780 01	1.79250 01
78	16	42	9.80500 01	3.15080 00	3.15080 00	1.57550 00	6.79990 00	3.43230 00
79	21	42	2.06950 02	5.86510 00	5.86510 00	6.39490 00	7.88230 00	9.06930 00
80	21	43	2.30030 02	8.05490 00	8.05490 00	7.10820 00	8.76160 00	1.00810 01
81	1	44	1.09440 02	5.04130 01	6.71170 00	9.67300 01	2.05920 01	1.53880 02

Figure C-16. Airplane B 44 Mass, 81 Member Math Model Frequency Data.

VEHICLE INITIAL CONDITIONS

VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)
 VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)
 EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)

XGDOT P°	YGDOT Q°	ZGDOT R°
PHI°	THETA°	PSI°
4.55000D 01	0.0	1.02000D 02
0.0	-1.56000D 00	0.0
0.0	-2.83000D 00	0.0

GENERALIZED SURFACE DATA

BETA = 0.0 DEGREES
 XGIN = 0.0
 ZGIN = 0.0

MODEL PARAMETERS

VEHICLE WT = 2.476790D 03

VEHICLE CG POSITION

X (FS) = 4.06266D 01
 Y (BL) = -2.44865D-01
 Z (WL) = 2.18889D 00

VEHICLE CG INITIAL GROUND COORDINATES

XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE CG, +FORWARD
 ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG, +DOWN
 XCG = 0.0
 ZCG = -4.08812D 01

VEHICLE INERTIAS (IN-LB-SEC**2)

I (XX) = 1.76551D 04
 I (YY) = 2.60677D 04
 I (ZZ) = 3.95496D 04

Figure C-17. Airplane B 44 Mass, 81 Member, Math Model Initial Conditions, Overall Mass, and c.g. Properties

MASS DATA

MASS COORDINATES F.S.,W.L.,B.L.					MASS MOMENTS OF INERTIA (LB-IN-SEC**2)		
I	W	X**	Y**	Z**	IX	IY	IZ
1	1.233000 02	2.331870 02	0.0	1.500000 01	2.669300 01	3.436000 01	4.266000 01
2	3.970000 01	1.737700 01	-4.042500 01	-4.716500 01	2.310000 01	2.477000 01	1.646700 01
3	3.970000 01	1.737700 01	4.042500 01	-4.716500 01	2.310000 01	2.477000 01	1.646700 01
4	6.390000 01	8.925000 01	0.0	-8.963000 00	2.683900 01	5.268000 01	2.126600 01
5	3.077000 02	6.457000 01	0.0	-1.027500 01	1.870600 02	4.353000 01	2.057000 01
6	8.176000 01	7.209000 01	0.0	2.050000 01	1.046000 01	1.566600 01	1.452800 01
7	1.533800 02	2.357000 01	0.0	-1.150000 01	3.115920 02	1.326800 02	2.614300 02
8	1.584600 02	2.357000 01	0.0	1.455400 01	2.739170 02	2.214300 01	2.738570 02
9	1.187400 02	8.750000-01	0.0	-1.818500 01	3.128000 01	6.318700 01	4.210100 01
10	2.064200 02	8.750000-01	0.0	1.184900 01	8.990000 00	3.901400 01	3.455400 01
11	5.597000 02	-1.503200 01	0.0	4.072000 00	2.285360 02	2.793880 02	3.536100 02
12	4.480000 01	1.101800 02	0.0	-7.850000 00	1.378500 01	3.855200 01	3.027900 01
13	3.138000 01	8.463000 01	0.0	4.731000 01	1.368900 01	1.216700 01	8.393000 00
14	1.182000 01	1.101800 02	0.0	4.581000 01	2.349000 00	4.624000 00	4.924000 00
15	9.306000 01	3.358000 01	1.210660 02	-2.500000 00	4.680000 02	3.540000 01	5.020000 02
16	1.770000 01	4.300000 01	3.369800 02	1.045000 01	4.500000-01	1.780000 00	2.150000 00
17	9.306000 01	3.358000 01	-1.210660 02	-2.500000 00	4.680000 02	3.540000 01	5.020000 02
18	1.770000 01	4.300000 01	-2.369800 02	1.045000 01	4.500000-01	1.780000 00	2.150000 00
19	3.300000 01	3.657000 01	0.0	-9.400000 00	1.326000 02	3.707400 01	1.246600 02
20	3.300000 01	4.357000 01	0.0	1.750000 01	1.326000 02	3.707200 01	1.246600 02
21	1.940000 01	8.154000 01	0.0	2.160000 01	4.600000 00	1.660000 01	9.400000 00
22	1.940000 01	1.607000 02	0.0	2.370000 01	4.600000 00	1.660000 01	9.400000 00
23	1.700000 02	8.087000 01	0.0	1.200000 01	4.900000 01	1.470000 02	1.330000 02
24	2.860000 01	1.101800 02	0.0	2.420000 01	5.925000 00	2.382800 01	2.035500 01
25	1.470000 01	2.332000 02	0.0	7.700000 01	6.400000 00	1.429000 01	6.400000 00

Figure C-18. Airplane B 25 Mass, 38 Member Math Model Mass Data

BEAM			MODULUS OF ELASTICITY		AREA		MODULUS OF RIGIDITY		MOMENTS OF INERTIA				LENGTH		DAMPING RATIO	
I	J		E		A	G			JX	I (YY)	I (ZZ)		XLB		CBAR	
1	1	12	1.05000	07	2.02000	00	4.00000	06	6.46800	01	5.19000	01	1.25110	02	1.00000-02	
2	1	24	1.05000	07	3.14140	00	4.00000	06	1.05360	02	8.14200	01	1.23400	02	1.00000-02	
3	2	7	3.00000	07	3.43620	00	1.10000	07	5.31060	00	1.89000-01	5.12160	00	5.42620	01	1.00000-02
4	3	7	3.00000	07	3.43620	00	1.10000	07	5.31060	00	1.89000-01	5.12160	00	5.42620	01	1.00000-02
5	4	5	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	3.32000-02	2.47150	01	1.00000-02	
6	4	12	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	3.32000-02	2.47150	01	1.00000-02	
7	4	23	2.90000	07	1.46400-01	1.10000	07	3.32000-02	1.66000-02	1.66000-02	1.66000-02	2.25760	01	1.00000-02		
8	5	6	2.90000	07	3.56600-01	1.10000	07	7.62240	00	6.95120	00	6.71200-01	3.16800	01	1.00000-02	
9	5	19	2.90000	07	5.85600-01	1.10000	07	4.20000	00	4.11880	00	8.12000-02	2.80140	01	1.00000-02	
10	5	20	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	3.48200	01	1.00000-02		
11	5	21	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	3.61110	01	1.00000-02		
12	6	13	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.95980	01	1.00000-02		
13	6	20	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.86770	01	1.00000-02		
14	6	21	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	9.51380	00	1.00000-02		
15	7	8	2.90000	07	6.34000-01	1.10000	07	3.21110	00	7.11000-02	3.14000	00	2.60540	01	1.00000-02	
16	7	9	2.90000	07	6.34000-01	1.10000	07	4.72320	00	4.64520	00	7.80000-02	2.36590	01	1.00000-02	
17	7	15	1.05000	07	3.10240	00	4.00000	06	6.36670	02	2.59400	01	1.21810	02	1.00000-02	
18	7	17	1.05000	07	3.10240	00	4.00000	06	6.36670	02	2.59400	01	1.21810	02	1.00000-02	
19	7	19	2.90000	07	3.56600-01	1.10000	07	7.62420	00	6.95120	00	6.73000-01	1.31690	01	1.00000-02	
20	8	10	2.90000	07	4.70200-01	1.10000	07	1.74960	00	1.35600	00	3.93300-01	2.26560	01	1.00000-02	
21	8	15	2.90000	07	1.37000	00	1.10000	07	5.26260	00	0.0	4.21700	00	1.22670	02	1.00000-02
22	8	17	2.90000	07	1.37000	00	1.10000	07	5.26260	00	0.0	4.21700	00	1.22670	02	1.00000-02
23	8	20	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.02100	01	1.00000-02		
24	9	10	2.90000	07	6.17400-01	1.10000	07	7.52000-02	3.76000-02	3.76000-02	3.76000-02	3.60340	01	1.00000-02		
25	9	11	2.90000	07	7.24600-01	1.10000	07	1.14000	00	5.70000-01	5.70000-01	2.73570	01	1.00000-02		
26	10	11	2.90000	07	7.24600-01	1.10000	07	1.14000	00	5.70000-01	5.70000-01	1.77660	01	1.00000-02		
27	12	21	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	4.10800	01	1.00000-02		
28	12	22	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	3.29430	01	1.00000-02		
29	12	24	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	3.26500	01	1.00000-02		
30	13	14	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.55940	01	1.00000-02		
31	14	24	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.10100	01	1.00000-02		
32	15	16	1.05000	07	3.10240	00	4.00000	06	6.36670	02	2.59400	01	1.17010	02	1.00000-02	
33	17	18	1.05000	07	3.10240	00	4.00000	06	6.36670	02	2.59400	01	1.17010	02	1.00000-02	
34	19	20	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.77960	01	1.00000-02		
35	21	22	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	1.92750	01	1.00000-02		
36	8	19	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	2.72540	01	1.00000-02		
37	22	24	2.90000	07	2.92800-01	1.10000	07	6.64000-02	3.32000-02	3.32000-02	3.32000-02	9.54360	00	1.00000-02		
38	1	25	1.05000	07	9.90600-01	4.00000	06	7.01200	01	1.20000	00	6.89200	01	1.00000-02		

Figure C-19. Airplane B 25 Mass, 38 Member Math Model Member Property Data

BEAM UNCOUPLED, UNDAMPED FREQUENCIES (CPS)																
I	J	(1)	(2)	(3)	(4)	(5)	(6)									
1	1	12	9.92740	01	6.96770	00	1.39330	01	3.60290	01	7.76000	01	7.76000	01	3.89000	01
1	1	24	1.31090	02	1.01590	01	1.87350	01	1.87350	01	5.15000	01	1.09840	02	5.72310	01
3	2	7	3.10160	02	2.41730	01	4.64370	00	4.64370	00	9.02630	00	8.20000	00	3.21310	01
3	3	7	3.10160	02	2.41730	01	4.64370	00	4.64370	00	9.02630	00	8.20000	00	3.21310	01
4	4	5	9.50780	01	4.48740	00	4.48740	00	4.48740	00	1.87080	00	6.40510	00	9.71300	00
4	5	9	9.50780	01	4.48740	00	4.48740	00	4.48740	00	1.87080	00	6.40510	00	9.71300	00
6	4	12	1.90820	02	1.06200	01	1.06200	01	1.06200	01	4.66140	00	7.14260	00	9.50220	00
6	4	23	8.86640	01	4.58110	00	4.58110	00	4.58110	00	3.28940	00	3.74230	00	3.74230	00
8	5	6	9.05270	01	1.35800	01	4.37030	01	4.37030	01	1.84230	01	1.04180	02	4.21150	01
9	5	19	1.31900	02	6.07350	00	4.32560	01	4.32560	01	1.14320	01	7.32100	01	7.65800	00
10	5	20	8.36750	01	2.80250	00	2.80250	00	2.80250	00	1.28930	00	5.89560	00	4.39210	00
11	5	21	8.36330	01	2.70820	00	2.70820	00	2.70820	00	1.63500	00	6.70280	00	9.49410	00
12	6	13	1.57450	02	6.20550	00	6.20550	00	6.20550	00	5.08770	00	1.06430	01	1.194910	01
13	6	20	1.58830	02	6.46050	00	6.46050	00	6.46050	00	2.12360	00	8.01610	00	4.94370	00
14	6	21	2.93710	02	3.60110	01	3.60110	01	3.60110	01	1.13630	01	1.77720	01	2.07010	01
15	7	8	1.48740	02	4.40130	01	6.62290	00	6.62290	00	7.65840	00	7.19660	00	2.57210	01
16	7	9	1.67250	02	8.58960	00	6.62870	01	6.62870	01	1.27370	01	5.42710	01	5.64930	00
17	7	15	1.03000	02	4.10990	01	8.47020	00	8.47020	00	2.60630	01	3.67140	01	8.35870	01
18	7	17	1.03000	02	4.10990	01	8.47020	00	8.47020	00	2.60630	01	3.67140	01	8.35870	01
19	7	19	2.02970	02	7.33510	01	2.35740	02	2.35740	02	1.90570	01	9.55870	01	1.97220	01
20	8	10	1.27490	02	1.76830	01	3.28140	01	3.28140	01	8.68340	00	5.33900	01	1.28120	01
21	8	15	1.12200	02	5.55890	00	0.0	0.0	0.0	0.0	4.01390	00	0.0	0.0	1.14160	01
22	8	17	1.12200	02	5.55890	00	0.0	0.0	0.0	0.0	4.01390	00	0.0	0.0	1.14160	01
23	8	20	1.46450	02	8.45030	00	8.45030	00	8.45030	00	1.50040	00	9.02730	00	3.47980	00
24	9	10	1.35250	02	3.84960	00	3.84960	00	3.84960	00	4.16220	00	5.99940	00	6.92730	00
25	9	11	1.05250	02	1.16210	01	1.16210	01	1.16210	01	6.68500	00	1.33680	01	1.24380	01
26	10	11	1.23550	02	2.14390	01	2.14390	01	2.14390	01	8.69060	00	1.72360	01	1.56100	01
27	12	21	1.77300	02	5.03450	00	5.03450	00	5.03450	00	4.94940	00	6.56180	00	7.73610	00
28	12	22	1.97990	02	7.01050	00	7.01050	00	7.01050	00	5.52690	00	7.32740	00	8.83860	00
29	12	24	1.74910	02	1.91070	01	7.13670	01	7.13670	01	4.22070	01	7.44230	01	2.21160	01
30	13	14	2.74020	02	1.24890	01	1.24890	01	1.24890	01	6.71360	01	1.50660	01	1.69180	01
31	14	24	3.11960	02	1.73170	01	1.73170	01	1.73170	01	1.03160	01	1.27750	01	1.35530	01
32	15	16	1.56760	02	6.51130	01	1.34190	01	1.34190	01	3.43050	01	7.96440	01	1.04950	02
33	17	18	1.56760	02	6.51130	01	1.34190	01	1.34190	01	3.43050	01	7.96440	01	1.04950	02
34	19	20	2.12730	02	8.92750	00	8.92750	00	8.92750	00	1.58420	00	6.87990	00	3.75190	00
35	21	22	3.33190	02	2.01640	01	2.01640	01	2.01640	01	1.02140	01	1.23470	01	1.84080	01
36	2	19	1.26130	02	5.39430	00	5.39430	00	5.39430	00	1.29220	00	7.77460	00	2.99690	00
37	22	24	4.24130	02	5.19250	01	5.19250	01	5.19250	01	1.35720	01	1.59010	01	1.85350	01
38	1	25	1.09020	02	5.08090	01	6.70440	00	6.70440	00	5.88450	01	2.05920	01	1.55260	01

Figure C-21. Airplane B 25 Mass, 38 Member Math Model Frequency Data

VEHICLE INITIAL CONDITIONS

VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)
 VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)
 EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)

XGDOT	YGDOT	ZGDOT
P°	Q°	R°
PHI°	THETA°	PSI°
4.55000D 01	0.0	1.02000D 02
0.0	-1.56000D 00	0.0
0.0	-2.83000D 00	0.0

GENERALIZED SURFACE DATA

BETA = 0.0 DEGREES
 XGIN = 0.0
 ZGIN = 0.0

MODEL PARAMETERS

VEHICLE WT = 2.474190D 03

VEHICLE CG POSITION
 X (FS) = 4.20414D 01
 Y (BL) = 0.0
 Z (WL) = 2.30509D 00

VEHICLE INERTIAS (IN-LB-SEC**2)
 I (XX) = 1.67144D 04
 I (YY) = 2.55400D 04
 I (ZZ) = 3.78100D 04

VEHICLE CG INITIAL GROUND COORDINATES
 XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE CG, +FORWARD
 ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG, +DOWN
 XCG = 0.0
 ZCG = -4.12043D 01

Figure C-22. Airplane B 25 Mass, 38 Member Math Model Initial Conditions, Overall Mass and c.g. Properties

VEHICLE INITIAL CONDITIONS

VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)
 VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)
 EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)

XGDOT	YGDOT	ZGDOT
P°	Q°	R°
PHI°	THETA°	PSI°
2.590600 02	0.0	1.950000 01
0.0	-1.850000 00	0.0
0.0	-6.730000-01	0.0

GENERALIZED SURFACE DATA

BETA = 90.0 DEGREES
 XGIN = 0.0
 ZGIN = 100.0

MODEL PARAMETERS

VEHICLE WT = 2.4741900 03

VEHICLE CG POSITION
 X (FS) = 4.113640 01
 Y (FL) = 0.0
 Z (WL) = 1.936720 00

VEHICLE CG INITIAL GROUND COORDINATES
 XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE CG, *FORWARD
 ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG, *DOWN
 XCG = -6.402010 01
 ZCG = -1.483030 02

VEHICLE INERTIAS (IN-LB-SEC**2)
 I (XX) = 1.650070 04
 I (YY) = 2.549840 04
 I (ZZ) = 3.648350 04

Figure C-23. Airplane B 24 Mass, 37 Member Math Model Initial Conditions and Model Parameter Data

VEHICLE INITIAL CONDITIONS

VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)
 VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)
 EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)

XGDOT	YGDOT	ZGDOT
P°	Q°	R°
PHI°	THETA°	PSI°
2.59000D 02	0.0	1.95000D 01
0.0	-1.85000D 00	0.0
0.0	-6.73000D-01	0.0

GENERALIZED SURFACE DATA

BETA = 90.0 DEGREES
 XGIN = 0.0
 ZGIN = 100.0

MODEL PARAMETERS

VEHICLE WT = 2.477090D 03

VEHICLE CG POSITION
 X (FS) = 4.15536D 01
 Y (BL) = -2.44836D-01
 Z (WL) = 1.82251D 00

VEHICLE CG INITIAL GROUND COORDINATES
 XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE CG,+FORWARD
 ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG,+DOWN
 XCG = -6.0664D 01
 ZCG = -1.46762D 02

VEHICLE INERTIAS (IN-LB-SEC**2)
 I(XX) = 1.74411D 04
 I(YY) = 2.52001D 04
 I(ZZ) = 3.88975D 04

Figure C-24. Airplane B 40 Mass, 80 Member Math Model Initial Conditions and Model Parameter Data